

# Current status and future plans of LSRC, optomechanics, and B-L dark matter experiments

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Mid-term report 2023/04/24

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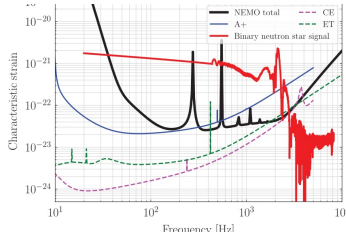
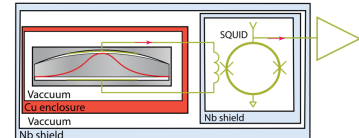
- Long SRC

- Sub contents

- Optomechanical torsion pendulum
- B-L dark matter

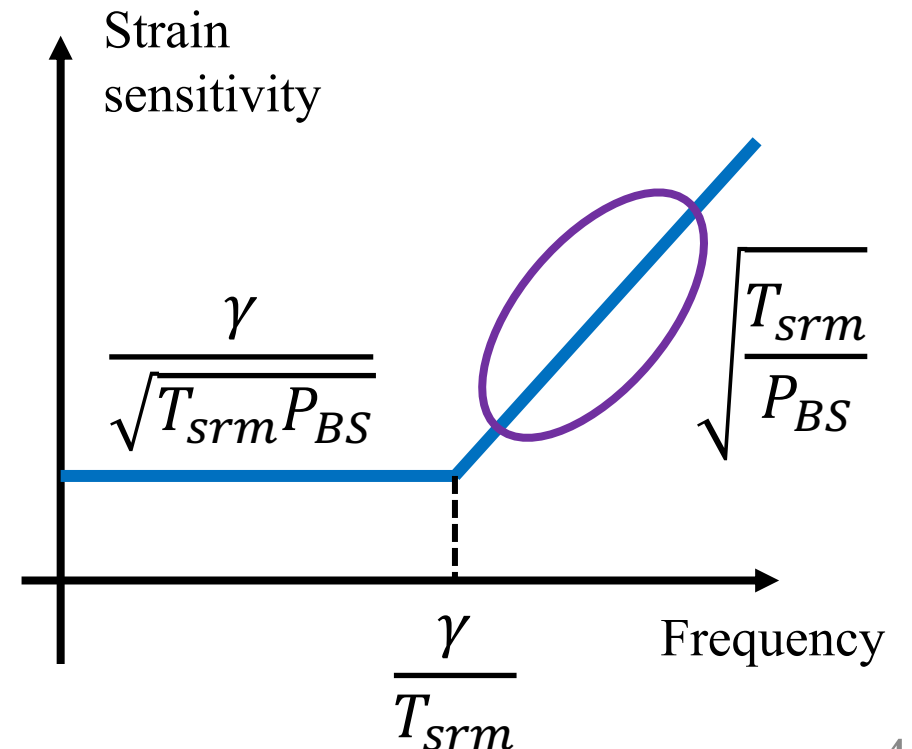
# Motivation

## ➤ High frequency GWs

Frequency	~kHz	Above kHz
Science	<ul style="list-style-type: none"> <li>Equation of state of NS</li> <li>Sky localization</li> <li>Pulsar ellipticity</li> <li>Harmonics of BBH ringdown</li> </ul>	<ul style="list-style-type: none"> <li>Merger of primordial BHs</li> <li>BH superradiance</li> <li>Phase transition in the early Universe</li> </ul>
Detector	Conventional large detector <ul style="list-style-type: none"> <li>NEMO</li> <li>LIGO-HF</li> <li>KAGRA-HF</li> </ul> 	New-type <ul style="list-style-type: none"> <li>Levitated sensors</li> <li>Bulk acoustic wave</li> <li>Interferometer</li> </ul> 

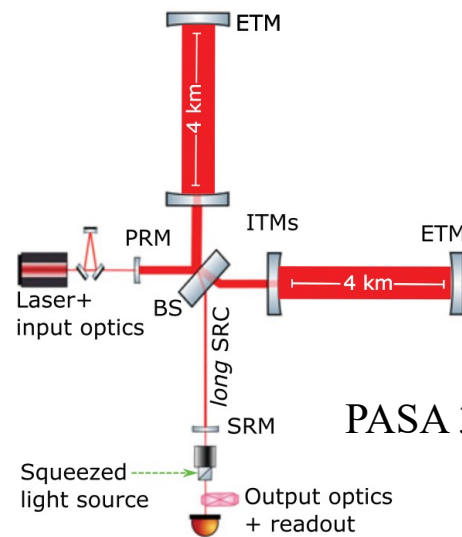
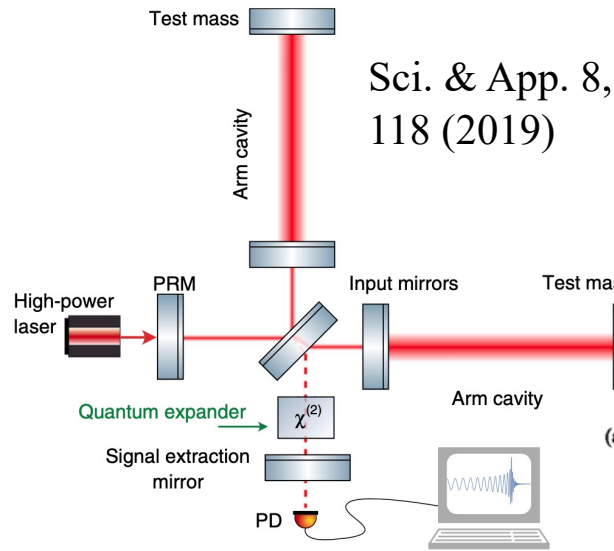
# Advantages of HF measurement

- Only shot noise, no displacement noises
  - Simple suspension is accepted
  - No couplings from other degrees of freedom
- Good sensitivity even with shorter arms
  - Longer arm and higher finesse (lower arm cavity pole) are better for the bucket sensitivity
  - It is hard to achieve good sensitivities above the bandwidth of the interferometer
  - Shorter interferometers can achieve better sensitivity than longer ones

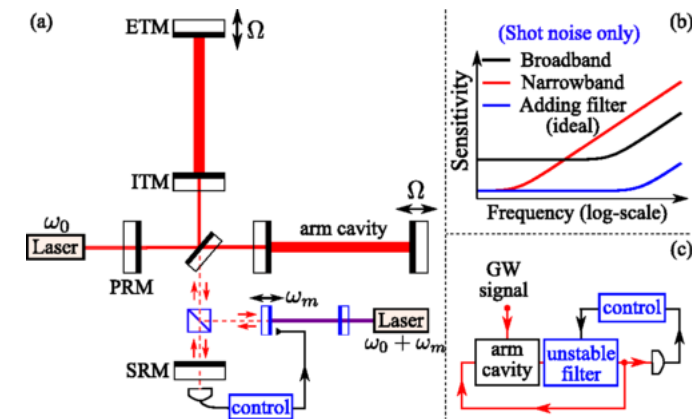


# Method

- Quantum expander
  - Nonlinear crystal in SRC
  
- Unstable optomechanical filter
  - Low-temperature high-Q mechanical oscillator
  
- Long signal recycling cavity
  - Another space for the long cavity



PRL 115, 211104 (2015)



# Sensitivity calculation

PRD 64, 042006 (2001) “BC paper”    PRD 65, 022002 (2001) “KLMTV paper”

## ➤ Quantum noise

$$S_h = \frac{h_{SQL}^2}{2} \left( \mathcal{K} + \frac{1}{\mathcal{K}} \right)$$

Radiation pressure noise

$$S_{h,shot} = \frac{h_{SQL}^2}{2\mathcal{K}}$$

$$\mathcal{K} = \left( \frac{\omega_{SQL}}{\omega} \right)^2 K(\omega)$$

$h_{SQL}^2$ : SQL sensitivity

Conventional

$$\frac{1}{K(\omega)} = 1 + \frac{(1-r)^2}{(1+r)^2 \gamma^2} \omega^2 \quad (L_{src} \rightarrow 0)$$

SRM amplitude reflectivity

Arm cavity line width

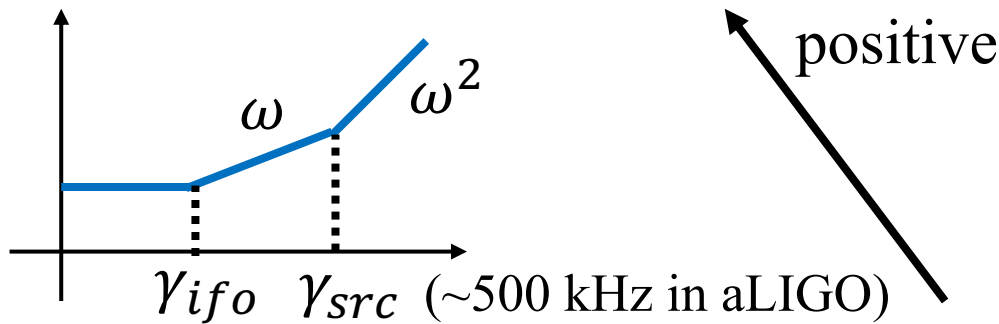
Non-zero  
SRC length

$$\frac{1}{K(\omega)} = 1 + \frac{(1-r)^2 - 8rL_{src}\gamma/c}{(1+r)^2 \gamma^2} \omega^2 + \frac{4rL_{src}^2/c^2}{(1+r)^2 \gamma^2} \omega^4$$

# Amplitude sensitivity

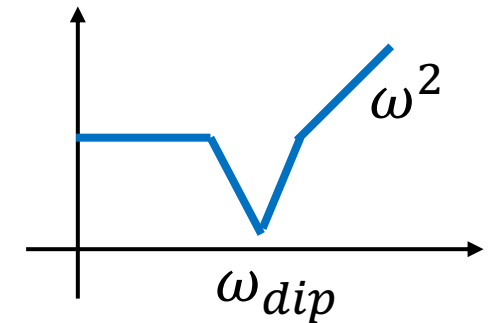
## ➤ Short SRC

- $\omega < \gamma_{ifo}$ : flat
- $\gamma_{ifo} < \omega < \gamma_{src}$ :  $\sqrt{S_h} \propto \omega$
- $\gamma_{src} < \omega$ :  $\sqrt{S_h} \propto \omega^2$   
(through two cavities)

