

Design of Phase-III TOBA

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Overview

- I would like to discuss the configuration of Phase-III TOBA for my Ph.D. thesis
- First part: comparison of the readout optical systems
- Second part: requirement of the suspension system
- I omit the introduction of TOBA because there are no M1 students

Contents

- Comparison of the readout optical systems
- Requirement of the suspension system
- Timeline for the next two years

Contents

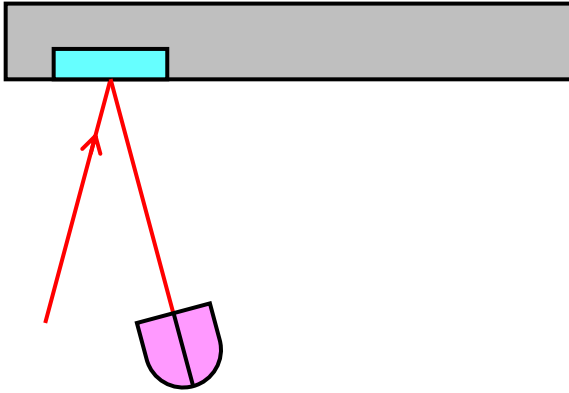
- Comparison of the readout optical systems
- Requirement of the suspension system
- Timeline for the next two years

Comparison of optical systems

- I summarized these considerations with two slides for each optical system
- We will come back to this table at the end

Unit: [rad/ $\sqrt{\text{Hz}}$]	Oplev	MI	PRMI	FPMI	QI	Cavities	WFS	CWFS, FWFS
Shot noise	2×10^{-12}	2×10^{-15}	5×10^{-16}	4×10^{-18}	2×10^{-15}	4×10^{-18}	1×10^{-11}	7×10^{-14}
Thermal noise	7×10^{-17}	1×10^{-17}	1×10^{-17}	1×10^{-17}	1×10^{-17}	1×10^{-17}	7×10^{-17}	7×10^{-17}
Seismic coupling	2×10^{-12}	2×10^{-13}	2×10^{-13}	2×10^{-13}	2×10^{-13}	2×10^{-13}	No coupling	No coupling
Numbers of optics	1	6	10	11	11 polarizing	8	5	6
PD	QPD	PD	PD, RFPD	PD, RFPD	3PD	2RFPD	RFQPD	RFQPD
Experience in Ando Lab	Shimos d-san's D	Shoda-san, Shimoda-san's M	Aritomi-san's M	Nothing	Okada-san	ANU, Takano-san's D	Nothing	Nothing

Optical lever



- Shot noise:

$$\delta\theta_{\text{shot}} = \frac{\pi w}{2L} \sqrt{\frac{\hbar c}{2\lambda P_0}} = 2 \times 10^{-12} \text{ rad}/\sqrt{\text{Hz}}$$

Beam radius at QPD: $w = 300 \mu\text{m}$

Arm length: $L = 30 \text{ cm}$

Laser wavelength: $\lambda = 1 \mu\text{m}$

Input laser power: $P_0 = 10 \text{ mW}$

- Thermal noise (mirror substrate):

$$\delta\theta_{\text{thermal}} = \sqrt{\frac{2k_B T}{\pi^{3/2} f} \frac{1 - \nu_s^2}{E_s} \frac{\phi_s}{w^3}} = 7 \times 10^{-17} \text{ rad}/\sqrt{\text{Hz}}$$

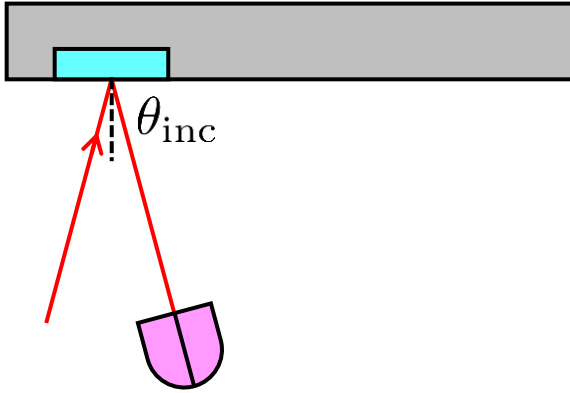
$$f = 0.1 \text{ Hz} \quad w = 100 \mu\text{m} \quad T = 4 \text{ K}$$

Substrate: fused silica Young's modulus: $E_s = 7.4 \text{ GPa}$

Poisson's ratio: $\nu_s = 0.17$

Loss angle: $\phi_s = 10^{-8}$

Optical lever



- Seismic coupling:

$$\delta\theta_{\text{seis}} = \frac{\sin \theta_{\text{inc}}}{2L} \delta x_{\text{seis}} \text{CMRR} = 2 \times 10^{-12} \text{ rad}/\sqrt{\text{Hz}}$$

Incident angle: $\theta_{\text{inc}} = 1 \text{ mrad}$

Arm length: $L = 30 \text{ cm}$

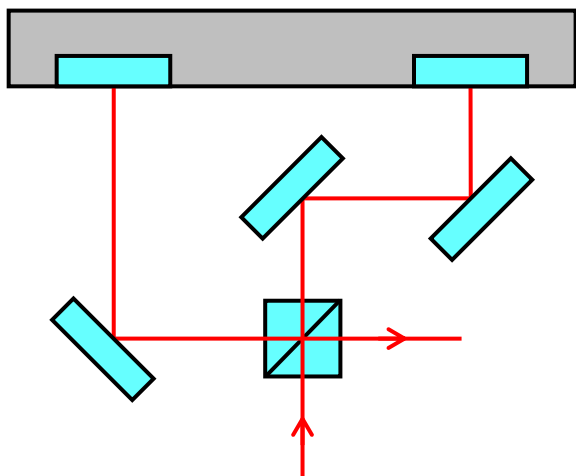
Translational seismic noise:

$$\delta x_{\text{seis}} = 10^{-7} \text{ m}/\sqrt{\text{Hz}}$$

Common mode rejection ratio
between TM and OB: $\text{CMRR} = 1/100$

- Numbers of optics: 1 mirror (only essential optics. Of course, some mirrors or BS are needed)
- PD: 1 QPD

Michelson interferometer



- Shot noise:

$$\delta\theta_{\text{shot}} = \frac{1}{2L} \sqrt{\frac{\hbar c \lambda}{\pi P_0}} = 2 \times 10^{-15} \text{ rad}/\sqrt{\text{Hz}}$$

Arm length: $L = 30 \text{ cm}$
 Laser wavelength: $\lambda = 1 \mu\text{m}$
 Input laser power: $P_0 = 10 \text{ mW}$

