

# Products of our daily trivial discussion

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# WFS: Ambition

- Initial motivation: intuitive (or, geometric) understanding of the coupled WFS (cWFS)
- During the calculation I noticed
  - ◉ Why WFS is called “wave front” sensor
  - ◉ Most people fall a pitfall in calculating WFS
- Of course I was able to explain cWFS in a geometrical way
- In this section:
  - ◉ Introduce Hermite-Gaussian (HG) modes
  - ◉ Show the pitfall in calculation of WFS
  - ◉ Explain cWFS in a geometrical way

# WFS: HG Mode

Hermite Gaussian HG<sub>lm</sub> mode

$$U_{lm}(x, y, z) = \left( \frac{2}{\pi w(z)} \right)^{\frac{1}{2}} e^{i(1+l+m)\eta(z) - ikz} \exp \left[ -\frac{x^2 + y^2}{w(z)^2} - ik \frac{x^2 + y^2}{2R(z)} \right]$$

$$w(z) = w_0 \sqrt{1 + \left( \frac{z}{z_R} \right)^2} : \text{beam radius} \quad R(z) = \frac{z^2 + z_R^2}{z} : \text{radius of curvature}$$

$$\eta(z) = \tan^{-1} \frac{z}{z_R} : \text{Gouy phase} \quad w_0 : \text{beam waist} \quad z_R = \frac{k w_0^2}{2} : \text{Rayleigh range}$$

Divide it in each axis:

$$U_l(x, z) = \left( \frac{2}{\pi w(z)} \right)^{\frac{1}{4}} \sqrt{\frac{1}{2^l l!}} H_l \left( \frac{\sqrt{2} x}{w(z)} \right) e^{il\eta(z)} \exp \left[ -\frac{x^2}{w(z)^2} - i \frac{k x^2}{2R(z)} \right]$$

$$U_{lm}(x, y, z) = e^{-ikz} U_l(x, z) U_m(y, z)$$

# WFS: Basis w/o Gouy Phase

Introduce HG basis without Gouy phase:

$$u_l(x, z) = U_l(x, z)e^{-il\eta(z)}$$

i.e.

$$u_l(x, z) = \left(\frac{2}{\pi w(z)}\right)^{\frac{1}{4}} \sqrt{\frac{1}{2^l l!}} H_l\left(\frac{\sqrt{2}x}{w(z)}\right) \exp\left[-\frac{x^2}{w(z)^2} - i\frac{kx^2}{2R(z)}\right]$$

Using this, HG<sub>lm</sub> mode can be written as:

$$U_{lm}(x, y, z) = e^{i(1+l+m)\eta(z) - ikz} u_l(x, z) u_m(y, z)$$

I'll show that mistaking  $u_l(x, z)$  as  $U_l(x, z)$  makes wrong results

# WFS: Fundamental Basis

From now on I consider (z,x) plane (ignore y-axis dependency)

- Fundamental mode

$$U_0(x, z) = u_0(x, z) = \left( \frac{2}{\pi w(z)} \right)^{\frac{1}{4}} \exp \left[ -\frac{x^2}{w(z)^2} - i \frac{kx^2}{2R(z)} \right]$$

- 1st mode

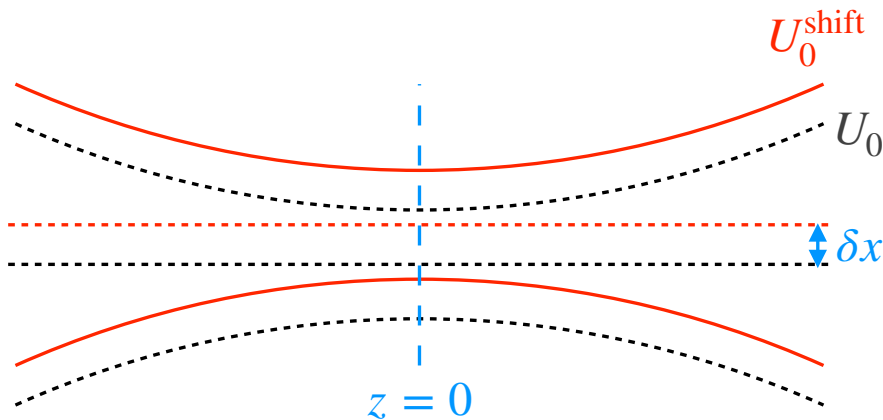
$$\begin{aligned} U_1(x, z) &= \left( \frac{2}{\pi w(z)} \right)^{\frac{1}{4}} \frac{2x}{w(z)} e^{i\eta(z)} \exp \left[ -\frac{x^2}{w(z)^2} - i \frac{kx^2}{2R(z)} \right] \\ &= \frac{2x}{w(z)} e^{i\eta(z)} U_0(x, z) \end{aligned}$$

- When considering correspondence of wave optics to ray optics these two modes is enough

# WFS: Transformation of Basis

Beam axis change at beam waist ( $z=0$ )