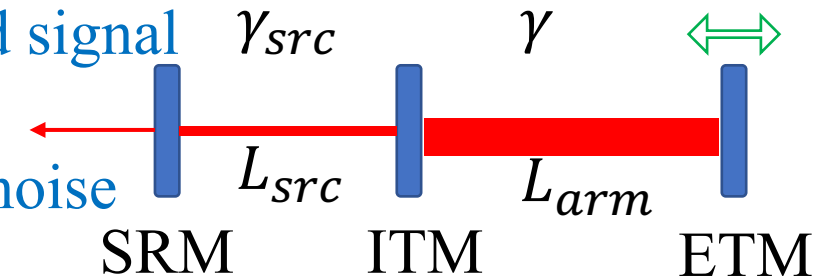


## ➤ Long SRC

- $\omega < \omega_{dip}$ : flat
- $\omega_{dip} < \omega$ :  $\sqrt{S_h} \propto \omega^2$



Enhanced signal  
v.s.  
flat shot noise



Non-zero  
SRC length

$$\frac{1}{K(\omega)} = 1 + \frac{(1-r)^2 - 8rL_{src}\gamma/c}{(1+r)^2\gamma^2} \omega^2 + \frac{4rL_{src}^2/c^2}{(1+r)^2\gamma^2} \omega^4$$

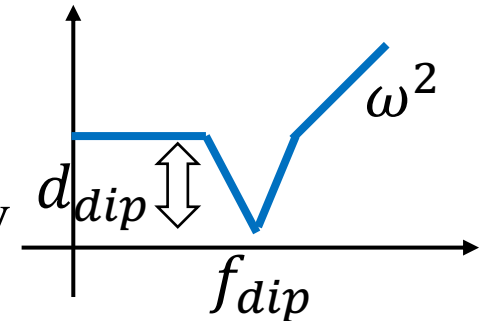
# Dip in the sensitivity

➤ The negative  $\omega^2$  term causes the dip when  $L_{src} > T_{srm}^2 L_{arm} / (8T_i)$

Dip frequency:  $f_{dip} = \frac{c}{8\pi} \sqrt{\frac{T_i}{L_{arm} L_{src}}}$      $\sim$ kHz with km-scale arm  
 $\sim$ MHz at table-top scale

Depth:  $d_{dip} = \frac{T_{srm}}{2} \sqrt{\frac{L_{arm}}{T_i L_{src}}}$

$T_{srm}$ : SRM transmissivity  
 $T_i$ : ITM transmissivity  
 $L_{arm}$ : Arm length  
 $L_{src}$ : SRC length



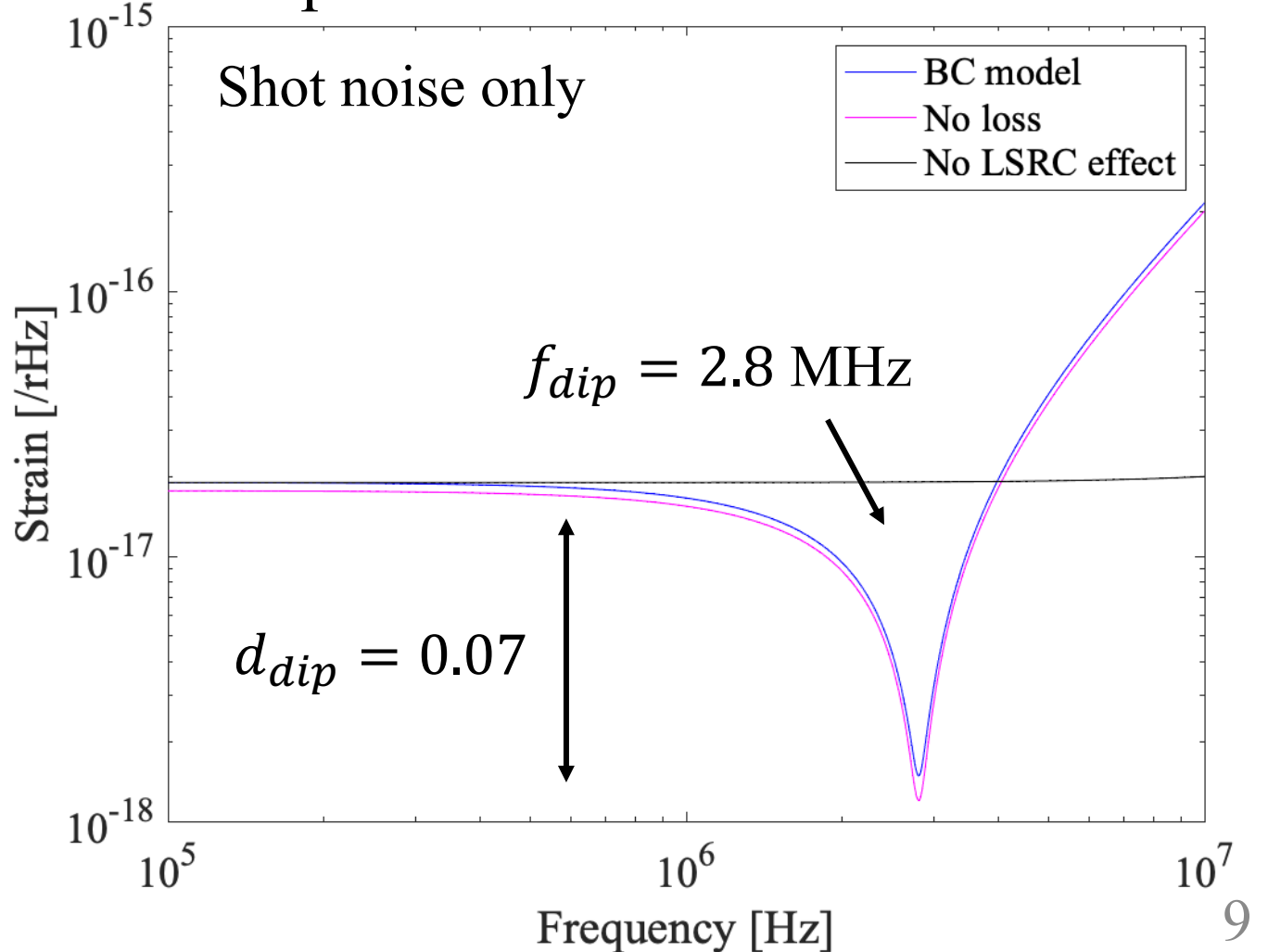
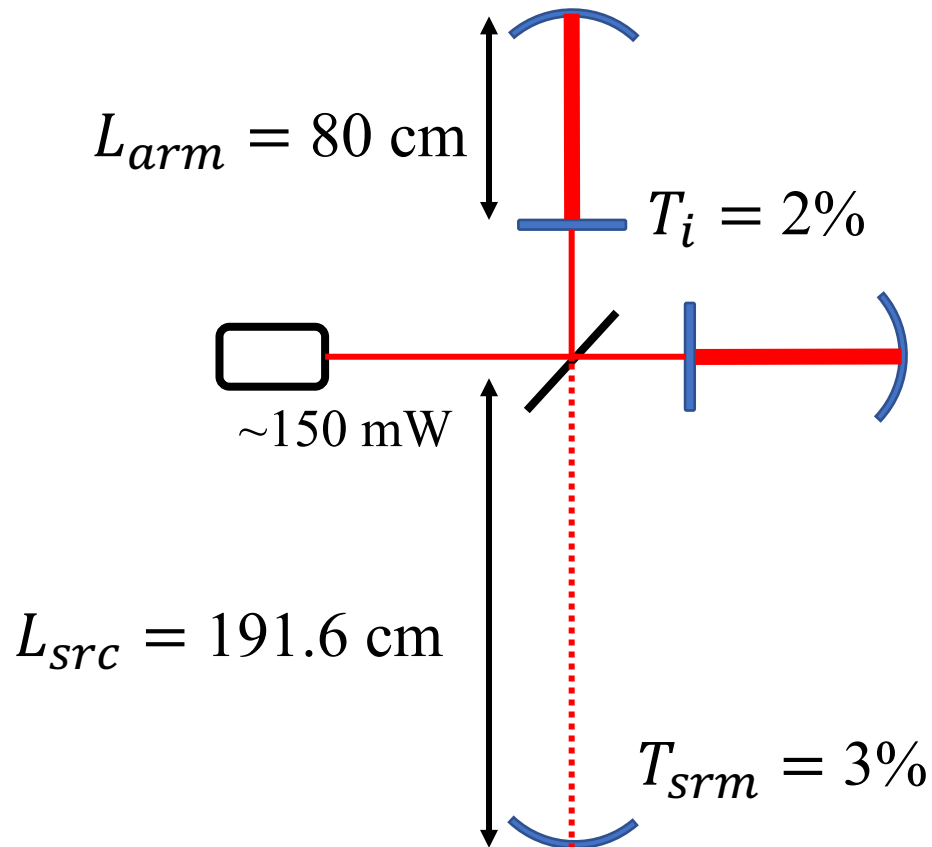
Non-zero  
SRC length

$$\frac{1}{K(\omega)} = 1 + \frac{(1-r)^2 - 8rL_{src}\gamma/c}{(1+r)^2\gamma^2} \omega^2 + \frac{4rL_{src}^2/c^2}{(1+r)^2\gamma^2} \omega^4$$