- Thermal noise (bar):

$$\delta\theta_{\text{thermal}} = \frac{1}{L} \sqrt{\frac{4k_B T}{\omega} \frac{\phi_{\text{bar}}}{\mu \omega_0^2}} = 1 \times 10^{-17} \text{ rad}/\sqrt{\text{Hz}}$$

$$T = 4 \text{ K} \quad \omega = 2\pi \times 0.1 \text{ Hz} \quad \phi_{\text{bar}} = 10^{-6}$$

$$\text{Frequency of second mode: } \omega_0 = 2\pi \times 10 \text{ kHz}$$

$$\text{Reduced mass of second mode: } \mu = 0.3 \text{ kg}$$

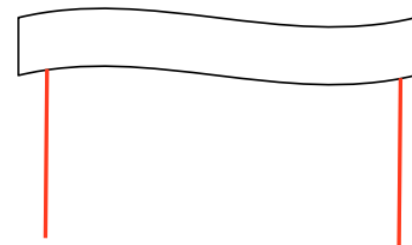
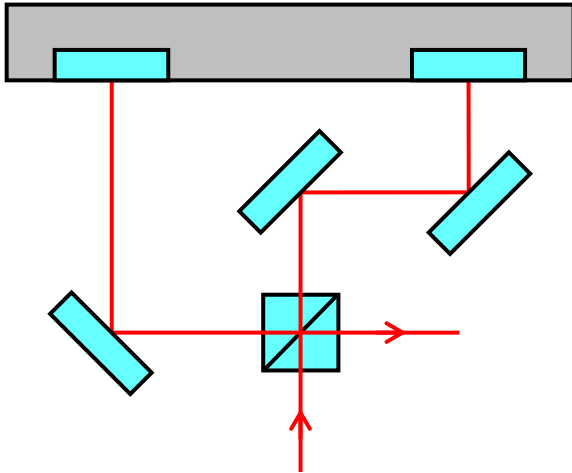


図 4.8: 試験マスの2次のモード

Aritomi-san's master thesis

Michelson interferometer



- Seismic coupling:

$$\delta\theta_{\text{seis}} = \frac{\theta_{\text{mir}}}{L} \delta x_{\text{seis}} \text{CMRR} = 2 \times 10^{-13} \text{ rad}/\sqrt{\text{Hz}}$$

Angle of two mirrors: $\theta_{\text{mir}} = 10^{-6} \text{ rad}$

Arm length: $L = 30 \text{ cm}$

Translational seismic noise:

$$\delta x_{\text{seis}} = 5 \times 10^{-6} \text{ m}/\sqrt{\text{Hz}}$$

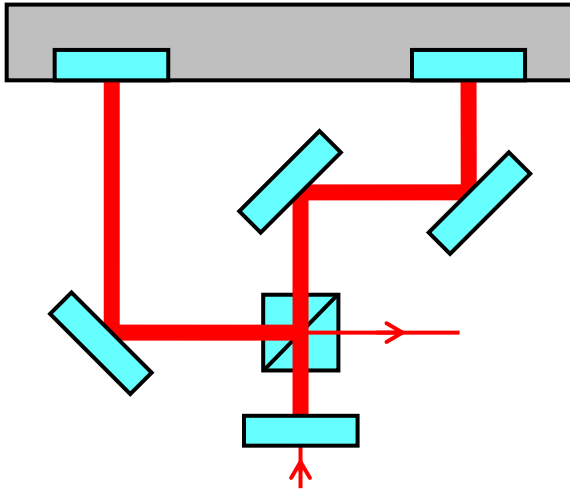
Common mode rejection ratio

between TM and OB: $\text{CMRR} = 1/100$

- Cannot meet the requirement
→ discuss in the next section

- Numbers of optics: 5 mirrors, 1 BS
- PD: 1 PD

Power recycled MI



- Shot noise:

$$\delta\theta_{\text{shot}} = \frac{1}{2L} \sqrt{\frac{\hbar c \lambda}{\pi G P_0}} = 5 \times 10^{-16} \text{ rad}/\sqrt{\text{Hz}}$$

Arm length:	$L = 30 \text{ cm}$
Laser wavelength:	$\lambda = 1 \mu\text{m}$
Input laser power:	$P_0 = 10 \text{ mW}$
Power recycle gain:	$G = 10$

- Thermal noise (bar): same as MI

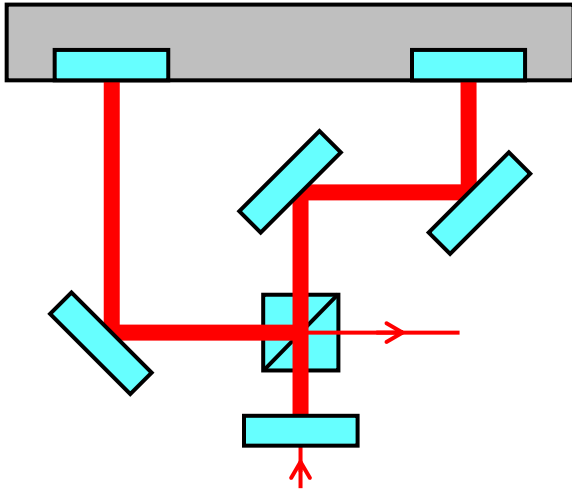
$$\delta\theta_{\text{thermal}} = \frac{1}{L} \sqrt{\frac{4k_B T}{\omega} \frac{\phi_{\text{bar}}}{\mu \omega_0^2}} = 1 \times 10^{-17} \text{ rad}/\sqrt{\text{Hz}}$$

$$T = 4 \text{ K} \quad \omega = 2\pi \times 0.1 \text{ Hz} \quad \phi_{\text{bar}} = 10^{-6}$$

$$\text{Frequency of second mode: } \omega_0 = 2\pi \times 10 \text{ kHz}$$

$$\text{Reduced mass of second mode: } \mu = 0.3 \text{ kg}$$

Power recycled MI



- Seismic coupling: same as MI

$$\delta\theta_{\text{seis}} = \frac{\theta_{\text{mir}}}{L} \delta x_{\text{seis}} \text{CMRR} = 2 \times 10^{-13} \text{ rad}/\sqrt{\text{Hz}}$$

Angle of two mirrors: $\theta_{\text{mir}} = 10^{-6} \text{ rad}$

Arm length: $L = 30 \text{ cm}$

Translational seismic noise:

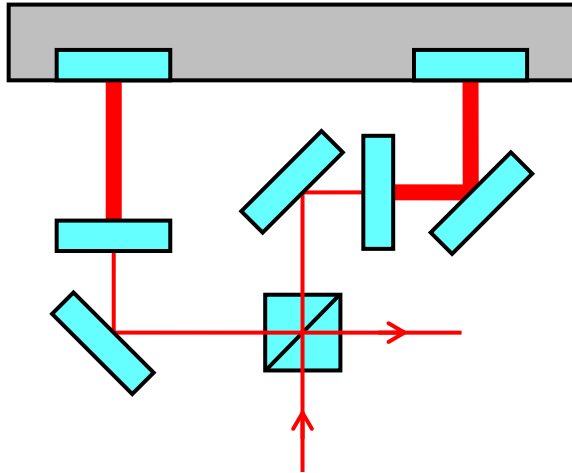
$$\delta x_{\text{seis}} = 5 \times 10^{-6} \text{ m}/\sqrt{\text{Hz}}$$

