

Displacement Noises in Laser Interferometric Gravitational Wave Detectors

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Slides

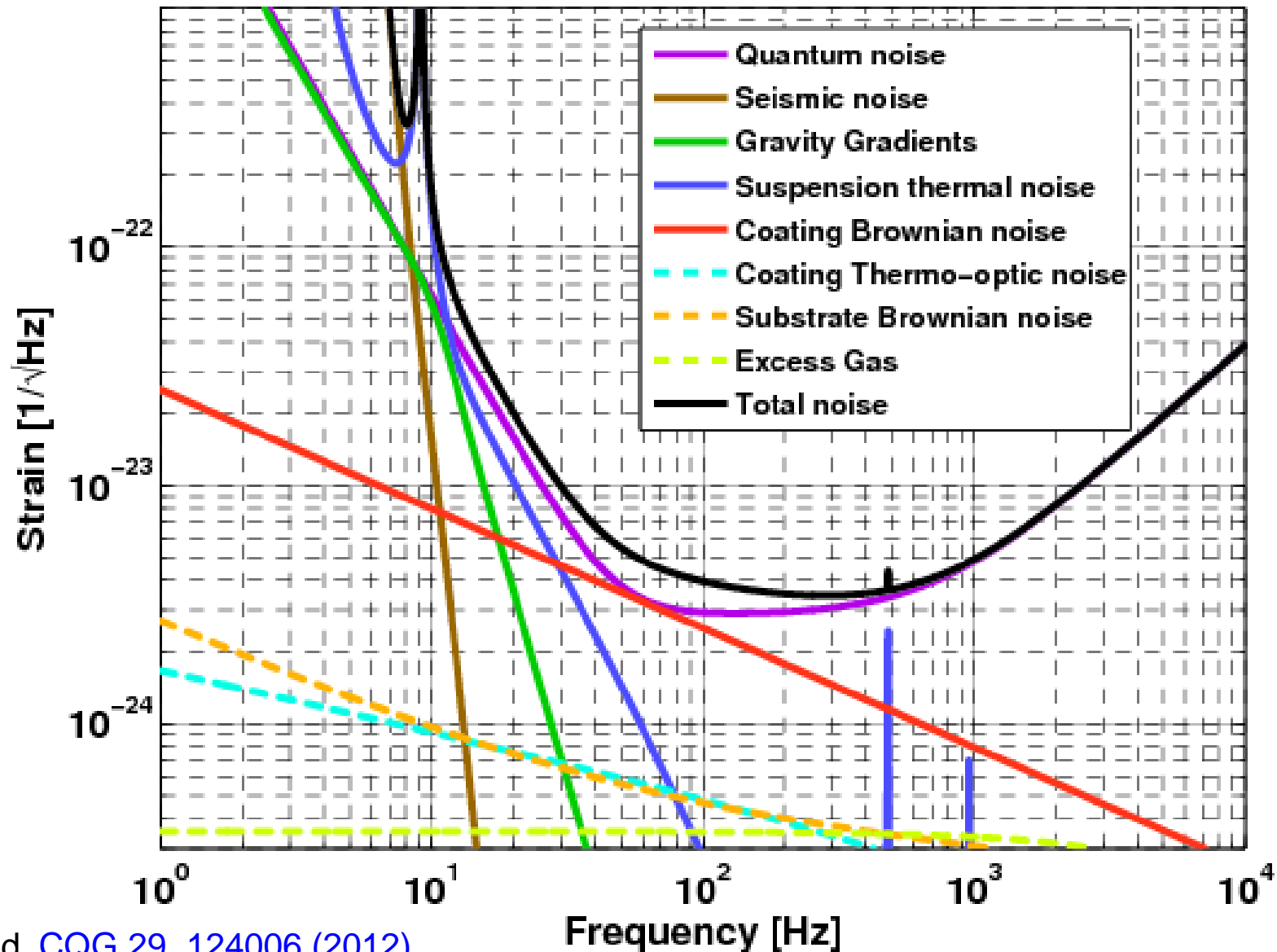
<http://granite.phys.s.u-tokyo.ac.jp/michimura/lectures/GWPhysics20171212.pdf>