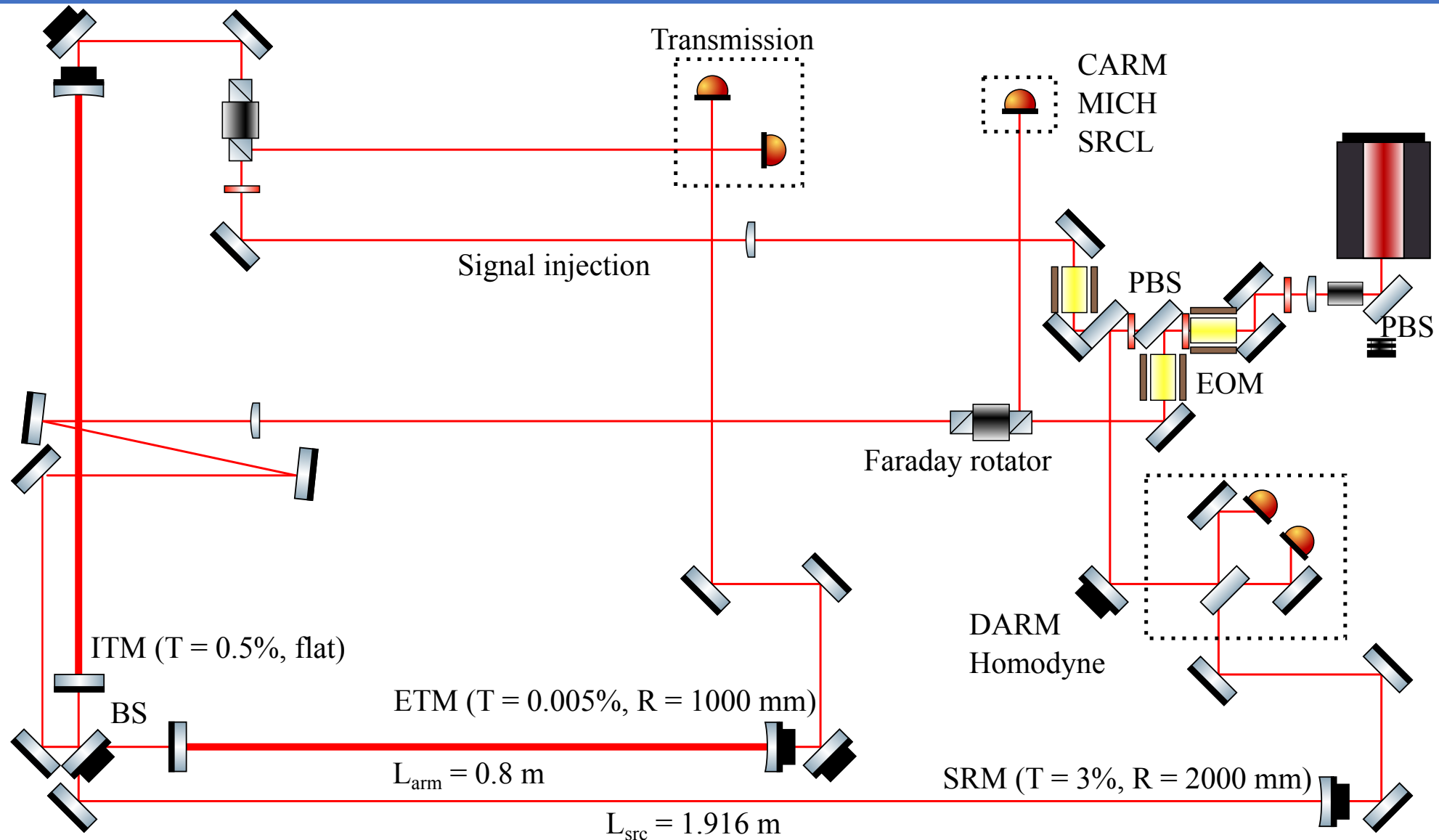


# Experimental plan

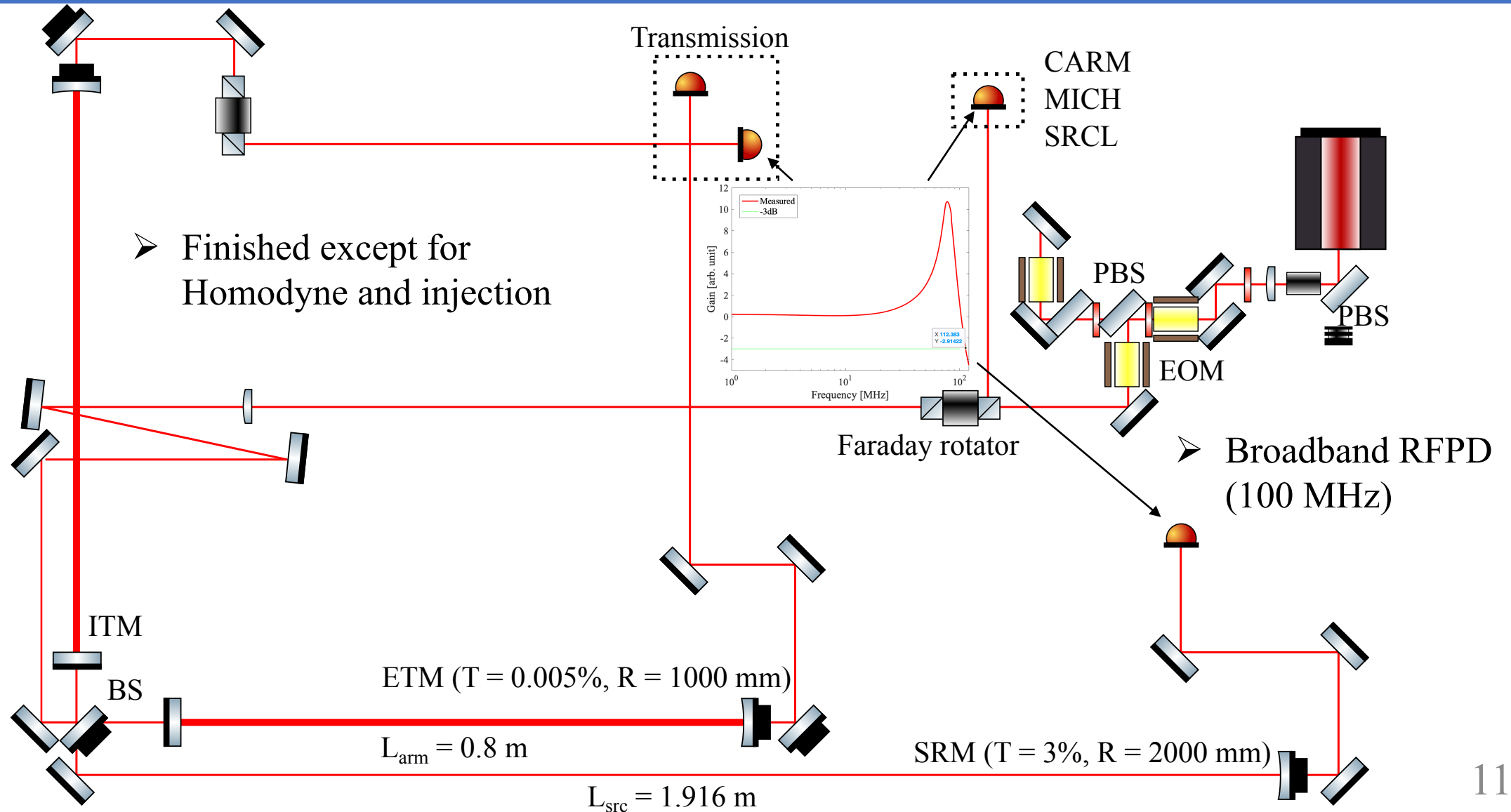
➤ Demonstration of LSRC at the table-top scale with SRFPMI



# Optical layout



# Current status



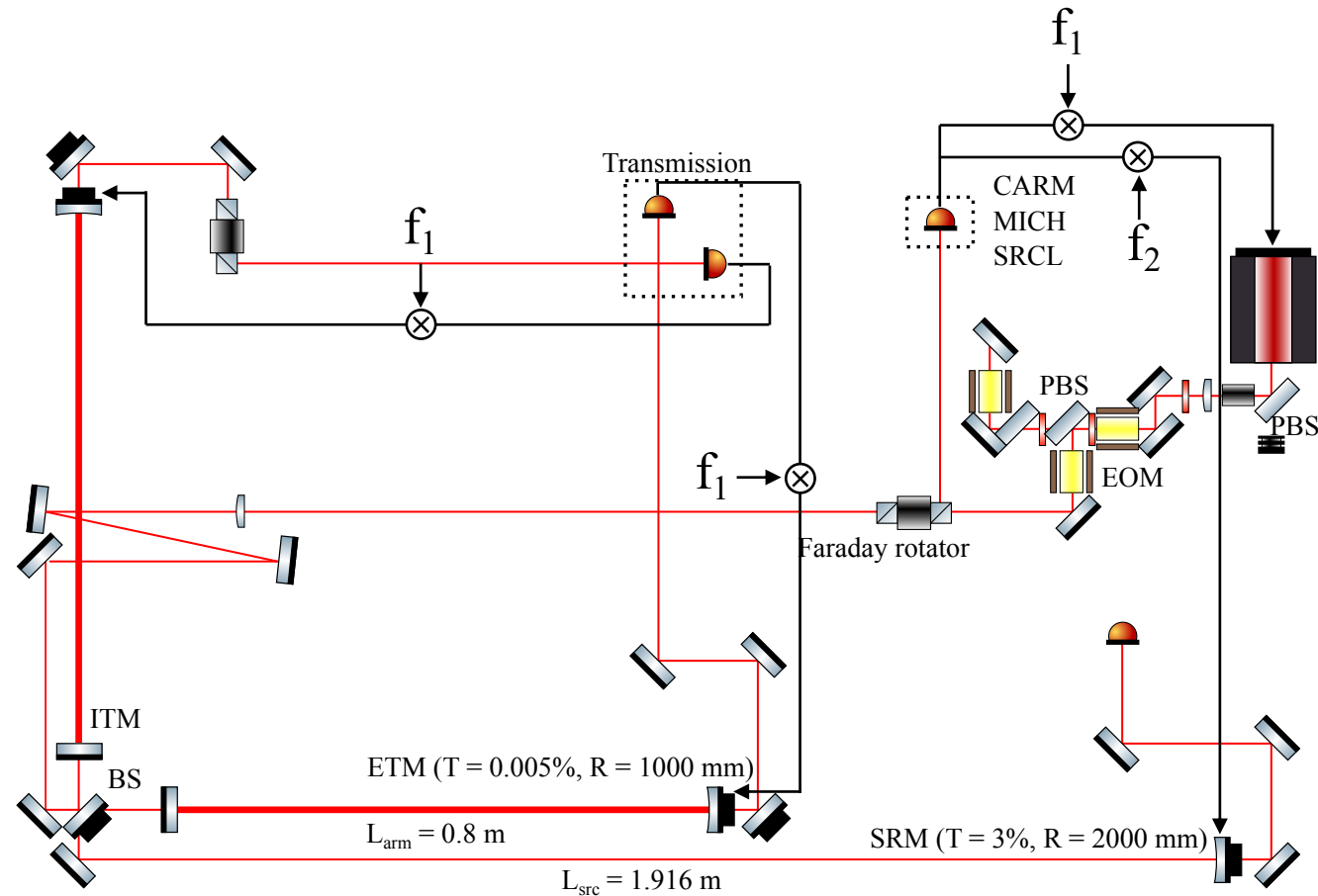
# Length sensing and control (old)