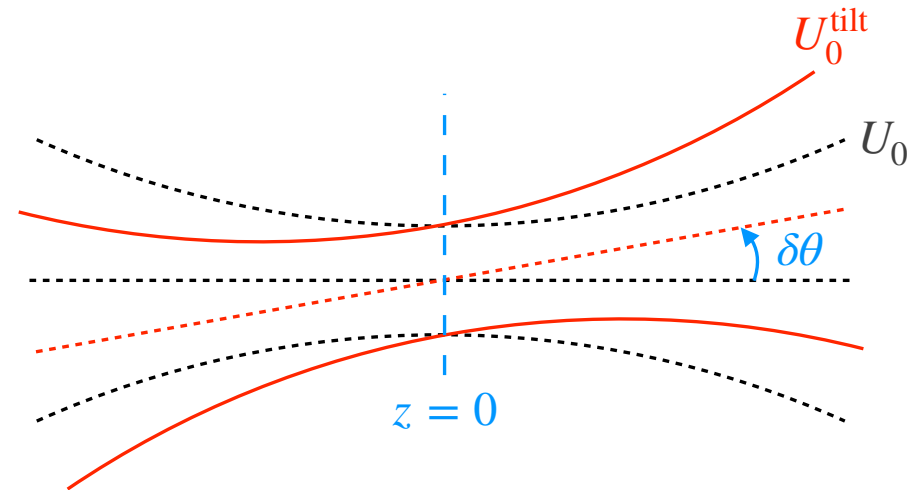
- shift



$$U_0^{\text{shift}}(x, z) = U_0(x, z) + \frac{\delta x}{w_0} U_1(x, z)$$

$$U_1^{\text{shift}}(x, z) = U_1(x, z) - \frac{\delta x}{w_0} U_0(x, z)$$

- tilt



$$U_0^{\text{tilt}}(x, z) = U_0(x, z) - \frac{\delta\theta}{\alpha_0} U_1(x, z)$$

$$U_1^{\text{tilt}}(x, z) = U_1(x, z) - \frac{\delta\theta}{\alpha_0} U_0(x, z)$$

# WFS: Transformation of Basis

- Backward beam

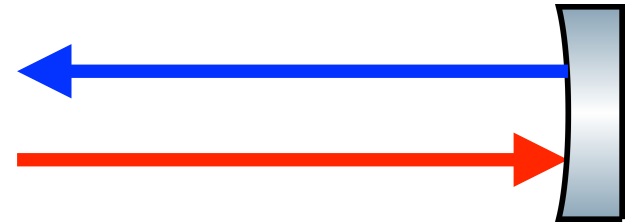
$$U^{\leftarrow}(x, z) = (U^{\rightarrow}(x, z))^*$$

- Reflection by a mode-matched mirror (i.e. a mirror with the same curvature as the beam)

$$U_l^{\leftarrow}(x, z) = (U_l^{\rightarrow}(x, z))^* \times e^{i2l\eta(z)}$$

Why?

- Phase of actual incident beam:  $l\eta(z)$
- Phase of basis of outgoing beam:  $-l\eta(z)$
- For continuity of phase, the reflected beam must proceed by  $2l\eta(z)$  relative to the basis



# WFS: Transformation of Basis

- Matrix notation

$$\gamma := \frac{\delta x}{w_0} - i \frac{\delta \theta}{\alpha_0}, \quad M_\gamma := \begin{pmatrix} 1 & -\gamma^* \\ \gamma & 1 \end{pmatrix}$$

$$(U'_0 \ U'_1) = (U_0 \ U_1) \begin{pmatrix} 1 & -\gamma^* \\ \gamma & 1 \end{pmatrix} = (U_0 \ U_1) M_\gamma$$

- Inverse transformation

$$M_\gamma^{-1} = \frac{1}{|\gamma|^2} \begin{pmatrix} 1 & \gamma^* \\ -\gamma & 1 \end{pmatrix} \simeq \begin{pmatrix} 1 & \gamma^* \\ -\gamma & 1 \end{pmatrix}$$

for small  $\gamma$  ( $|\gamma| \ll 1$ )



# WFS: Measurement by Detector

- QPD signal = beat between  $u_0$  &  $u_1$
- Consider

$$U'_1(x, z) = \left( \frac{\delta x}{w_0} - i \frac{\delta \theta}{\alpha_0} \right) U_1(x, z) = \left( \frac{\delta x}{w_0} - i \frac{\delta \theta}{\alpha_0} \right) e^{i\eta(z)} u_1(x, z)$$

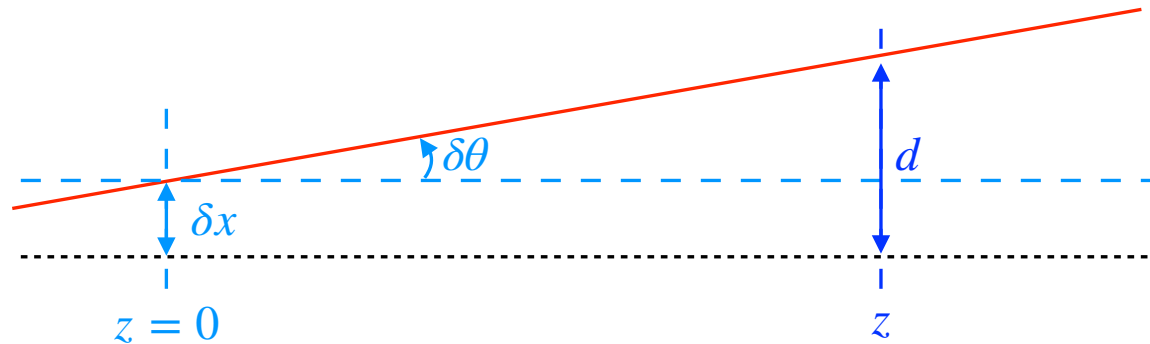
- After some math, we get

$$\begin{aligned} \left( \frac{\delta x}{w_0} - i \frac{\delta \theta}{\alpha_0} \right) e^{i\eta(z)} &= \left( \frac{\delta x}{w_0} \cos \eta(z) + \frac{\delta \theta}{\alpha_0} \sin \eta(z) \right) + i \left( \frac{\delta x}{w_0} \sin \eta(z) - \frac{\delta \theta}{\alpha_0} \cos \eta(z) \right) \\ &= \frac{\delta x + z \delta \theta}{w(z)} - i \frac{k w(z)}{2} \frac{(R(x) - z) \delta \theta - \delta x}{R(z)} \end{aligned}$$

- real part: beam position shift at  $z$
- imaginary part: crossing angle of wavefronts at  $x=0$