Common mode rejection ratio

between TM and OB: $\text{CMRR} = 1/100$

- Numbers of optics: 6 mirrors, 2 BS (1 for PDH), 2 lenses
- PD: 1 RFPD, 1 PD

Fabry-Pérot MI



- Shot noise:

$$\delta\theta_{\text{shot}} = \frac{t^2}{8L} \sqrt{\frac{\hbar c \lambda}{\pi P_0}} = 4 \times 10^{-18} \text{ rad}/\sqrt{\text{Hz}}$$

Arm length: $L = 30 \text{ cm}$

Laser wavelength: $\lambda = 1 \mu\text{m}$

Input laser power: $P_0 = 10 \text{ mW}$

Transmittance of front mirrors: $t^2 = 1\%$ (End: 0%)

- Thermal noise (bar): same as MI

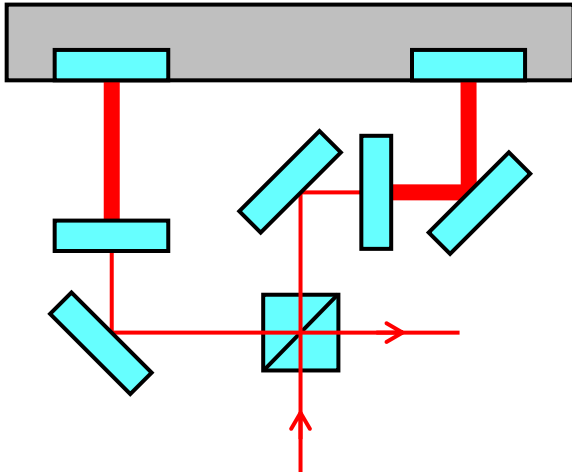
$$\delta\theta_{\text{thermal}} = \frac{1}{L} \sqrt{\frac{4k_B T}{\omega} \frac{\phi_{\text{bar}}}{\mu \omega_0^2}} = 1 \times 10^{-17} \text{ rad}/\sqrt{\text{Hz}}$$

$$T = 4 \text{ K} \quad \omega = 2\pi \times 0.1 \text{ Hz} \quad \phi_{\text{bar}} = 10^{-6}$$

Frequency of second mode: $\omega_0 = 2\pi \times 10 \text{ kHz}$

Reduced mass of second mode: $\mu = 0.3 \text{ kg}$

Fabry-Pérot MI



- Seismic coupling: same as MI

$$\delta\theta_{\text{seis}} = \frac{\theta_{\text{mir}}}{L} \delta x_{\text{seis}} \text{CMRR} = 2 \times 10^{-13} \text{ rad}/\sqrt{\text{Hz}}$$

Angle of two mirrors: $\theta_{\text{mir}} = 10^{-6} \text{ rad}$

Arm length: $L = 30 \text{ cm}$

Translational seismic noise:

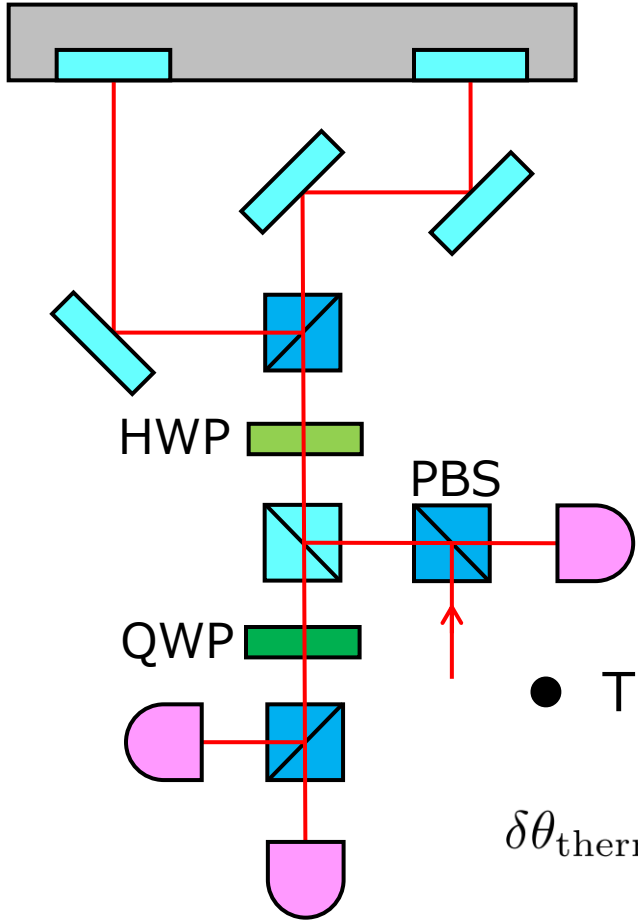
$$\delta x_{\text{seis}} = 5 \times 10^{-6} \text{ m}/\sqrt{\text{Hz}}$$

Common mode rejection ratio

between TM and OB: $\text{CMRR} = 1/100$

- Numbers of optics: 7 cavity mirrors, 2 BS, 2 lenses
- PD: 1 RFPD, 1 PD

Quadrature interferometer



- Shot noise: same as MI

$$\delta\theta_{\text{shot}} = \frac{1}{2L} \sqrt{\frac{\hbar c \lambda}{\pi P_0}} = 2 \times 10^{-15} \text{ rad}/\sqrt{\text{Hz}}$$