## ➤ FPMI

- Each arm: transmission PDH
- Another method: CARM (DARM) control by frequency (one ETM) feedback
- MICH: Q-phase, though very stable even without control

## ➤ SRMI

- Second sideband  $\sim 80$  MHz (2-m SRC FSR)



# Current issue

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- Not succeeded in RSE yet, two issues
- Lock acquisition
  - Rarely succeeding in the FPMI lock with SRM aligned due to career reflection
- Noise
  - RMS of relative transmission fluctuation  $\sim 0.1$ , corresponding to the detuning fluctuation  $\sim 0.3$  cavity line width
  - Enhanced by the SRM reflection, more noisy

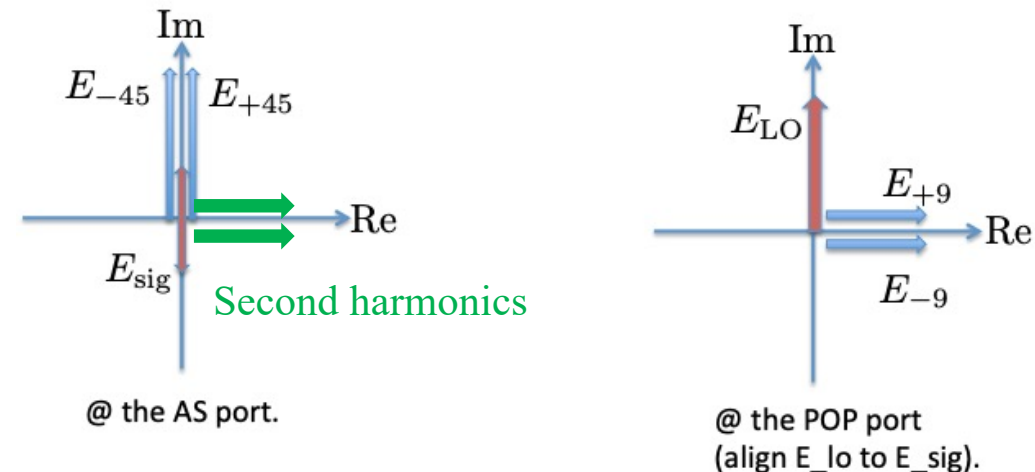
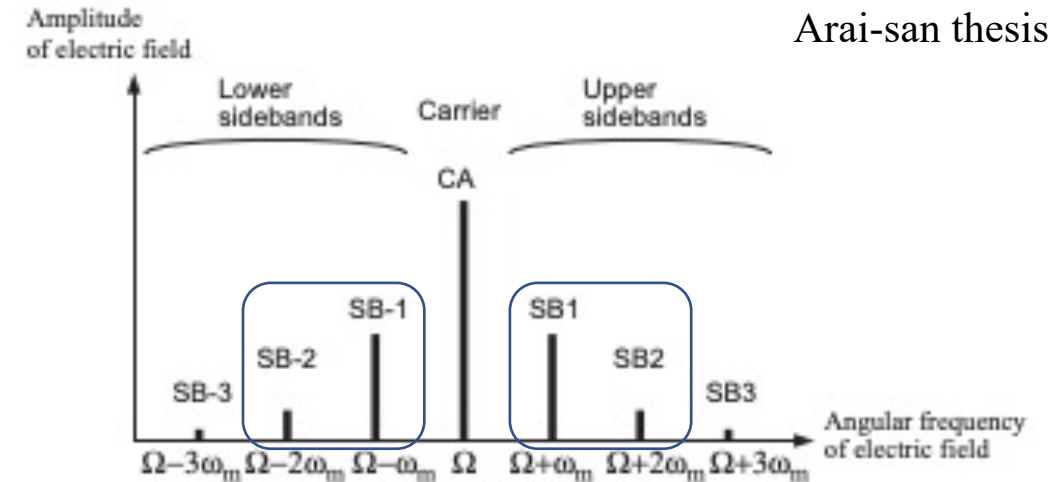
# How to solve

## ➤ Lock acquisition

- SRC control by the **third harmonic demodulation**
- Beating of 40 MHz and 80 MHz resonating in the SRC
- **Career free control** to keep the SRMI lock during the FPMI lock

## ➤ Good for Homodyne measurement

- The original plan is to use demodulation of  $f_2 - f_1$
- Just  $2f_2$  demodulation is suitable because it is an amplitude fluctuation



# Length sensing and control (new)

## ➤ FPMI

- Each arm:  $f_1$  (0.7 MHz) transmission PDH
- MICH:  $f_2$  (40 MHz) Q-phase

## ➤ SRC

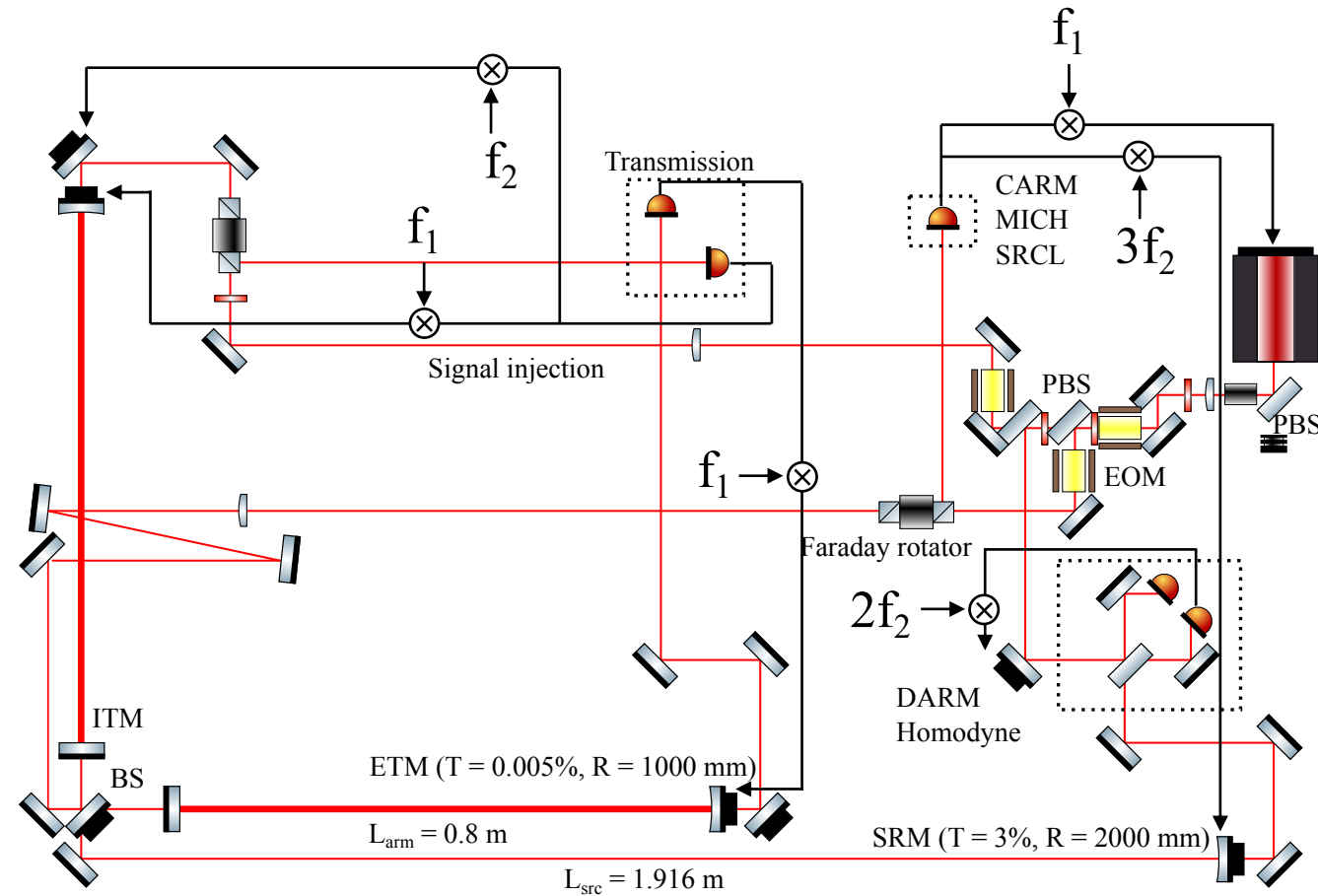
- $3f_2$  (120 MHz)

## ➤ Homodyne

- $2f_2$  (80 MHz)

## ➤ Injection

- $f_2$  (40 MHz)