# WFS: Optical Lever

- Consider the beam center shift  $d$  at  $z$



- For a beam shifted by  $\delta x$  and tilted by  $\delta\theta$  at the beam waist
- Beam center shift  $d = \delta x + z\delta\theta$
- Real part of the beat signal is

$$\frac{d}{w(z)}$$

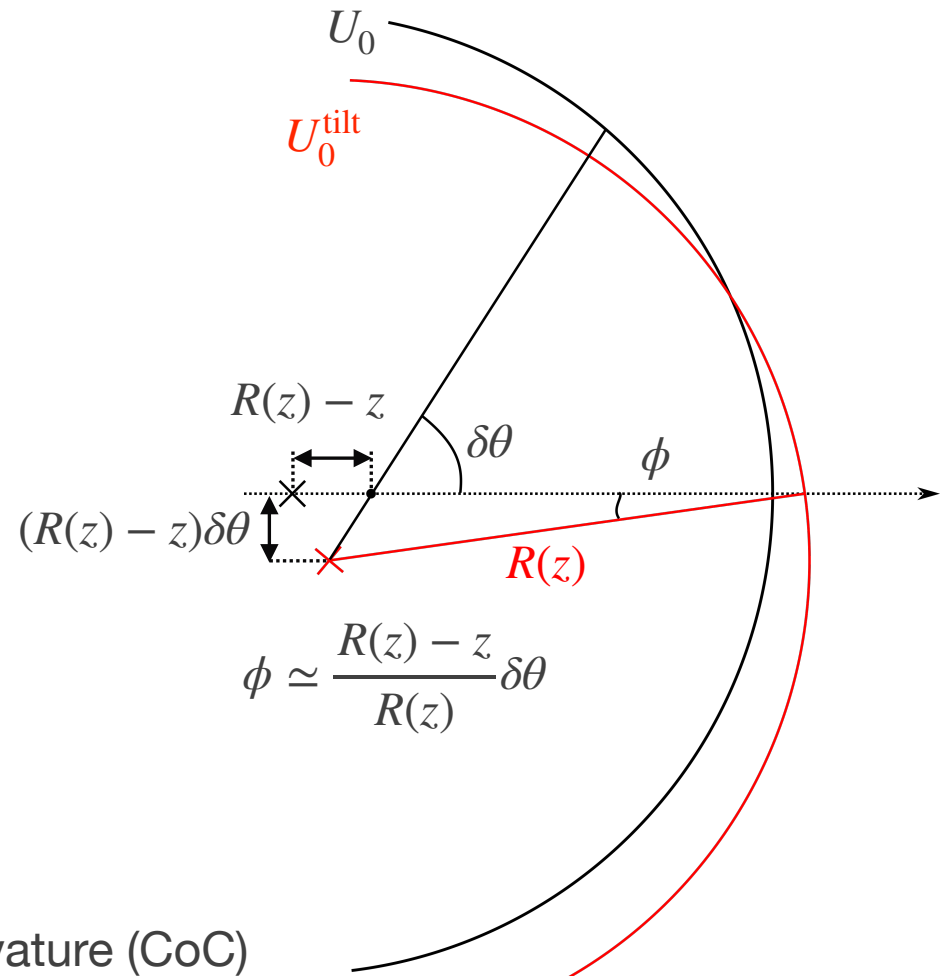
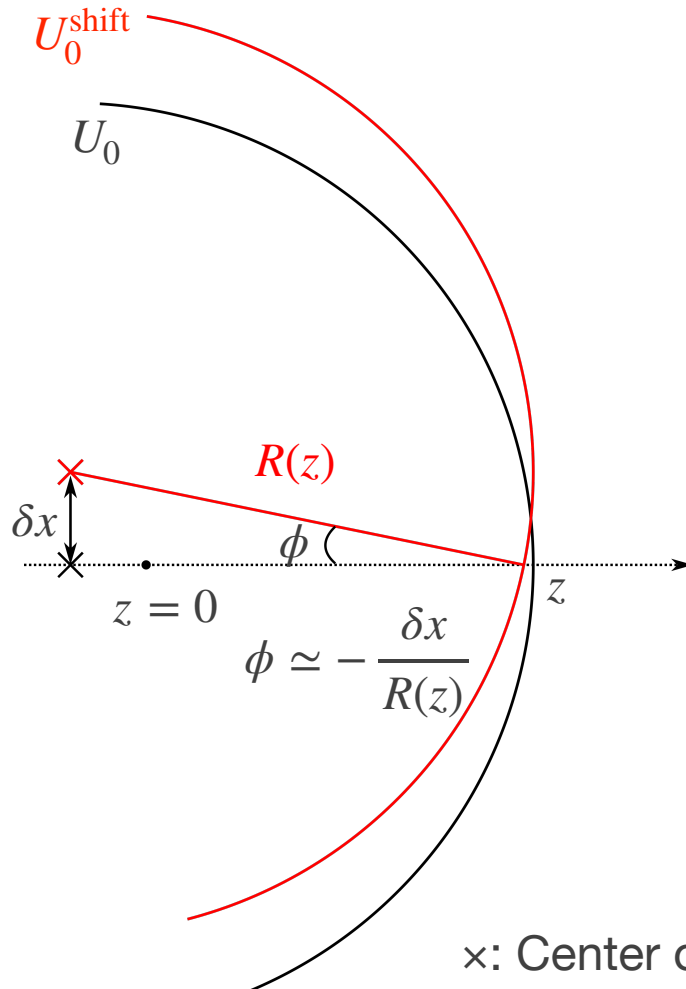
- Sensing beam spot shift

# WFS: Crossing Angle of Wave Fronts

- Consider crossing angle  $\phi$  of wave fronts at  $(x=0, z)$ :