or

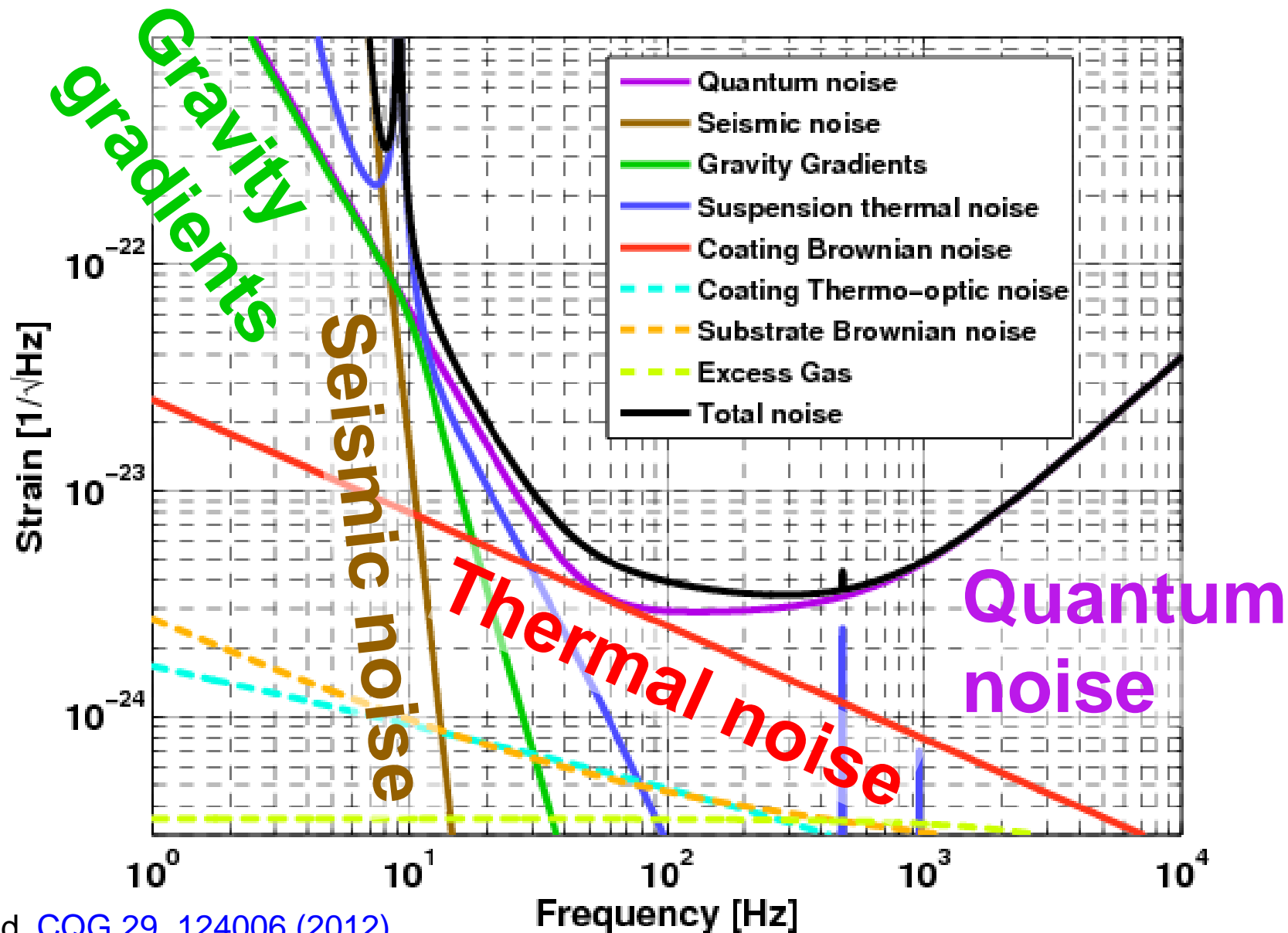
<https://tinyurl.com/GWPhysics20171212>



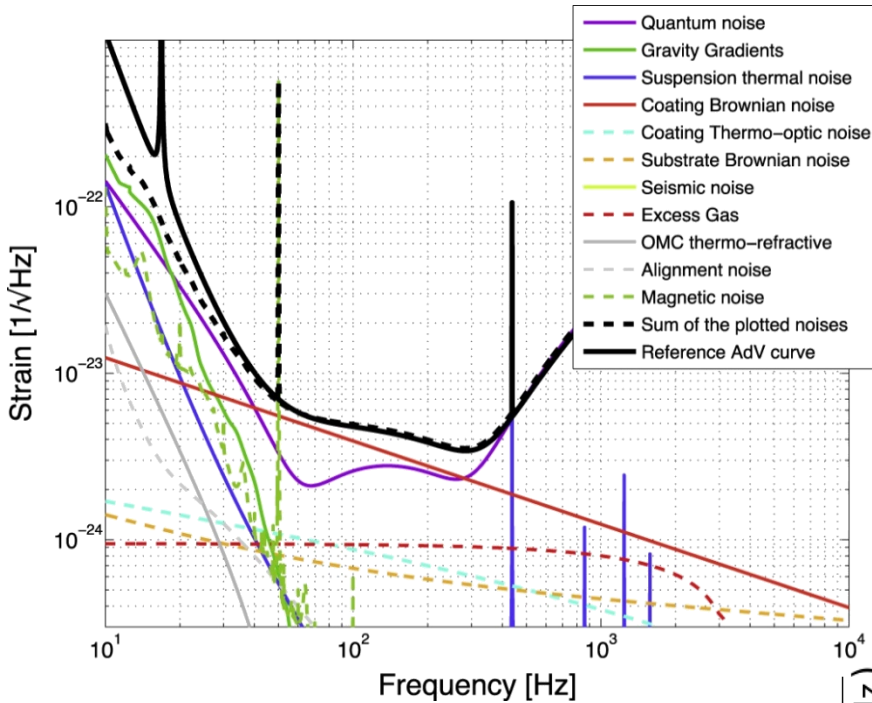
Advanced LIGO Design Sensitivity



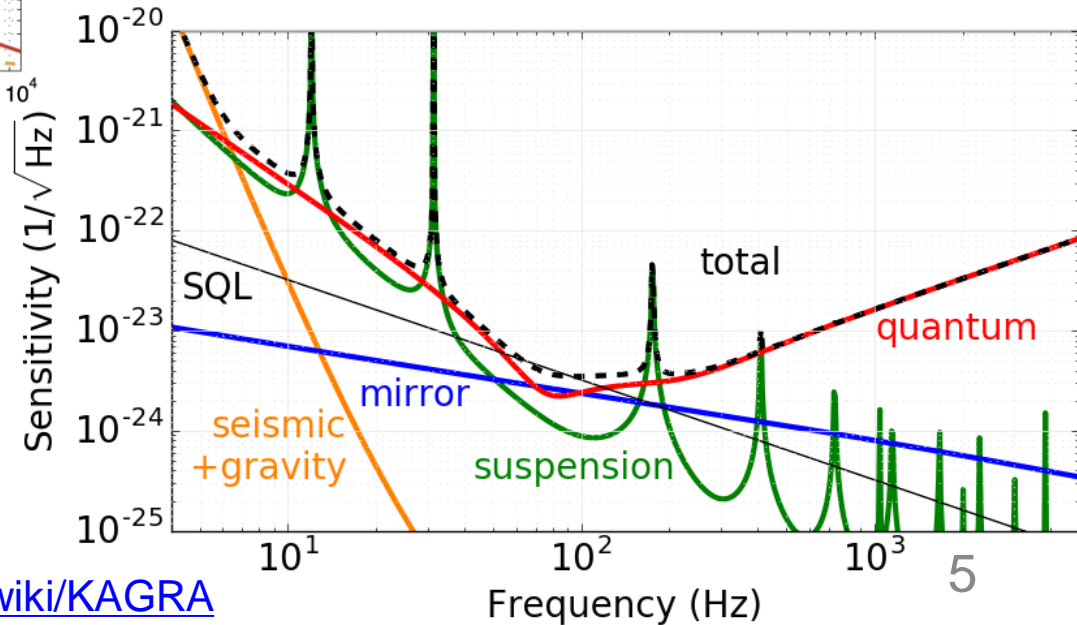