# Solving the noise issue

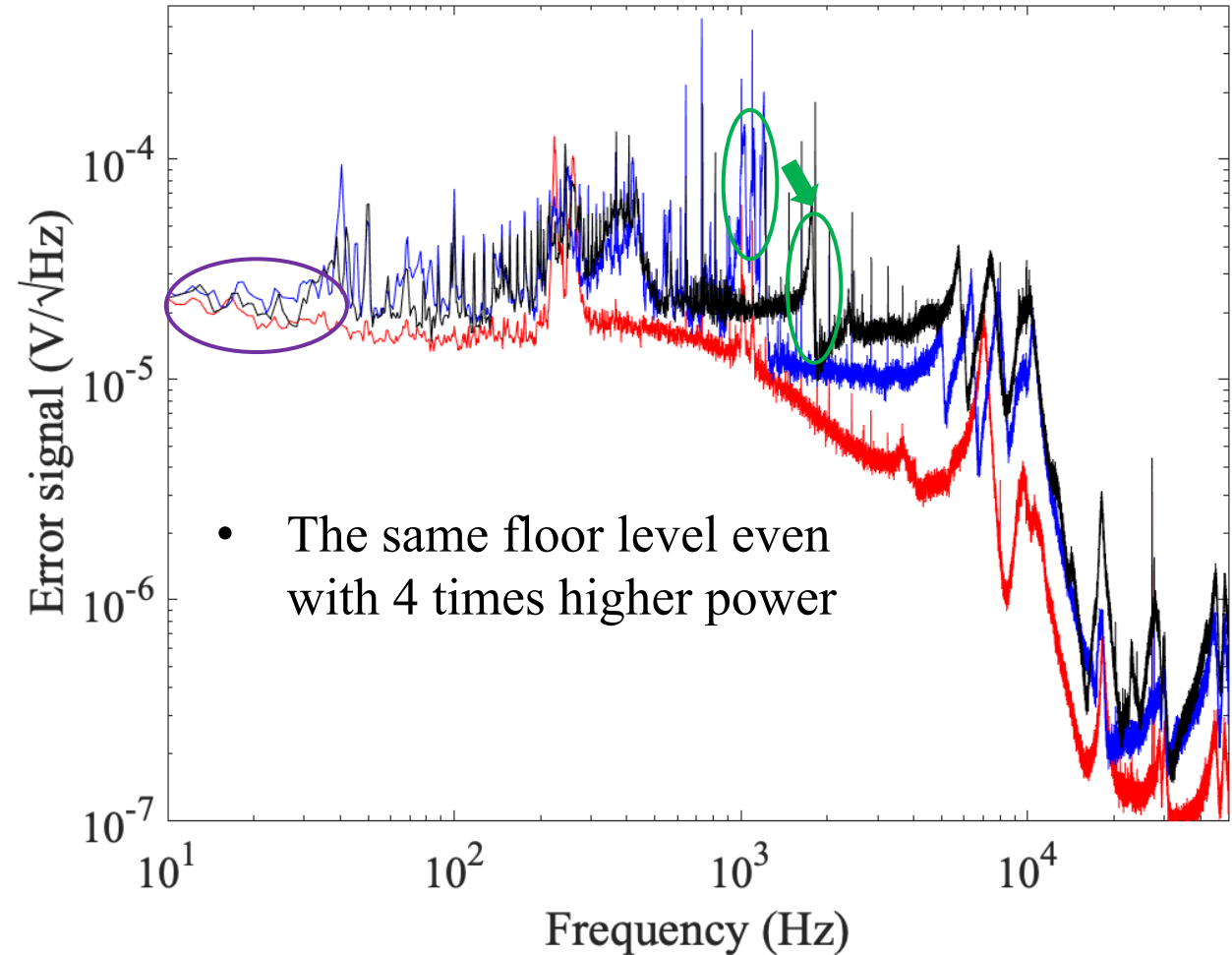
## ➤ Mainly two methods

- Increasing the power to reduce the Moku:Go ADC noise (red to blue)
- Lowering the height of the pedestal to make the parasitic resonant frequency higher (blue to black)

## ➤ Next step

- Increasing the trans-impedance gain of the PD to further reduce the ADC noise
- Checking the noise with the SRM aligned

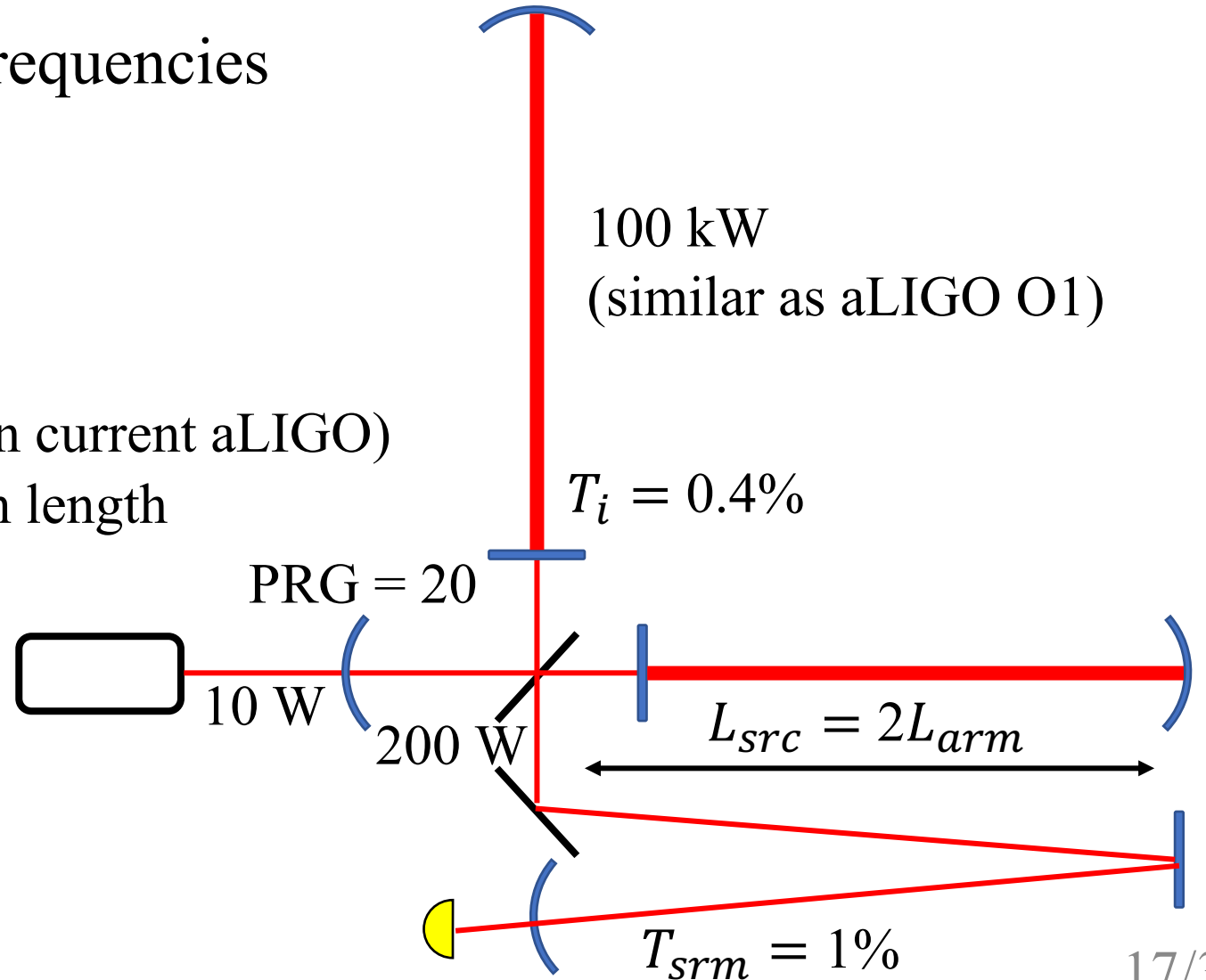
Raw error signal without any calibration





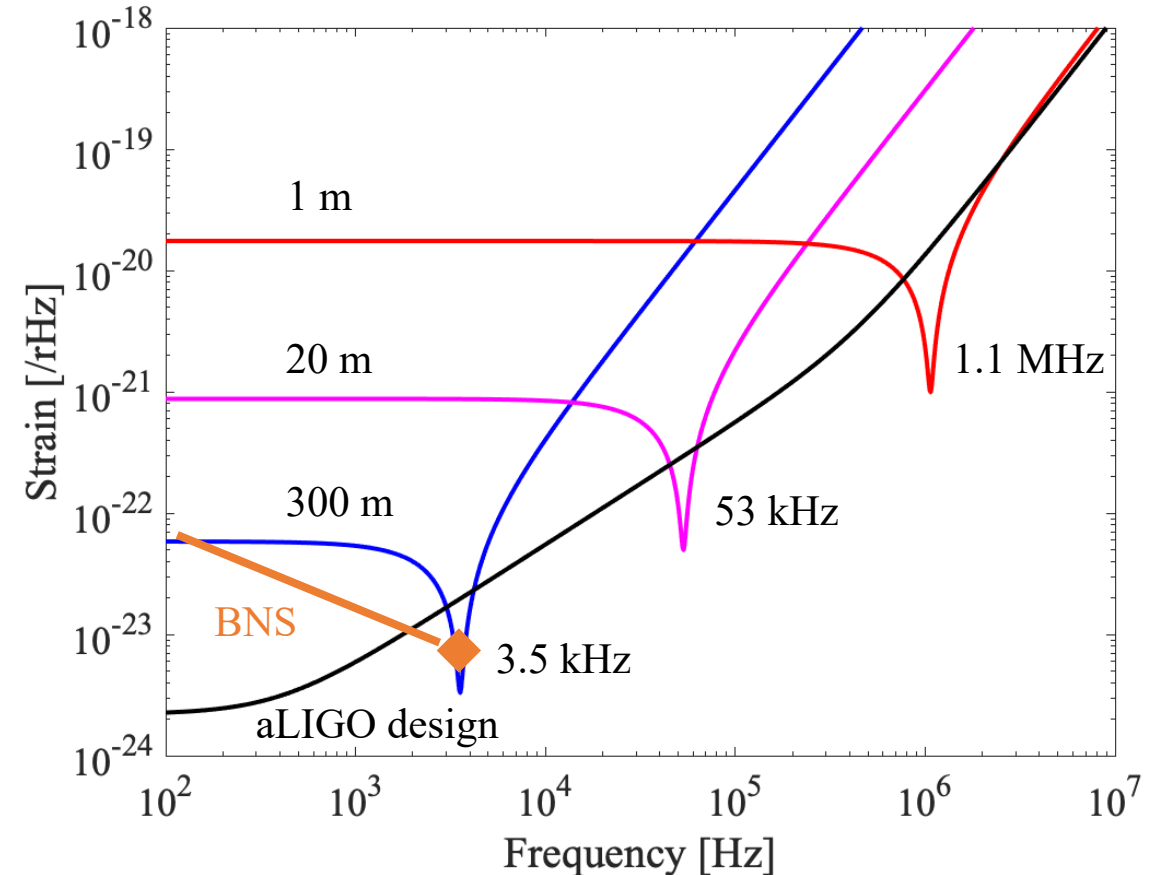
# Future

- GW observation at various frequencies
- Interferometer parameters
  - ITM transmissivity 0.4% (the same as KAGRA)
  - Power at BS 200 W (order of magnitude lower than current aLIGO)
  - SRC length is twice as the arm length
  - SRM transmission 1%
  - Roundtrip loss 100 ppm
  - SRM loss 1%
  - Detection loss 10%
  - 6 dB squeezing



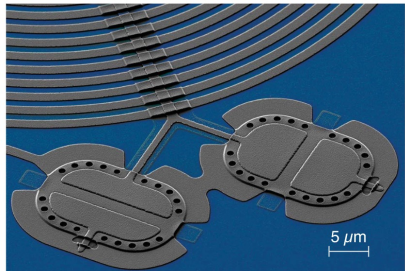
# Future

- LSRC can surpass the aLIGO design sensitivity at the dip frequency (ignoring FSR effect)
- The dip frequency with 300-m arms is similar as the BNS merger frequency
- Revival of TAMA-300 as a GW observatory