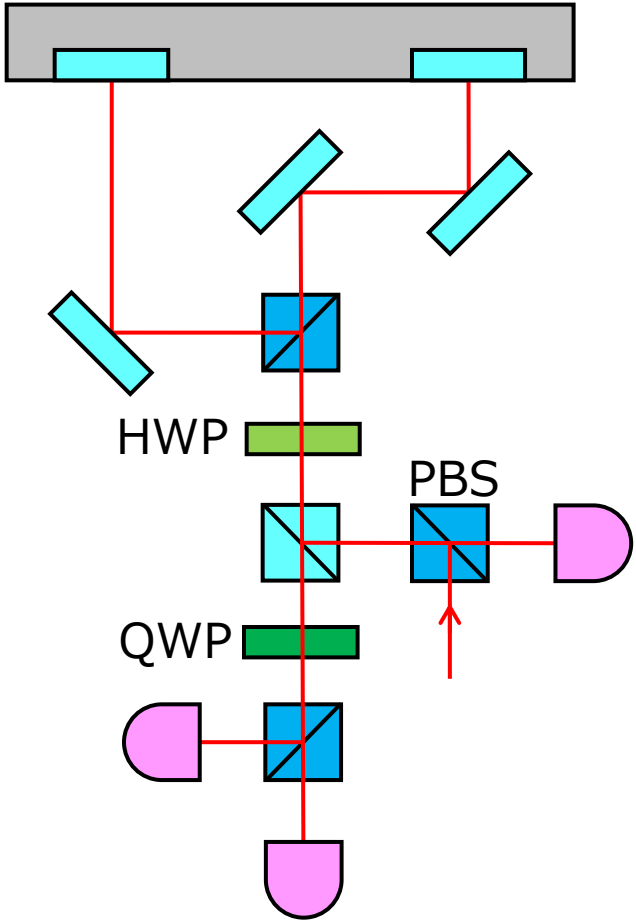
Arm length: $L = 30 \text{ cm}$
 Laser wavelength: $\lambda = 1 \mu\text{m}$
 Input laser power: $P_0 = 10 \text{ mW}$

- Thermal noise (bar): same as MI

$$\delta\theta_{\text{thermal}} = \frac{1}{L} \sqrt{\frac{4k_B T}{\omega} \frac{\phi_{\text{bar}}}{\mu \omega_0^2}} = 1 \times 10^{-17} \text{ rad}/\sqrt{\text{Hz}}$$

$T = 4 \text{ K}$ $\omega = 2\pi \times 0.1 \text{ Hz}$ $\phi_{\text{bar}} = 10^{-6}$
 Frequency of second mode: $\omega_0 = 2\pi \times 10 \text{ kHz}$
 Reduced mass of second mode: $\mu = 0.3 \text{ kg}$

Quadrature interferometer



- Seismic coupling: same as MI

$$\delta\theta_{\text{seis}} = \frac{\theta_{\text{mir}}}{L} \delta x_{\text{seis}} \text{CMRR} = 2 \times 10^{-13} \text{ rad}/\sqrt{\text{Hz}}$$

Angle of two mirrors: $\theta_{\text{mir}} = 10^{-6} \text{ rad}$

Arm length: $L = 30 \text{ cm}$

Translational seismic noise:

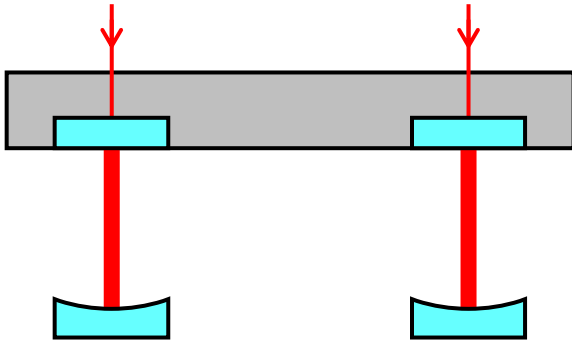
$$\delta x_{\text{seis}} = 5 \times 10^{-6} \text{ m}/\sqrt{\text{Hz}}$$

Common mode rejection ratio

between TM and OB: $\text{CMRR} = 1/100$

- Numbers of optics: 5 mirrors, 1 BS, 3 PBS, 1 QWP, 1 HWP
- PD: 3 PD

Differential Fabry–Pérot cavities



- Shot noise: same as FPMI

$$\delta\theta_{\text{shot}} = \frac{t^2}{8L} \sqrt{\frac{\hbar c \lambda}{\pi P_0}} = 4 \times 10^{-18} \text{ rad}/\sqrt{\text{Hz}}$$

Arm length: $L = 30 \text{ cm}$

Laser wavelength: $\lambda = 1 \mu\text{m}$

Input laser power: $P_0 = 10 \text{ mW}$

Transmittance of front mirrors: $t^2 = 1\%$ (End: 0%)

- Thermal noise (bar): same as MI

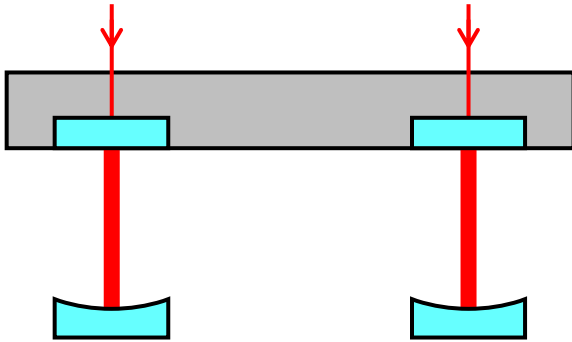
$$\delta\theta_{\text{thermal}} = \frac{1}{L} \sqrt{\frac{4k_B T}{\omega} \frac{\phi_{\text{bar}}}{\mu\omega_0^2}} = 1 \times 10^{-17} \text{ rad}/\sqrt{\text{Hz}}$$

$$T = 4 \text{ K} \quad \omega = 2\pi \times 0.1 \text{ Hz} \quad \phi_{\text{bar}} = 10^{-6}$$

Frequency of second mode: $\omega_0 = 2\pi \times 10 \text{ kHz}$

Reduced mass of second mode: $\mu = 0.3 \text{ kg}$

Differential Fabry–Pérot cavities



- Seismic coupling: same as MI

$$\delta\theta_{\text{seis}} = \frac{\theta_{\text{mir}}}{L} \delta x_{\text{seis}} \text{CMRR} = 2 \times 10^{-13} \text{ rad}/\sqrt{\text{Hz}}$$

Angle of two mirrors: $\theta_{\text{mir}} = 10^{-6} \text{ rad}$

Arm length: $L = 30 \text{ cm}$

Translational seismic noise:

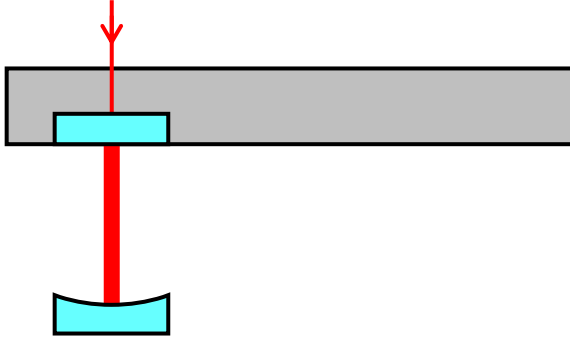
$$\delta x_{\text{seis}} = 5 \times 10^{-6} \text{ m}/\sqrt{\text{Hz}}$$