- shift

- tilt

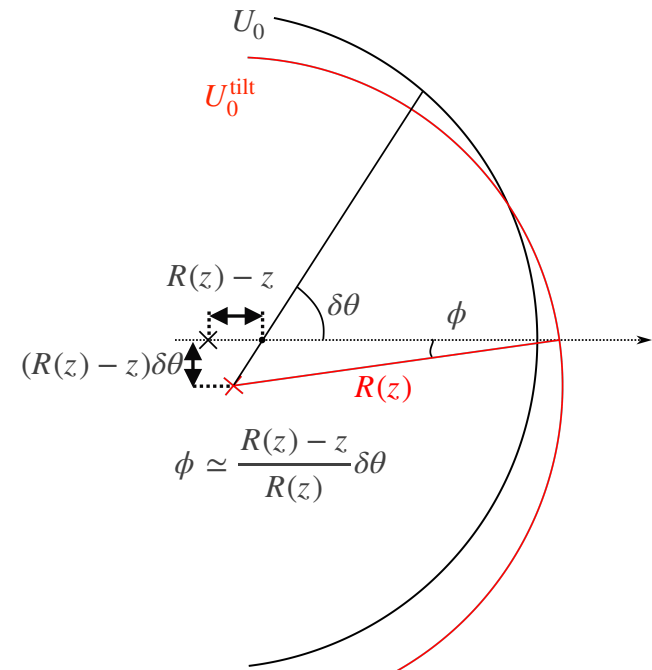
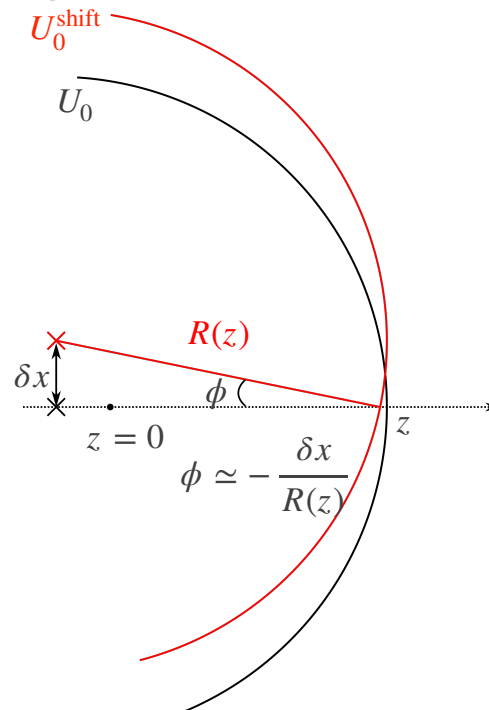


# WFS: Crossing Angle of Wave Fronts

- Consider crossing angle  $\phi$  of wave fronts at  $(x=0, z)$ :

$$\phi = \frac{(R(z) - z)\delta\theta - \delta x}{R(z)}$$

- Imaginary part of the beat signal  $\propto \phi$ 
  - Sensing crossing angle of wave front



# WFS: Signal Detection

Beat signal:

- Real = beam center shift
- Imag = crossing angle of wave front

How to extract these signals?

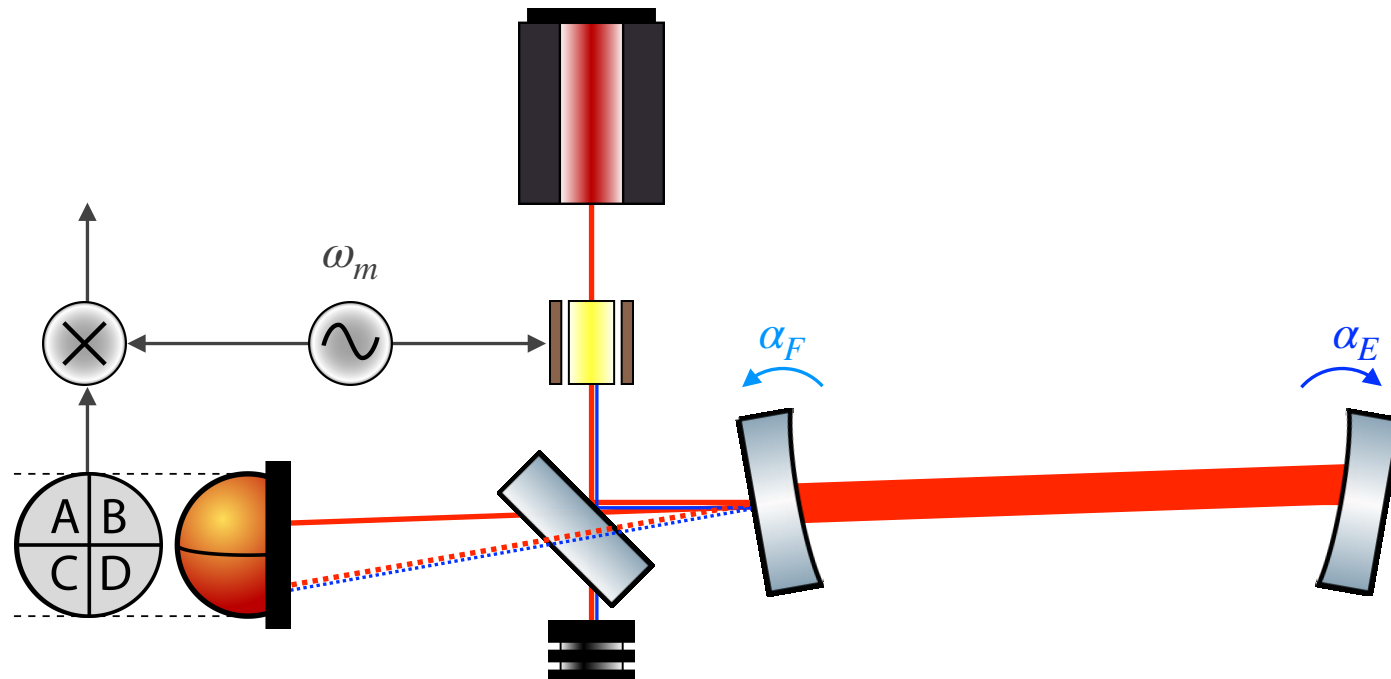
- Real: DC signal  $\rightarrow$  optical lever

$$\int_{\text{QPD}} dS \left| u_0 + \gamma u_1 \right|^2 = \int_{\text{QPD}} dS 2u_0 u_1 \text{Re}[\gamma] \propto \text{Re}[\gamma]$$