Advanced LIGO Design Sensitivity



Advanced Virgo and KAGRA



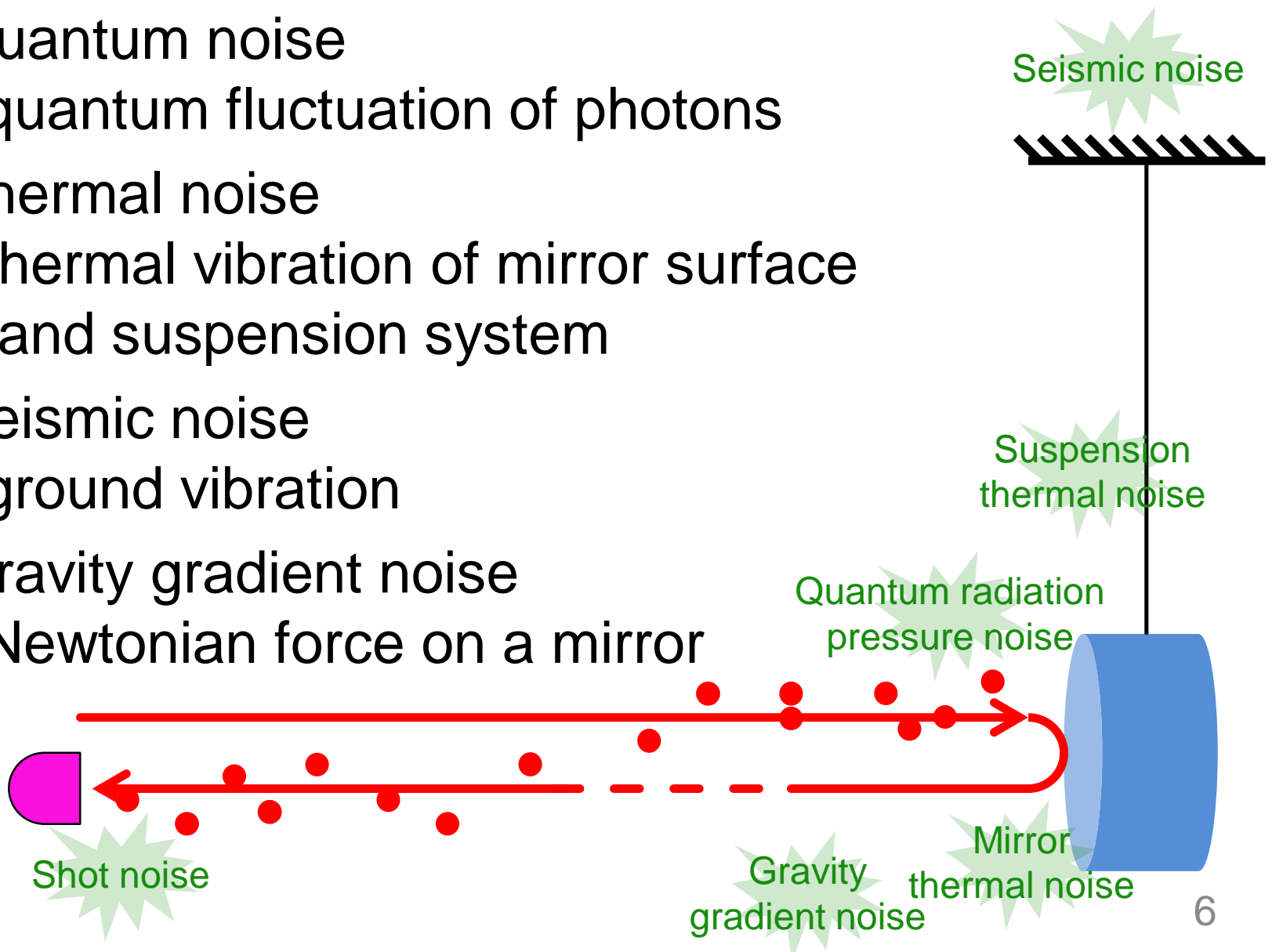
F. Acernese+, [CQG 32, 024001 \(2015\)](#)



<http://gwwiki.icrr.u-tokyo.ac.jp/JGWwiki/KAGRA>

Fundamental Noises

- Quantum noise
quantum fluctuation of photons
- Thermal noise
thermal vibration of mirror surface
and suspension system
- Seismic noise
ground vibration
- Gravity gradient noise
Newtonian force on a mirror