Common mode rejection ratio

between TM and OB: $\text{CMRR} = 1/100$

- Numbers of optics: 4 mirrors, 2 BS, 2 lenses
- PD: 2 RFPD

Wavefront sensor



- Shot noise:

$$\delta\theta_{\text{shot}} = \frac{1}{8J_0J_1w} \sqrt{\frac{2\hbar c\lambda}{P_0}} = 1 \times 10^{-11} \text{ rad}/\sqrt{\text{Hz}}$$

$$J_0 = 1 \quad J_1 = 0.05$$

$$\text{Beam radius:} \quad w = 300 \mu\text{m}$$

$$\text{Laser wavelength:} \quad \lambda = 1 \mu\text{m}$$

$$\text{Input laser power:} \quad P_0 = 10 \text{ mW}$$

- Thermal noise (mirror substrate): same as oplev

$$\delta\theta_{\text{thermal}} = \sqrt{\frac{2k_B T}{\pi^{3/2} f} \frac{1 - \nu_s^2}{E_s} \frac{\phi_s}{w^3}} = 7 \times 10^{-17} \text{ rad}/\sqrt{\text{Hz}}$$

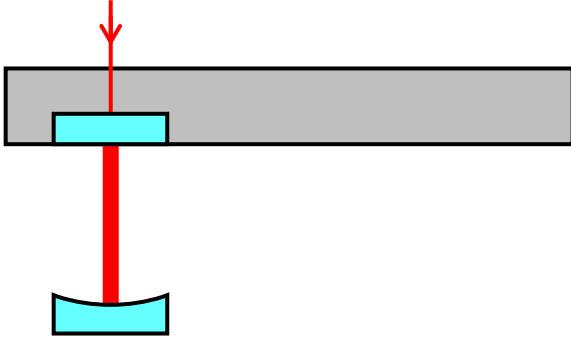
$$f = 0.1 \text{ Hz} \quad w = 100 \mu\text{m} \quad T = 4 \text{ K}$$

$$\text{Substrate: fused silica} \quad \text{Young's modulus: } E_s = 7.4 \text{ GPa}$$

$$\text{Poisson's ratio: } \nu_s = 0.17$$

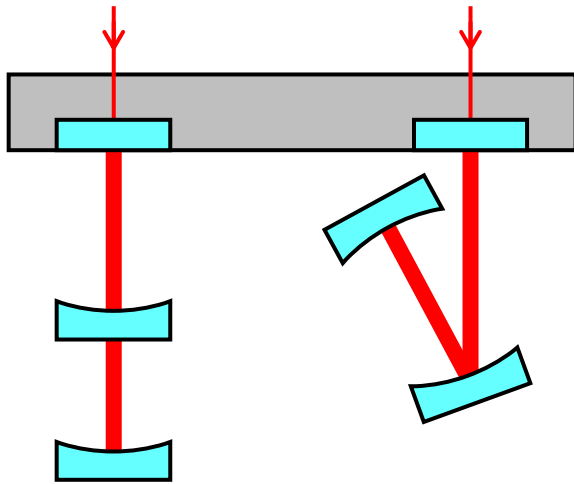
$$\text{Loss angle: } \phi_s = 10^{-8}$$

Wavefront sensor



- Seismic coupling:
 - In principle, no coupling by using a flat mirror and sufficient PDH (length) control
 - Non-linear coupling?
- Numbers of optics: 2 cavity mirrors, 1 BS, 2 lenses
- PD: 1 RFQPD

Coupled or Folded WFS



- Shot noise:

$$\delta\theta_{\text{shot}} = \frac{1}{8J_0J_1\mathcal{F}w} \sqrt{\frac{2\hbar c\lambda}{P_0}} = 7 \times 10^{-14} \text{ rad}/\sqrt{\text{Hz}}$$

$$J_0 = 1 \quad J_1 = 0.05$$

$$\text{Beam radius:} \quad w = 300 \mu\text{m}$$

$$\text{Laser wavelength:} \quad \lambda = 1 \mu\text{m}$$

$$\text{Input laser power:} \quad P_0 = 10 \text{ mW}$$

$$\text{Finesse:} \quad \mathcal{F} = 300$$

- Thermal noise (mirror substrate): same as oplev

$$\delta\theta_{\text{thermal}} = \sqrt{\frac{2k_B T}{\pi^{3/2} f} \frac{1 - \nu_s^2}{E_s} \frac{\phi_s}{w^3}} = 7 \times 10^{-17} \text{ rad}/\sqrt{\text{Hz}}$$

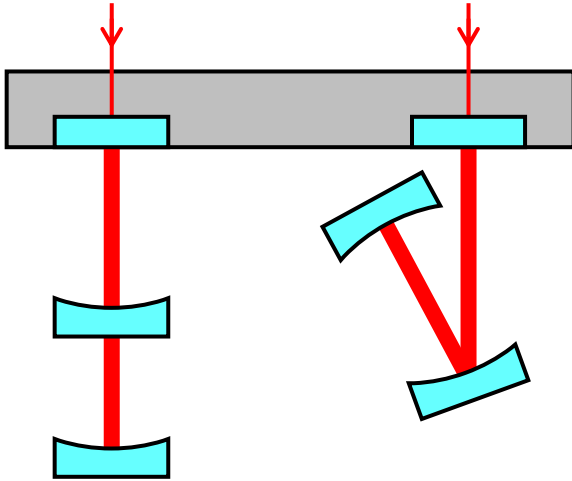
$$f = 0.1 \text{ Hz} \quad w = 100 \mu\text{m} \quad T = 4 \text{ K}$$

$$\text{Substrate: fused silica} \quad \text{Young's modulus: } E_s = 7.4 \text{ GPa}$$

$$\text{Poisson's ratio: } \nu_s = 0.17$$

$$\text{Loss angle: } \phi_s = 10^{-8}$$

Coupled or Folded WFS



- Seismic coupling:
 - In principle, no coupling by using a flat mirror and sufficient PDH (length) control
 - Non-linear coupling?
- Numbers of optics: 3 cavity mirrors, 1 BS, 2 lenses
- PD: 1 RFQPD

Comparison of optical systems

- Oplev, WFS, CWFS cannot meet the shot noise requirement
- WFS cannot meet even with KAGRA parameter [Aso+ \(2013\)](#)
- CWFS will meet with large beam and high finesse

Unit: [rad/ $\sqrt{\text{Hz}}$]	Oplev	MI	PRMI	FPMI	QI	Cavities	WFS	CWFS, FWFS
Shot noise	2×10^{-12}	2×10^{-15}	5×10^{-16}	4×10^{-18}	2×10^{-15}	4×10^{-18}	1×10^{-11}	7×10^{-14}
Thermal noise	7×10^{-17}	1×10^{-17}	1×10^{-17}	1×10^{-17}	1×10^{-17}	1×10^{-17}	7×10^{-17}	7×10^{-17}
Seismic coupling	2×10^{-12}	2×10^{-13}	2×10^{-13}	2×10^{-13}	2×10^{-13}	2×10^{-13}	No coupling	No coupling
Numbers of optics	1	6	10	11	11 polarizing	8	5	6
PD	QPD	PD	PD, RFPD	PD, RFPD	3PD	2RFPD	RFQPD	RFQPD
Experience in Ando Lab	Shimos d-san's D	Shoda-san, Shimoda-san's M	Aritomi-san's M	Nothing	Okada-san	ANU, Takano-san's D	Nothing	Nothing