- Imag: phase modulation/demodulation  $\rightarrow$  WFS

$$\begin{aligned} \int_{\text{QPD}} dS \left| \gamma u_1 + u_0 e^{i\omega_m t} - u_0 e^{-i\omega_m t} \right|^2 &= \int_{\text{QPD}} dS 2u_0 u_1 \text{Im}[\gamma] \sin \omega_m t \\ &\propto \text{Im}[\gamma] \sin \omega_m t \end{aligned}$$

# WFS: Brief Introduction



- Front/End mirror tilt  $\rightarrow$  change cavity axis
- Phase modulation  $\rightarrow$  off resonance, reflected by the front mirror
- Measure beat signal between cavity-leakage and phase-modulated beam

# WFS: Mathematics

- $\gamma$  : axis difference between incident and cavity
- $\gamma_r$  : axis difference between cavity and front reflected
- Now incident beam is

$$E_{\text{in}} = \begin{pmatrix} U_0 & U_1 \end{pmatrix} \begin{pmatrix} a_0 \\ a_1 \end{pmatrix}$$

- Then, reflected beam is

$$\begin{aligned} E_{\text{refl}} &= \begin{pmatrix} U_0^c & U_1^c \end{pmatrix}^* e^{-2i\eta_F} \begin{pmatrix} r_0 & 0 \\ 0 & r_1 \end{pmatrix} M_\gamma \begin{pmatrix} a_0 \\ a_1 \end{pmatrix} \\ &= \begin{pmatrix} U_0^r & U_1^r \end{pmatrix}^* M_{\gamma_r}^{-1} \begin{pmatrix} r_0 & 0 \\ 0 & r_1 \end{pmatrix} M_\gamma \begin{pmatrix} a_0 \\ a_1 \end{pmatrix} \end{aligned}$$

$r_i$  : cavity reflectivity  
of each mode

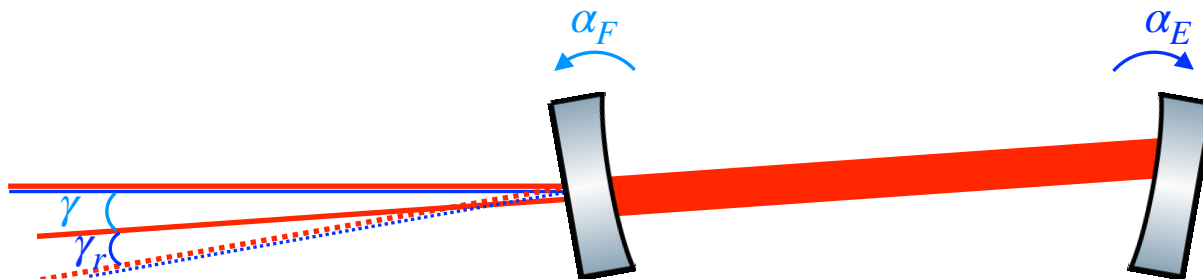
$U_i$  : incident axis

$U_i^c$  : cavity axis

$U_i^r$  : front refl. axis

$\eta_F$  : Gouy phase  
at front mirror

Pitfalls



# WFS: Why Pitfalls

- When considering resonant condition of higher order mode, Gouy phase diff. from TEM<sub>00</sub> is taken into account
  - ▶ We calculate coefficients of  $u_l$ , not  $U_l$
  - ▶ If applying transformation of the basis, we have to compensate Gouy phase at the position of the mirrors!
- In many literatures authors forgot this correction and obtained wrong results...
- WFS signal

$$W_{\text{WFS}} \propto \frac{\delta x_r}{w_0} \sin \eta - \frac{\delta \theta_r}{\alpha_0} \cos \eta$$

- In Michimura-san's document

$$W_{\text{WFS}} \propto \frac{\delta x}{w_0} \sin \eta - \frac{\delta \theta}{\alpha_0} \cos \eta$$

- The mistake comes from this Gouy phase difference

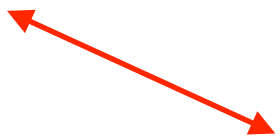


# WFS: Why WFS

- Again, WFS signal

$$W_{\text{WFS}} \propto \frac{\delta x_r}{w_0} \sin \eta - \frac{\delta \theta_r}{\alpha_0} \cos \eta$$