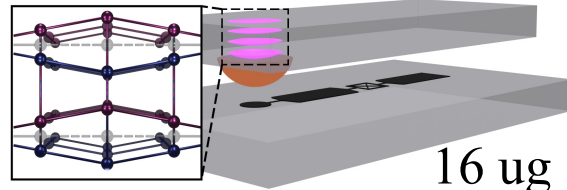
# Background

➤ The massive quantum (16 ug) and the lightest gravity (90 mg)



70 pg

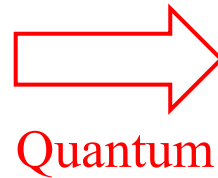
Science  
372, 622  
(2021)



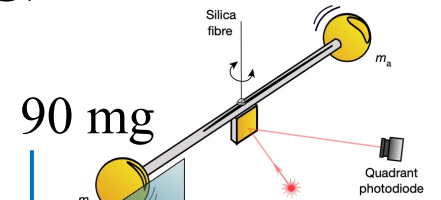
16 ug

Arxiv:2211.00449

- ✓ Bulk acoustic wave
- ✓ Electro-mechanics

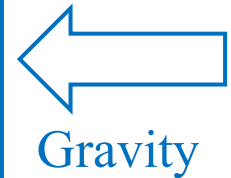


Planck mass  
22 ug



90 mg

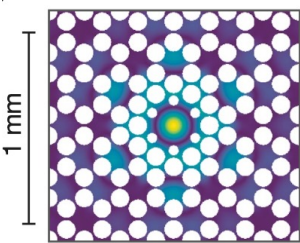
Nature  
591, 225  
(2021)



pg      ng      ug      mg      g      Mass

Nat. Phys. 15,  
745 (2019)

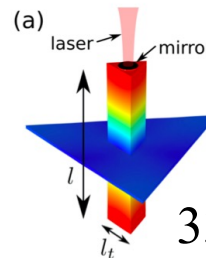
10 ng



Beyond standard quantum limit  
Will be entangled soon



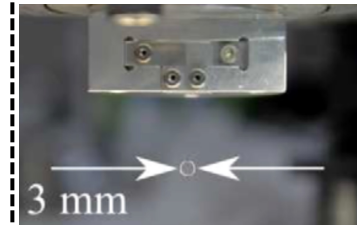
50 ng



33 ug

Near quantum

arxiv:2104.11648

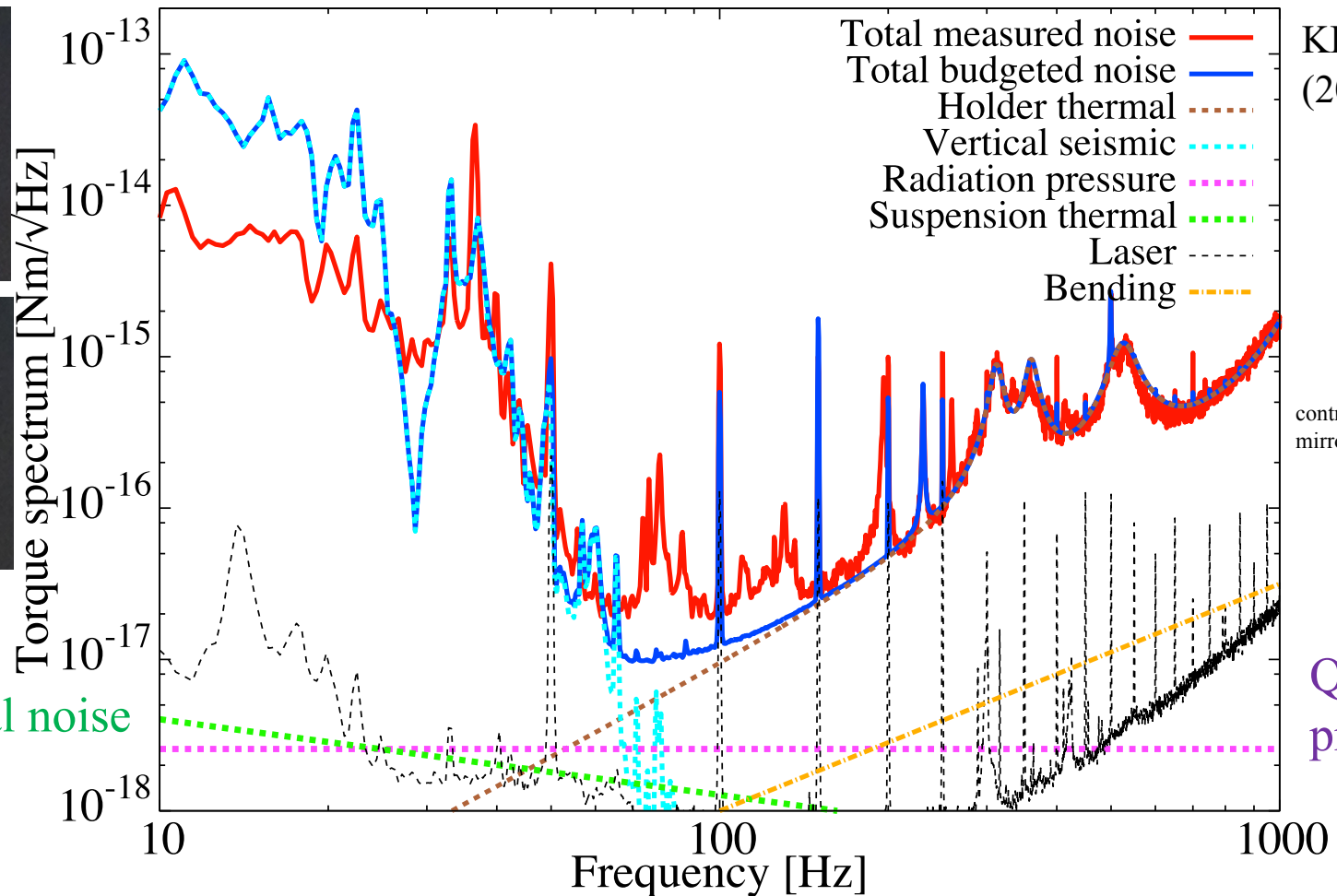
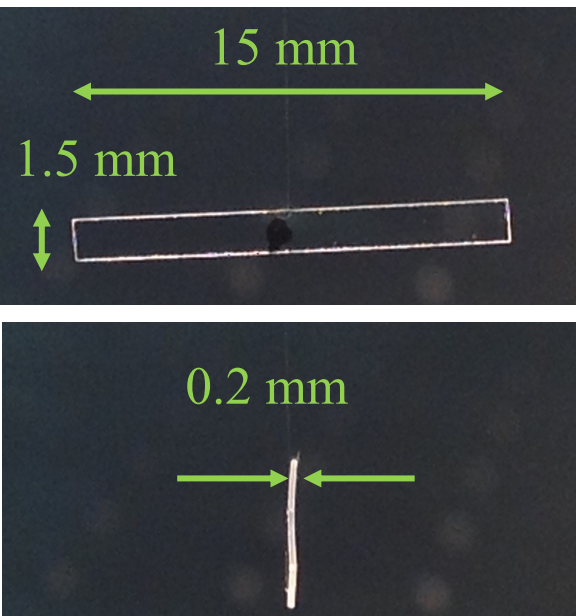


7 mg

PRL 122, 071101 (2019) 19/30

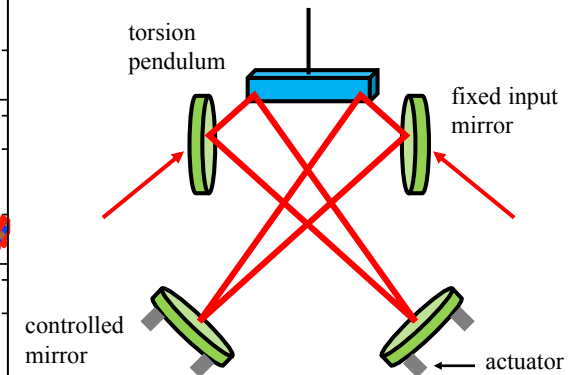
# My previous works

- Best sensitivity of  $20 \text{ aNm}/\sqrt{\text{Hz}}$  in mg-scale torque sensors



Suspension thermal noise

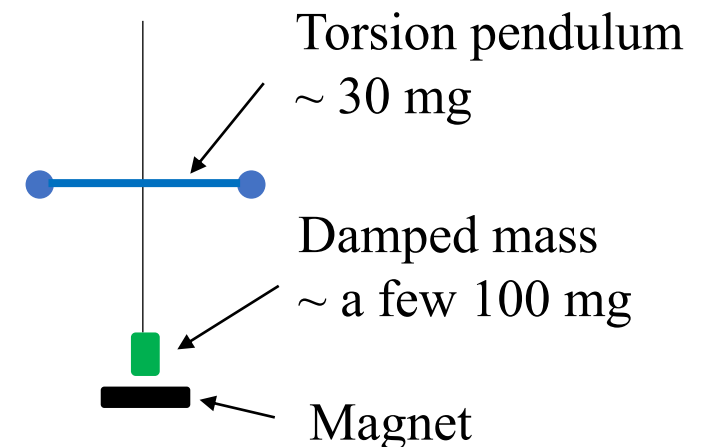
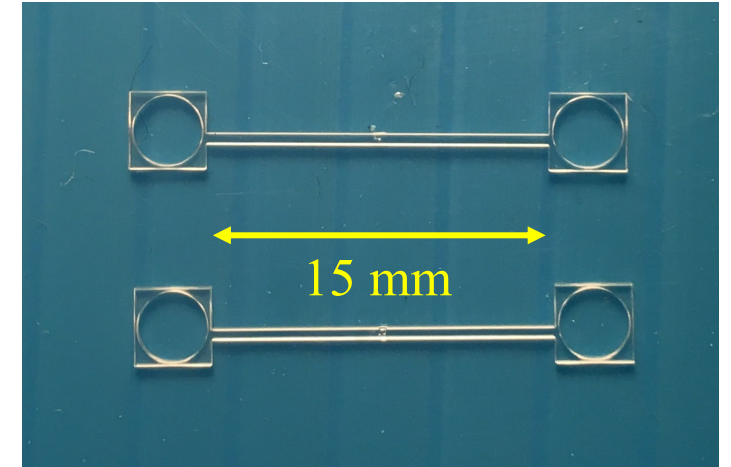
KK+, PRA 101, 011802 (R)  
(2020)