Comparison of optical systems

- I give them rough scores to make the ranking
- Michelson interferometer: very simple
- Two cavities: sensitive and quite simple

Unit: [rad/ $\sqrt{\text{Hz}}$]	MI	PRMI	FPMI	QI	Cavities
Shot noise	2×10^{-15} 1	5×10^{-16} 2	4×10^{-18} 3	2×10^{-15} 1	4×10^{-18} 3
Thermal noise	1×10^{-17}	1×10^{-17}	1×10^{-17}	1×10^{-17}	1×10^{-17}
Seismic coupling	2×10^{-12}	2×10^{-13}	2×10^{-13}	2×10^{-13}	2×10^{-13}
Numbers of optics	6 5	10 3	11 2	11 polarizing 1	8 4
PD	PD 3	PD, RFPP 2	PD, RFPP 2	3PD 2	2RFPD 1
Experience in Ando Lab	Shoda-san, Shimoda-san's M 3	Aritomi-san's M 2	Nothing 1	Okada-san 2	ANU, Takano-san's D 3

12

9

8

6

11

My concerning points

- MI is simple, easy to operate and sensitive, so it makes sense that it has been used in many exp. so far
- Most sensitive exp.: MINT?
 2×10^{-10} rad/ $\sqrt{\text{Hz}}$ at 0.2-30 Hz at room temp.

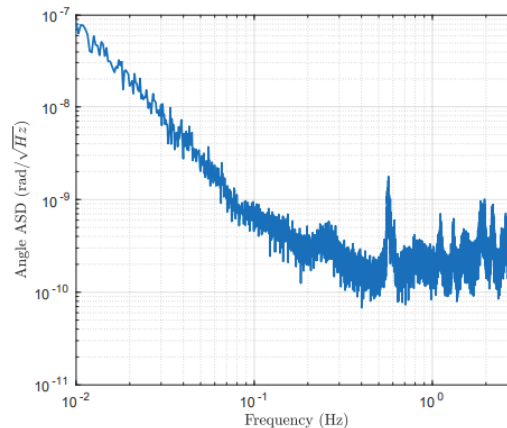


FIG. 7: Amplitude spectral density of the inertial angular noise.

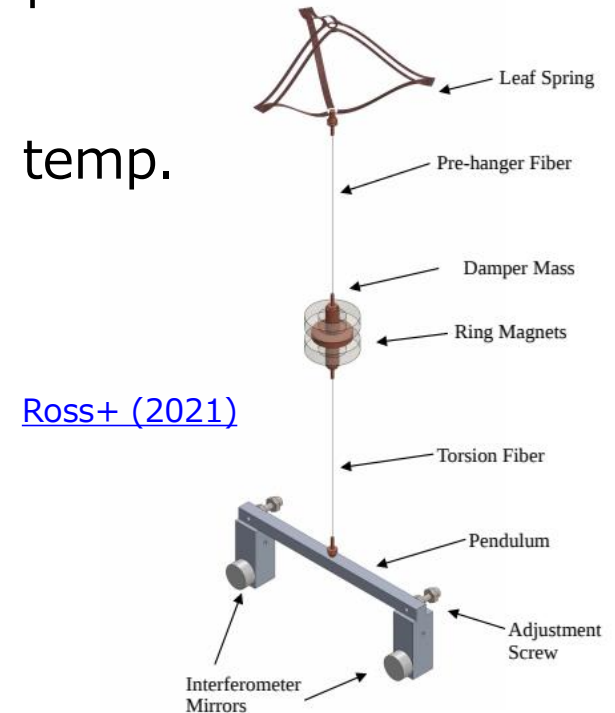


FIG. 2: CAD rendering of the MINT pendulum and eddy current damper assembly.

- Is MI not impactful enough for Ph.D.?
Difficult if not the highest sensitivity in the world?
- Is it first in the world to build a torsion pendulum with cryo. temp. and two cavities to readout angles?

Contents

- Comparison of the readout optical systems
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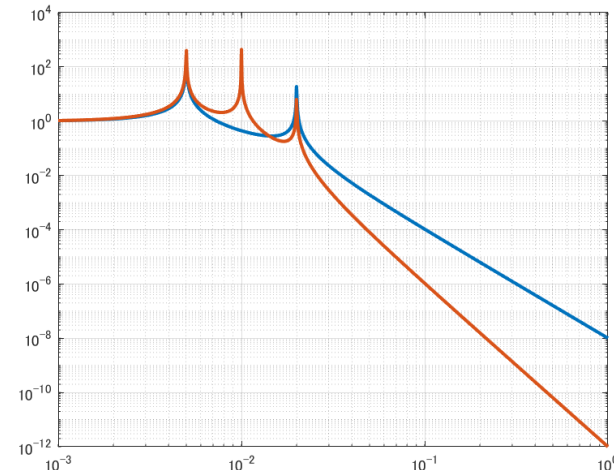
Two kinds of seismic noise

- We should take into account of two kinds of seismic noise to design TOBA's suspension
- Rotational seismic noise
 - Assuming 10^{-9} rad/ $\sqrt{\text{Hz}}$ at 0.1 Hz
 - Need to be isolated to 10^{-15} rad/ $\sqrt{\text{Hz}}$
(= reduce 6 orders of magnitude)
- Translational seismic noise
 - 5×10^{-6} m/ $\sqrt{\text{Hz}}$ at 0.1 Hz
 - Need to reduce the coupling (transfer function) to $< 10^{-10}$ rad/m

Rotational seismic noise

- Requirement: reduce 6 orders of magnitude
- Multi-stage torsion pendulum can isolate torsional seismic noise
- 3-stage pendulum: 6 orders of magnitude (enough)
- 2-stage pendulum: 4 orders of magnitude
 - Isolate with CMRR for two more orders of magnitude
 - CMRR = 1/100
 - Match resonant freq. of TM and OB with the accuracy of 0.5%
 - Moment of inertia 1% (10 g scale)

$$\text{CMRR} \sim \frac{2\Delta f}{f_{\text{yaw}}} \quad f_{\text{yaw}} = \frac{1}{2\pi} \sqrt{\frac{\pi E d^4}{64l(1 + \nu)I}}$$



Translational seismic noise (1)

- Requirement: coupling $< 10^{-10}$ rad/m
- Coupling path 1: tilt of the two mirrors



$$\delta\theta_{\text{seis}} = \frac{\theta_{\text{mir}}}{L} \delta x_{\text{seis}} \text{CMRR} = 2 \times 10^{-13} \text{ rad}/\sqrt{\text{Hz}}$$