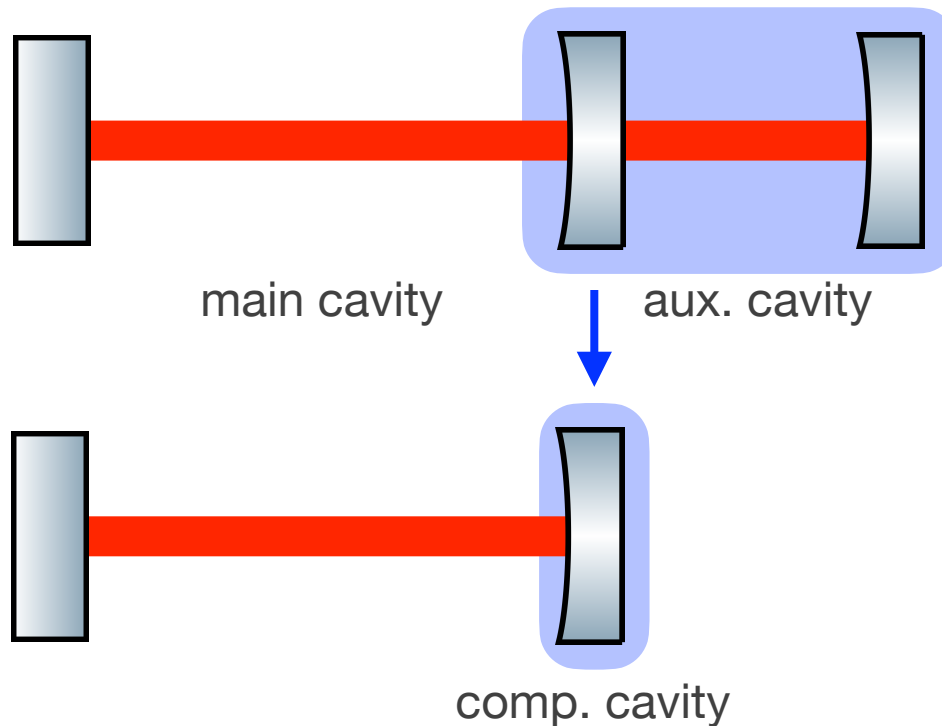
- Beat between  $u_0$  and  $u_1$

$$\left( \frac{\delta x}{w_0} - i \frac{\delta \theta}{\alpha_0} \right) e^{i\eta(z)} = \underbrace{\left( \frac{\delta x}{w_0} \cos \eta(z) + \frac{\delta \theta}{\alpha_0} \sin \eta(z) \right)}_{\text{beam spot shift}} + i \underbrace{\left( \frac{\delta x}{w_0} \sin \eta(z) - \frac{\delta \theta}{\alpha_0} \cos \eta(z) \right)}_{\text{wave front}}$$


- ▶ WFS actually sees crossing angle of wavefronts
- ▶ between cavity leakage & front refl. beam

# WFS: Coupled WFS


- Ordinary WFS:  $HG_{10}$  is off resonance
- Coupled WFS:  $HG_{10}$  also on resonance thanks to the aux. cavity



- How can we understand cWFS if we take the aux.cavity as a compound mirror?

# WFS Reflection at Mid Mirror

- Reflected beam:  $U_0^{\text{refl}} = e^{2i\eta} U_0$ ,  $U_1^{\text{refl}} = e^{4i\eta} U_1$
- When incident beam is

$$U_0 + \left( \frac{\delta x}{w_0} - i \frac{\delta \theta}{\alpha_0} \right) U_1$$


- then reflected beam is

$$e^{2i\eta} \left[ U_0 + \left( \frac{\delta x}{w_0} - i \frac{\delta \theta}{\alpha_0} \right) e^{2i\eta} U_1 \right]$$

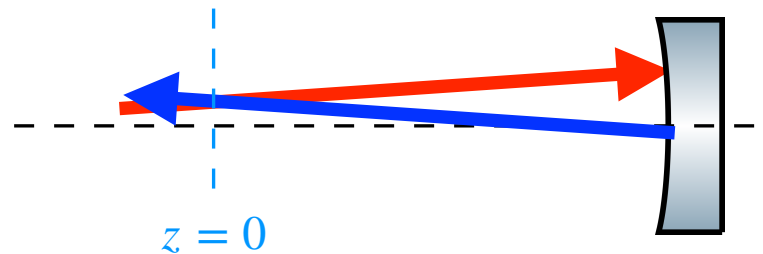
$$= e^{2i\eta} \left[ U_0 + \left( \frac{(1 - 2\frac{z}{R})\delta x + 2(1 - \frac{z}{R})z\delta \theta}{w_0} - i \frac{(1 - \frac{2z}{R})\delta \theta - \frac{2}{R}\delta x}{\alpha_0} \right) U_1 \right]$$

- The result is coincident with that of ray optics

# WFS: Reflection by Compound Mirror

- For the compound mirror, Gouy phase difference of HG<sub>00</sub> & HG<sub>10</sub> is compensated
  - ▶ Reflection beam is

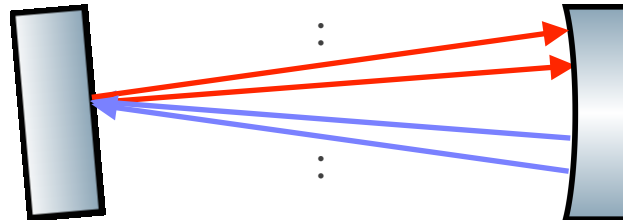
$$e^{2i\eta} \left[ U_0 + \left( \frac{\delta x}{w_0} - i \frac{\delta \theta}{\alpha_0} \right) e^{2i\eta} U_1 \times e^{-2i\eta} \right] = e^{2i\eta} \left[ U_0 + \left( \frac{\delta x}{w_0} - i \frac{\delta \theta}{\alpha_0} \right) U_1 \right]$$



- What this means?
  - ▶ Reflected beam goes to the same position at the beam waist

# WFS: Understanding cWFS

- Every time reflected by front mirror tilted  $\alpha_F$ , the beam tilt increase by  $2\alpha_F$
- After reflected by comp. mirror beam goes to the same position at the waist = front mirror without changing beam tilt
- The beam tilt again increase by front mirror reflection
- ...
- Finally, the beam tilt is increased by number of cavity reflection  $\propto$  cavity Finesse !