Quantum radiation  
pressure noise

# Current status

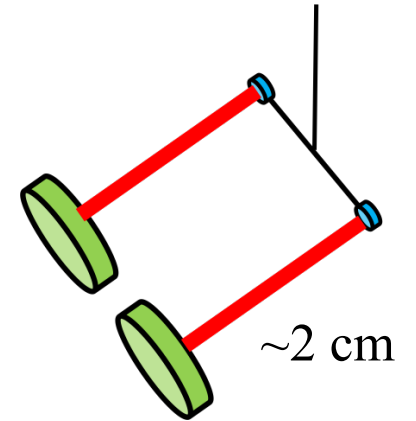
- New silica spacer
  - Two holes for the curved mirror at each edge, made by Opto-science and NSC
- Intensity stabilization on-going
- Will test the new test mass suspension with both ends clamp
  - Damped mass at the bottom is heavier than the torsion pendulum
  - The pendulum mode frequency is increased by a factor of  $\sqrt{\text{mass ratio}}$
  - Better stability, easier fabrication



# Short cavity

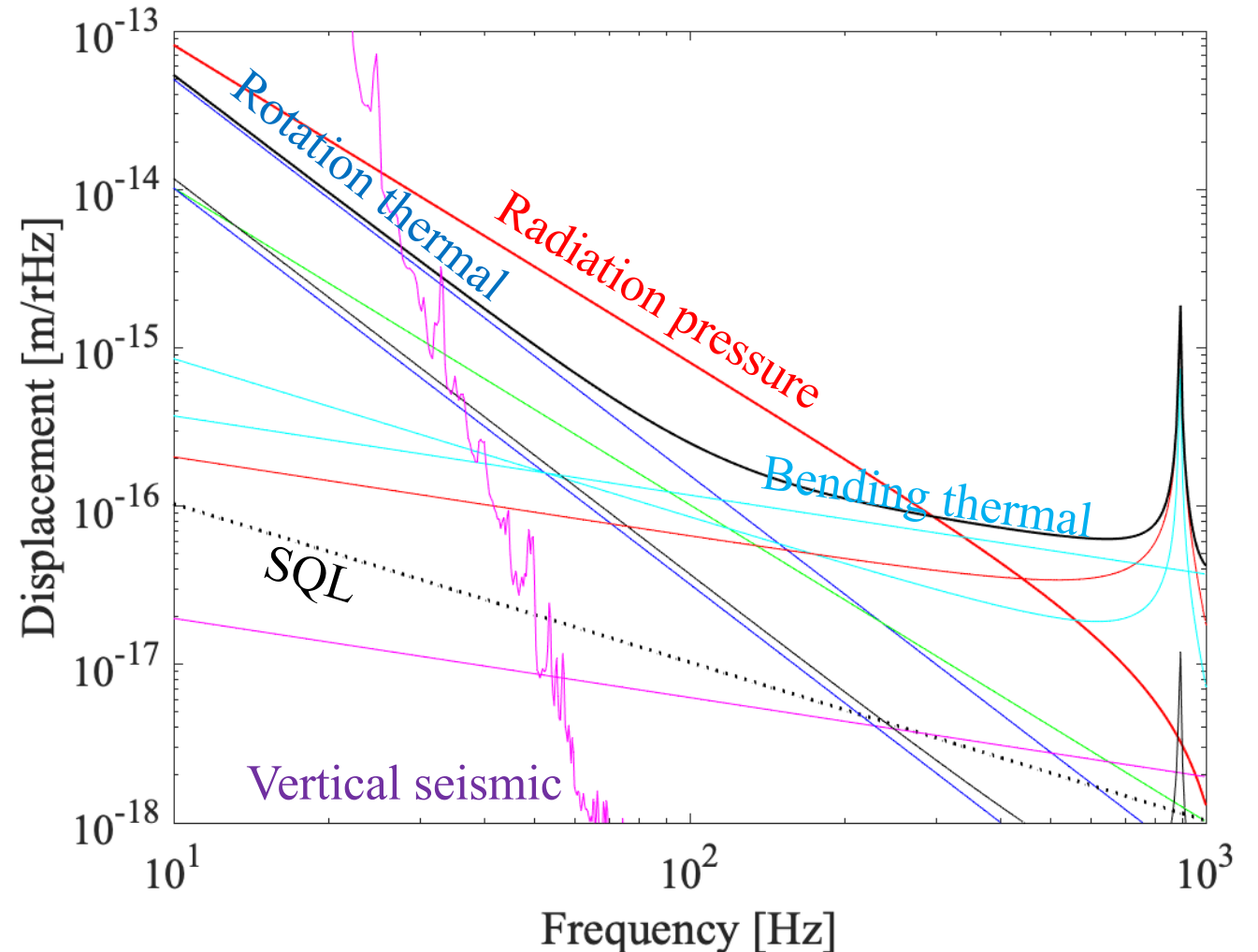
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- The negative g-factor is not necessary, which is required for the simple linear cavity
- In the case of the torsion pendulum, the optical springs at the edges overwhelm the anti torque spring
- That we can shorten the cavity is another advantage of the torsion pendulum in terms of the frequency noise



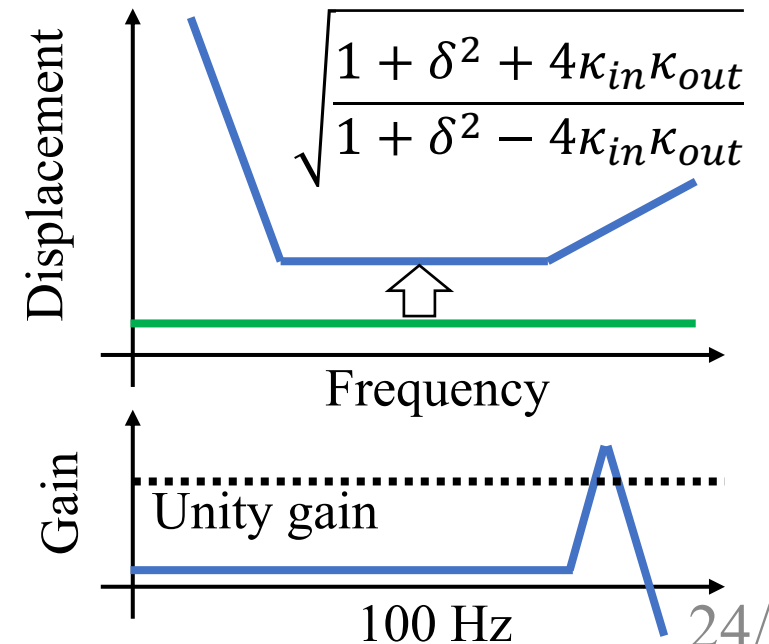
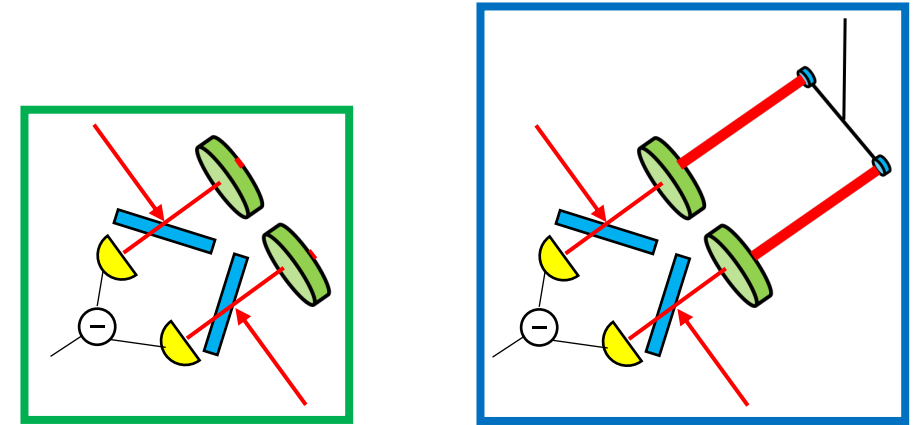
# Design sensitivity

- Radiation pressure dominant from 30 Hz to 300 Hz
- Vertical seismic noise at low frequencies
- Bending (Bar) thermal noise at high frequencies



# Measured spectrum

- Targeting frequency is around 100 Hz, which is much smaller than the optical spring frequency  $\sim 1$  kHz
- Feedback only around the optical spring with small openloop gain at 100 Hz (error signal measurement)
- Slight increasing of the floor compared to the shot noise without the cavity
  - A factor of  $\sim 1.3$  with  $\kappa_{in} = 0.9, \delta = 1/\sqrt{3}$





# B-L dark matter

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- $U(1)_{B-L}$  symmetry
- Different atoms feel different force
- Displacement of an optical cavity consisting of test masses made of different materials
- No experiments specifically targeting at the test