Angle of two mirrors: $\theta_{\text{mir}} = 10^{-6}$ rad

Arm length: $L = 30$ cm

Translational seismic noise:

$$\delta x_{\text{seis}} = 5 \times 10^{-6} \text{ m}/\sqrt{\text{Hz}}$$

Common mode rejection ratio

between TM and OB: $\text{CMRR} = 1/100$



Requirement: $\text{CMRR} < 10^{-4}$



Match the distance from the clamping point to the center of gravity for TM and OB with an accuracy of 1 mm

Translational seismic noise (2)

- Requirement: coupling $< 10^{-10}$ rad/m
- Coupling path 2: shift of center of gravity and suspension point

Requirement: $\Delta\phi_P < 2.5 \times 10^{-9}$

(Shimoda-san's M thesis)

- How to reduce
 - Counter-weight
 - Actuate
 - But feasibility is not clear...

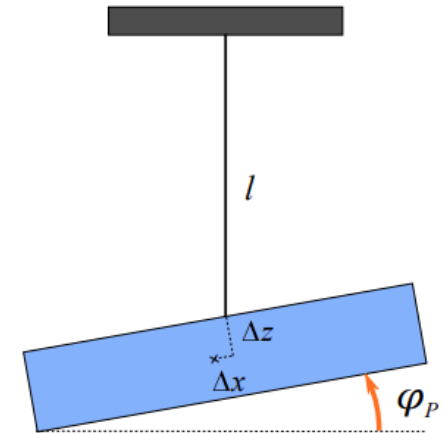
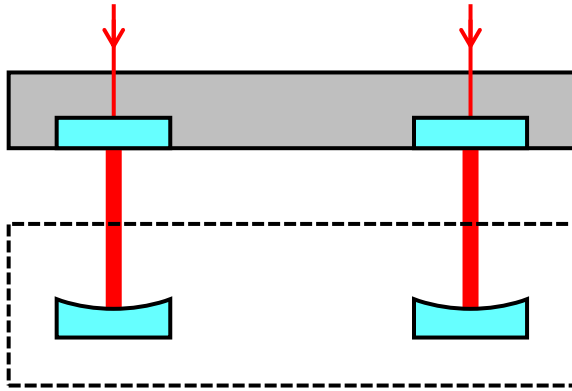
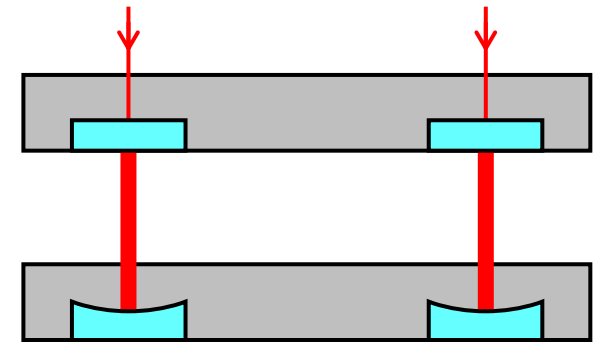
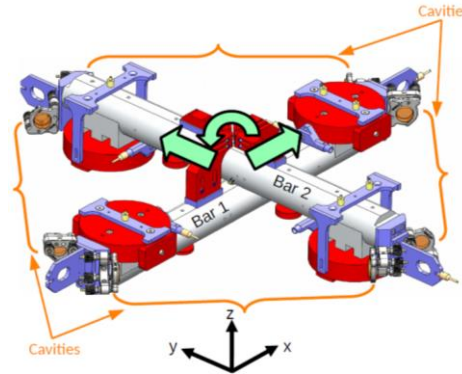


図 4.6: 重心と懸架点のズレ

Two cavities: optical bench



Reference:
optical bench or another test mass?