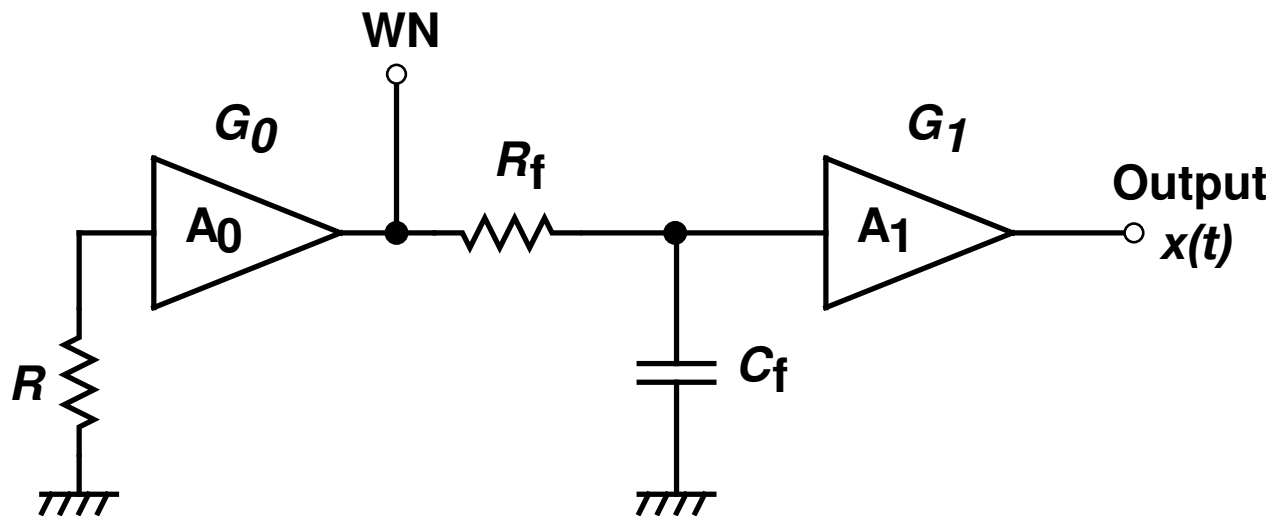


# Statistics: Motivation

- At start: question about Brown motion experiments
- How should we consider statistical error exactly in these experiments?
- Is what we've told B3 students right or not?
- Furthermore, the statistical analysis of Brown motion and axion search seems to have something in common
- In this section:
  - ◉ Statistical error of thermal noise of resistor
  - ◉ Statistical error of Brown motion
  - ◉ Common point of Brown motion and axion search

# Statistics: Thermal Noise of Resistors

- Measure thermal noise of resistors and estimate temperature of the resistor
- We impose students to take measurements so that statistical error is within 5%
- Output is low-passed
  - ▶ Effective number of measurements decreases by a factor of  $\tau_f$
  - ▶  $\tau_f$  : time constant of autocorrelation (= that of the low-pass filter)



# Statistics: Question for Thermal Noise

## Questions

- How should we consider the statistical error of variance?
  - ◉  $T \propto \text{Var}[x] \rightarrow$  error of  $T$  is prop. to error of variance of  $x$
  - ◉ Need to consider 4th order moment?
- What is the exact factor to be divided for calculating the statistical error?
  - ◉ Exactly  $\tau_f$  ? Is there any factor?

## Answers

- Calculate 4th order moment
  - ◉ Gaussian  $\rightarrow$  written by autocorrelation
- The factor is EXACTLY  $\tau_f$



# Statistics: No Filter Case

- First, consider the output without a low-pass filter
- $\hat{x}(t)$ : white Gaussian with  $\sigma_x^2$ ,  $E[\hat{x}(t)] = 0$ ,  $\text{Var}[\hat{x}(t)] = \sigma_x^2$
- Autocorrelation  $R_x(\tau) := E[\hat{x}(t)\hat{x}(t + \tau)] = \lim_{\Delta t \rightarrow 0} \sigma_x^2 \delta(\tau) \Delta t$
- Estimated variance

$$\hat{\sigma}_x^2 := \frac{1}{T} \int_{-T/2}^{T/2} dt \hat{x}(t)$$

- Mean of  $\hat{\sigma}_x^2$

$$E[\hat{\sigma}_x^2] = \frac{1}{T} \int_{-T/2}^{T/2} dt E[\hat{x}(t)^2] = \sigma_x^2$$

► unbiased estimator

- Variance of  $\hat{\sigma}_x^2$

$$\begin{aligned} \text{Var}[\hat{\sigma}_x^2] &= E[(\hat{\sigma}_x^2)^2] - E[\hat{\sigma}_x^2]^2 = \dots \\ &= \frac{2}{T} \sigma_x^4 \end{aligned}$$

# Statistics: With Filter

- Next, consider with filter
- $\hat{y}(t)$ : noise filtered by  $h(t)$ :  $\hat{y}(t) = \hat{x}(t) * h(t)$ ,  $E[\hat{y}(t)] = 0$ ,

$$\text{Var}[\hat{y}(t)] = \sigma_x^2 \int_{-\infty}^{\infty} df \left| \tilde{h}(f) \right|^2 =: \sigma_y^2$$

- Estimated variance

$$\hat{\sigma}_y^2 := \frac{1}{N} \sum_{n=0}^{N-1} \hat{y}(n)^2$$

- Mean of  $\hat{\sigma}_y^2$

$$E[\hat{\sigma}_y^2] = \frac{1}{N} \sum_{n=0}^{N-1} E[\hat{y}(n)^2] = \sigma_y^2$$

- ▶ unbiased estimator

# Statistics: With Filter

$$\begin{aligned} E[(\hat{\sigma}_y^2)^2] &= \frac{1}{T^2} \int_{-T/2}^{T/2} dt_1 \int_{-T/2}^{T/2} dt_2 E[\hat{y}(t_1)^2 \hat{y}(t_2)^2] = \dots \\ &= \sigma_y^4 + \frac{4}{T} \int_0^T d\tau (T - |\tau|) R(\tau)^2 \end{aligned}$$