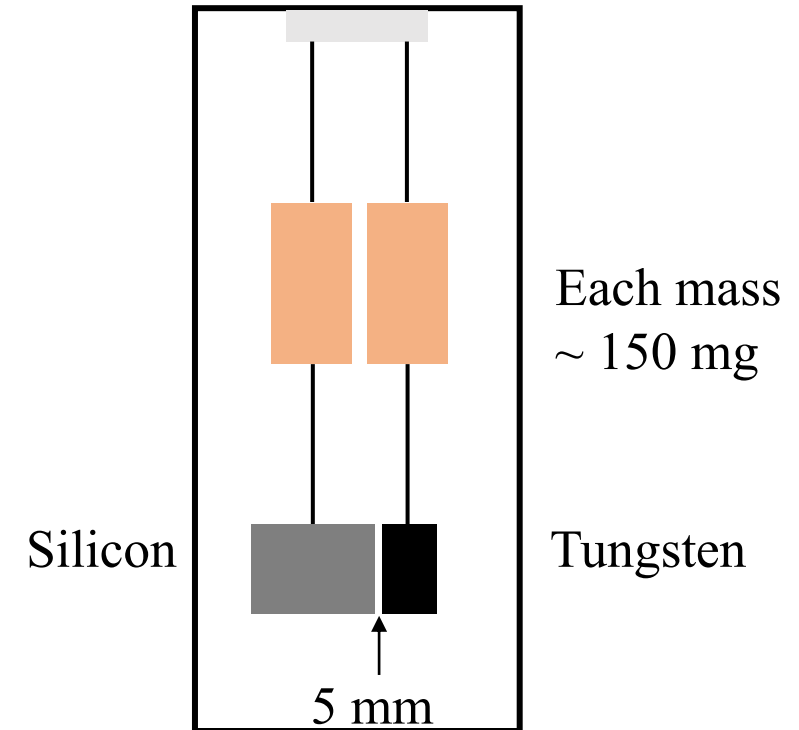
# Design

## ➤ Suspension

- The double pendulum chain is separated in Ono-kun's suspension

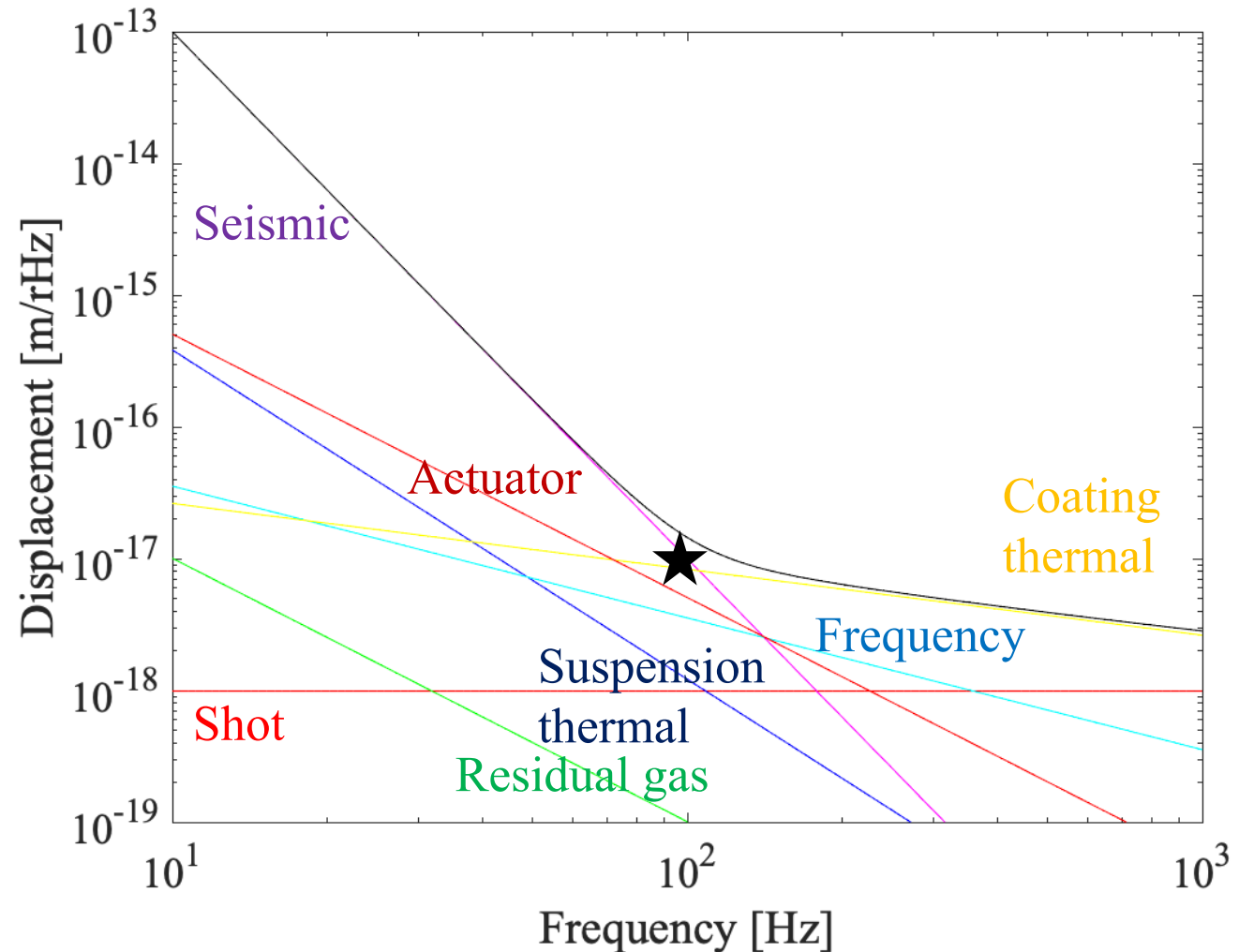
## ➤ Optical parameters

- Input power: 5 mW
- Cavity finesse: 3000
- Cavity length: 5 mm
- Side lock at the normalized detuning of  $1/\sqrt{2}$
- Intensity stabilization to the shot noise
- Frequency stabilization by 3 orders of magnitude



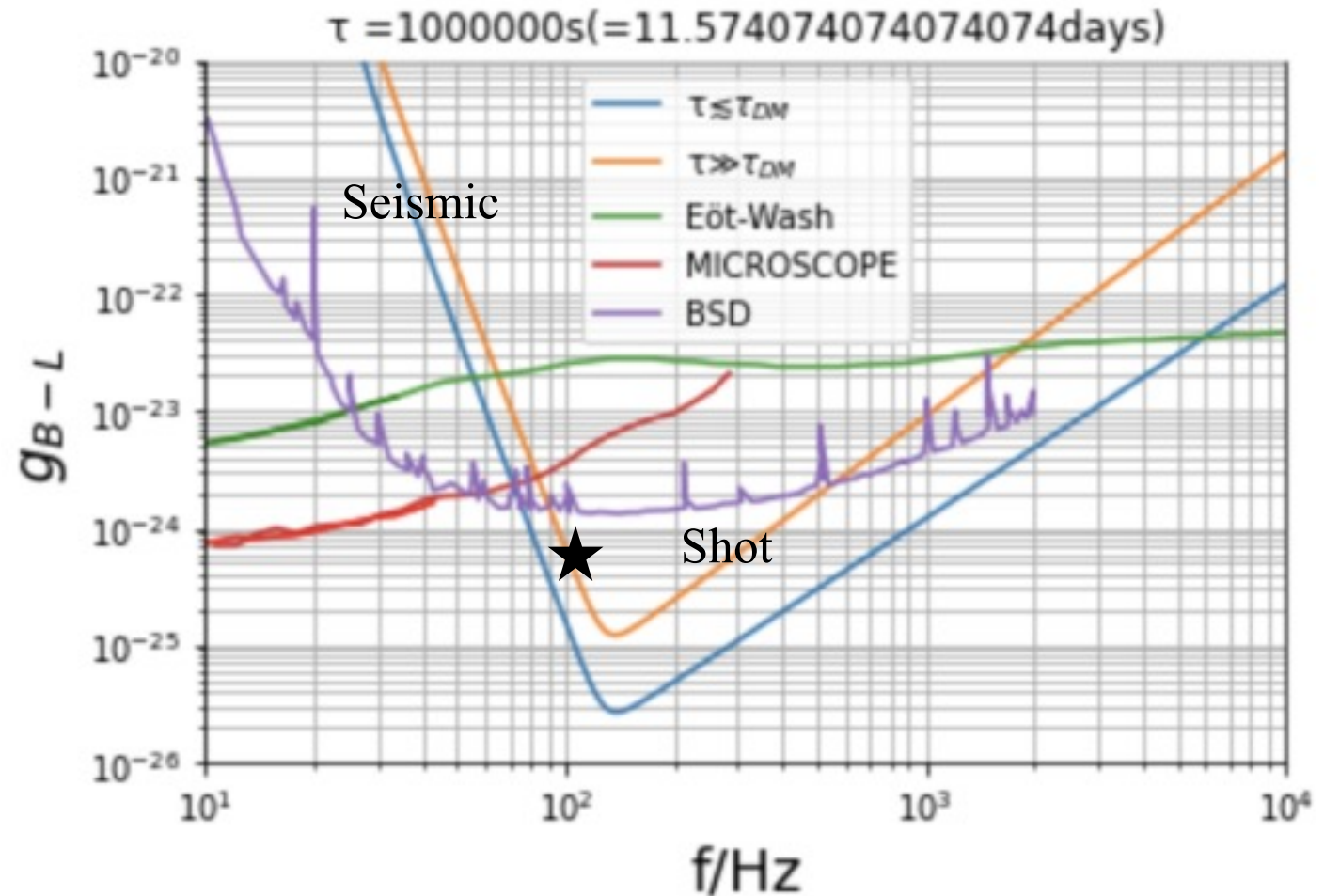
# Design sensitivity

- Target:  $1e-17$  m/ $\sqrt{\text{Hz}}$  at 100 Hz
  - The seismic, coating thermal, and actuator noises are critical
  - The frequency noise is not dominant thanks to the short cavity length
  - AlGaAs coating can reduce the coating thermal noise drastically

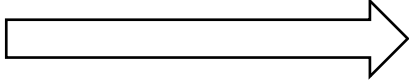
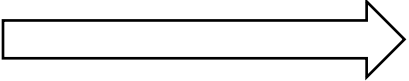
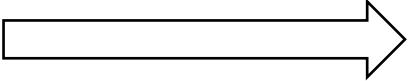
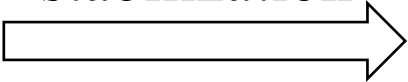
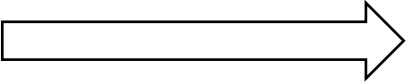
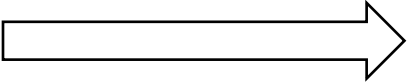
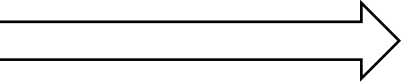
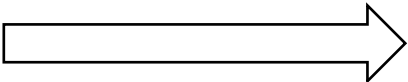
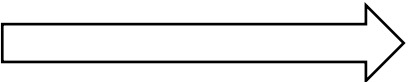
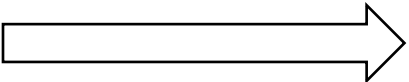
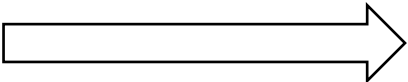


# Upper limit

- $g_{B-L} < 5e-25$  at 100 Hz
  - Beyond the previous works
  - Only 10 days
- Further improvement
  - More seismic isolation
  - AlGaAs coating
  - Longer operation



# Time schedule in 2023

	Q1	Q2	Q3	Q4
Long SRC	Experiment 		Paper writing 	Preparation of MHz detector 
Optomecha	Intensity stabilization 	Both clamp test 	Construction 	Cavity lock 
B-L	Design 	Construction 	Comissioning 	Operation 

# Summary

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## ➤ LSRC

- Improving the interferometer
- Aiming at completing the experiment by September
- MHz detector in the table top scale, kHz detector in TAMA-300

## ➤ Optomechanical torsion pendulum

- Recovering the setup with the improved configuration

## ➤ B-L

- Nice science with the realistic parameters