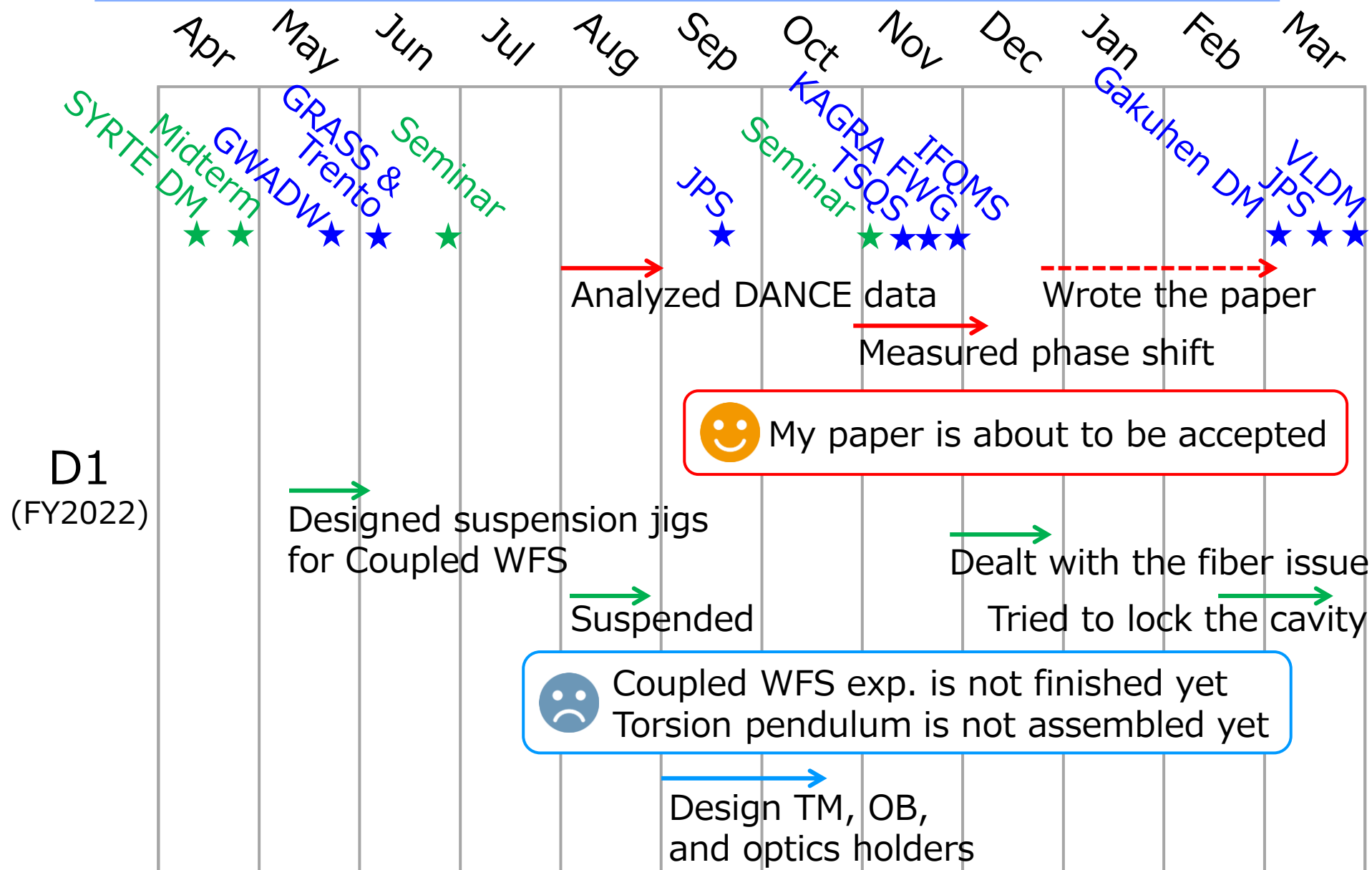


	Optical bench	Another test mass
Experience in Ando Lab	Many (All TOBA)	Few (Ono-kun's M, Komori-san's D?)
Common mode rejection	Difficult because test masses are different	Easier because the same two suspension

Contents

- Comparison of the readout optical systems
- Requirement of the suspension system
- **Timeline for the next two years**

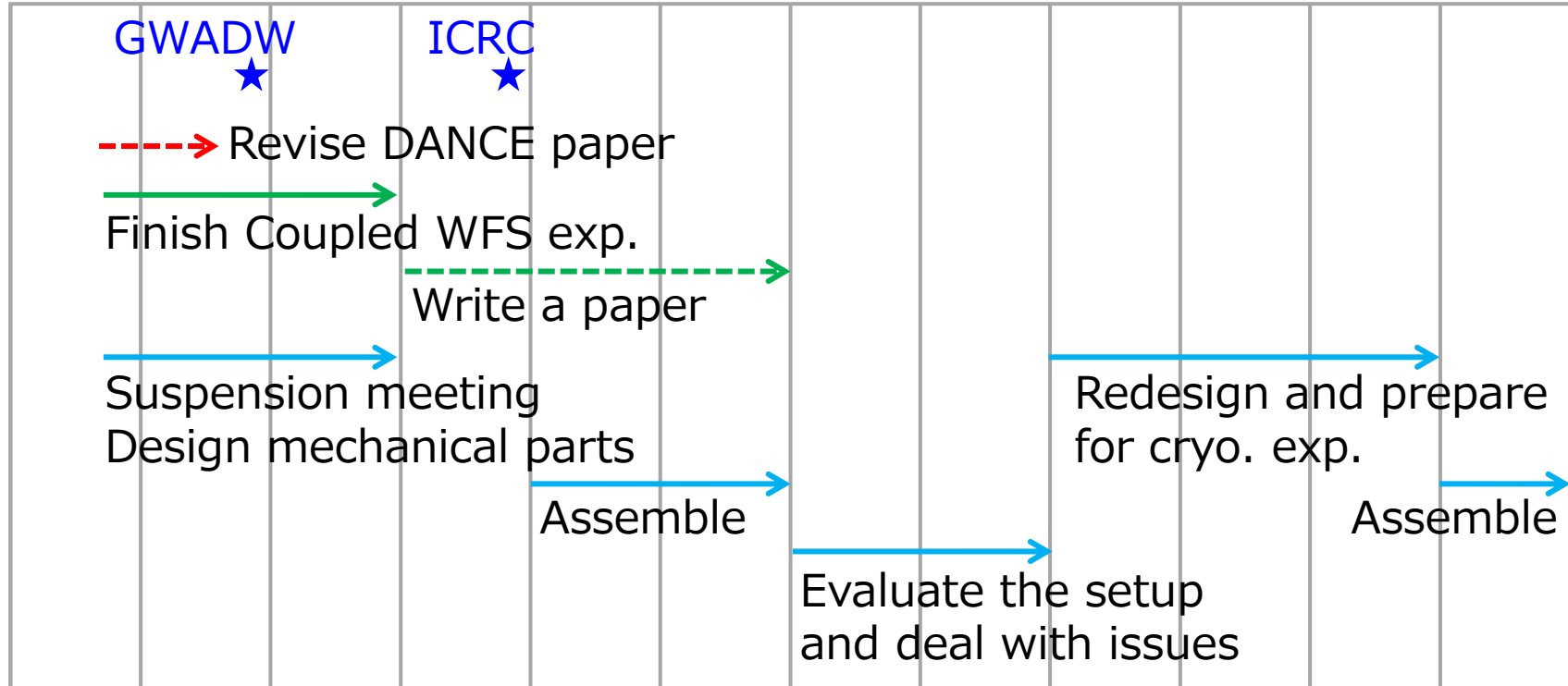
Reflections on FY2022



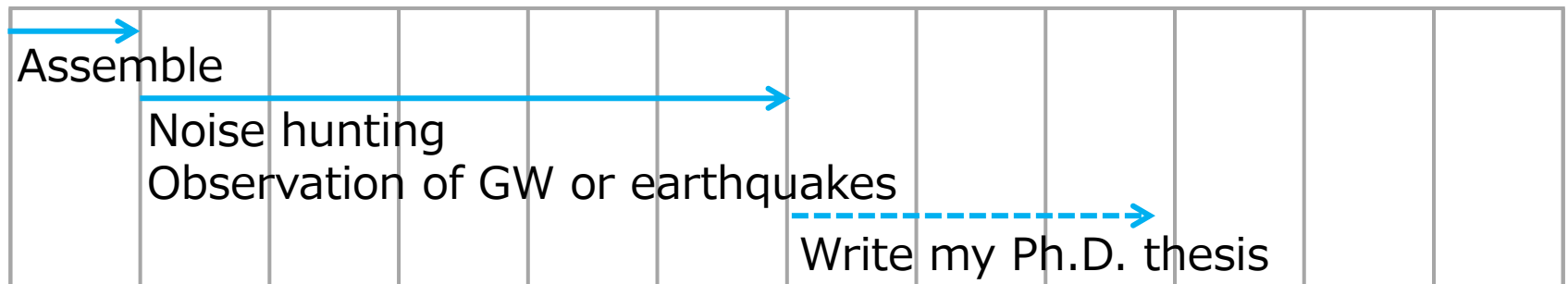
Plans of the next two years

Apr May Jun Jul Aug Sep Oct Nov Dec Jan Feb Mar

D2
(FY2023)



D3
(FY2024)



Summary

- Comparison of the readout optical systems
 - MI is quite simple, but two cavities are suitable for my Ph.D.?
- Requirement of the suspension system
- Timeline for the next two years
 - I should start the engine to finish the experiment in a year and a half

また1年間よろしくお願ひします