- Therefore

$$\text{Var}[\hat{\sigma}_y^2] = \frac{4}{T^2} \int_0^T d\tau (T - |\tau|) R(\tau)^2$$

- For enough large  $T$

$$\text{Var}[\hat{\sigma}_y^2] \simeq \frac{4}{T} \int_0^T d\tau R(\tau)^2$$

# Statistics: With Filter

- In our case

$$\sigma_y^2 = \frac{\sigma_x^2}{R_f C_f} = \frac{\sigma_x^2}{\tau_f}, \quad R(\tau) = \frac{\sigma_x^2}{2R_f C_f} e^{-\frac{\tau}{R_f C_f}} = \frac{\sigma_x^2}{2\tau_f} e^{-\frac{\tau}{\tau_f}} = \sigma_y^2 e^{-\frac{\tau}{\tau_f}}$$

- Then, for  $T \gg \tau_f$

$$\text{Var}[\hat{\sigma}_y^2] \simeq \frac{2\tau_f}{T} \sigma_y^2$$

- Comparing to no filter case:

$$\text{Var}[\hat{\sigma}_x^2] = \frac{2}{T} \sigma_x^2 \qquad \text{Var}[\hat{\sigma}_y^2] = \frac{2\tau_f}{T} \sigma_y^2$$

- Due to the low-pass filter, statistical error is bigger by  $\tau_f$ 
  - ▶ Fortunately, what we've told to B3 student is right!

# Statistics: SNR of Brown Motion

- Signal:  $\hat{x}[n]$
- Spectral density estimator

$$\hat{S}_j^T := \frac{2}{T} \left| \sum_{n=0}^{N-1} \hat{x}[n] e^{-i2\pi \frac{nj}{N}} \right|^2$$

- Hypotheses

$$H_0 : \hat{x}[n] = \hat{w}[n]$$

$$H_1 : \hat{x}[n] = \hat{s}[n] + \hat{w}[n]$$

- For each hypothesis, the probability density is:

$$p \left( \hat{S}_j^T \mid H_0 \right) = \frac{1}{S_w(f_j)} \exp \left[ -\frac{\hat{S}_j^T}{S_w(f_j)} \right] \quad \mathbb{E} \left[ \hat{S}_j^T \mid H_0 \right] = S_w(f_j)$$

$$p \left( \hat{S}_j^T \mid H_1 \right) = \frac{1}{S_w(f_j)} \exp \left[ -\frac{\hat{S}_j^T}{S_s(f_j) + S_w(f_j)} \right] \quad \mathbb{E} \left[ \hat{S}_j^T \mid H_1 \right] = S_s(f_j) + S_w(f_j)$$

# Statistics: Likelihood Ratio

- Next, define likelihood ratio:

$$\Lambda(\hat{x} | H_1) := \frac{p(\hat{x} | H_1)}{p(\hat{x} | H_0)}$$
$$= \prod_{j=1}^{N-1} \frac{p(\hat{S}_j^T | H_1)}{p(\hat{S}_j^T | H_0)}$$

$$l(\hat{x} | H_1) := \ln \Lambda(\hat{x} | H_1)$$
$$= \sum_{j=1}^{N-1} \left[ \ln p(\hat{S}_j^T | H_1) - \ln p(\hat{S}_j^T | H_0) \right]$$
$$= \sum_{j=1}^{N-1} \left[ -\frac{\hat{S}_j^T}{S_s(f_j) + S_w(f_j)} + \frac{\hat{S}_j^T}{S_w(f_j)} - \ln \frac{S_w(f_j)}{S_s(f_j) + S_w(f_j)} \right]$$

# Statistics: Fisher Information

- Using likelihood ratio, calculate fisher information

$$I(\lambda) := \mathbb{E} \left[ \left( \frac{\partial}{\partial \lambda} l(\hat{x} | H_1(\lambda)) \right)^2 \middle| H_1(\lambda) \right]$$

- Then, the lower band of statistical error is given by Cramer-Rao inequality:

$$\text{Var}[\lambda] \geq \frac{1}{I(\lambda)}$$

- SNR is then defined as

$$\frac{S^2}{N^2} = \frac{\lambda^2}{1/I(\lambda)}$$

# Statistics: SNR

- In Brown motion case,  $\lambda = T_{\text{room}}$
- After some calculation we get

$$I(\lambda) = \lambda^2 \sum_{j=1}^{N-1} \left( \frac{S_s(f_j)}{S_s(f_j) + S_w(f_j)} \right)^2$$

- Around resonance peak  $S_s(f_j) \gg S_w(f_j)$ 
  - ▶  $I(\lambda) \simeq \lambda^2 \times \text{number of bins within bandwidth of resonance peak}$

$$\simeq \lambda^2 \frac{2\pi f_0 T}{Q}$$

$$\frac{S^2}{N^2} \simeq \frac{2\pi f_0 T}{Q}$$

→ SNR is proportional to  $\sqrt{T}$



# Statistics: Axion Search

- How about axion search?
- I think same procedure is applicable
- Coherent case:

$$I(\lambda) = \lambda^2 \left( \frac{S_s(f_j)}{S_s(f_j) + S_w(f_j)} \right)^2$$

- Incoherent case:

$$I(\lambda) = \lambda^2 \sum_{j=1}^{N-1} \left( \frac{S_s(f_j)}{S_s(f_j) + S_w(f_j)} \right)^2$$
$$\simeq \lambda^2 T \int_0^\infty df \left( \frac{S_s(f)}{S_s(f) + S_w(f)} \right)^2$$

- That may make our understanding further?