Contents

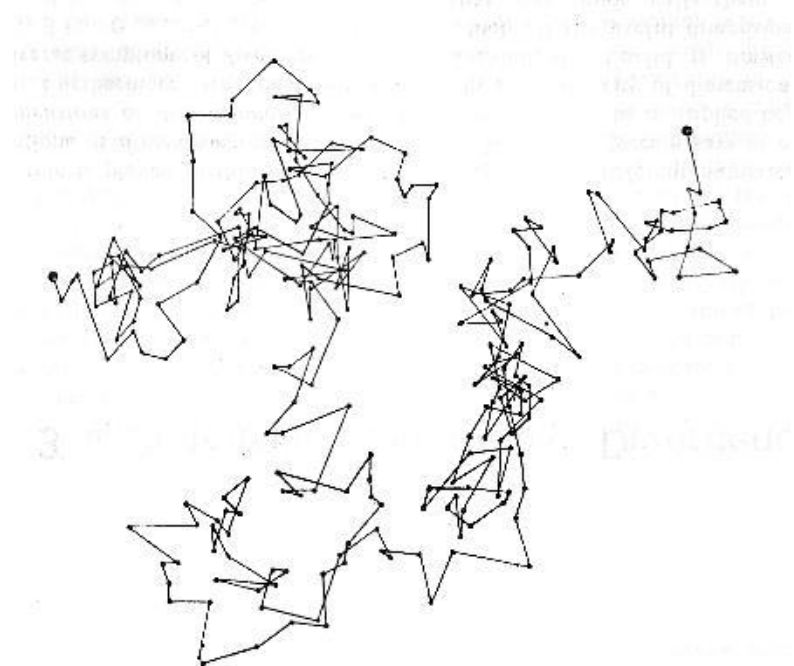
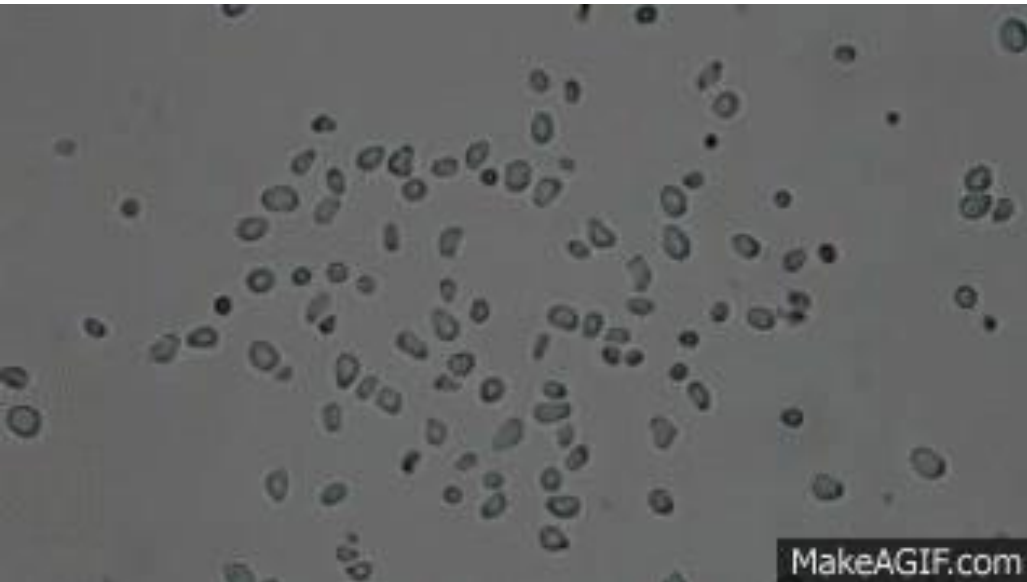
- Thermal noise
 - Brownian motion, Johnson-Nyquist noise
 - Fluctuation-dissipation theorem
 - Suspension thermal noise
 - Mirror thermal noise
 - Coating thermal noise

- Seismic noise
 - Seismic vibration
 - Vibration isolation
 - Gravity gradient noise
 - Underground site

Thermal Noise

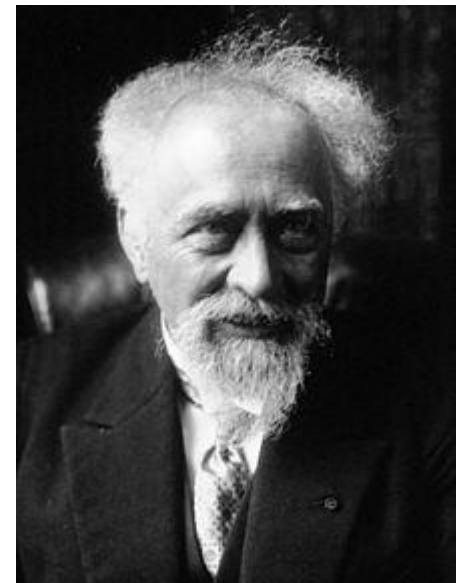
Brownian Motion

- 1827 Robert Brown
Discovered **random motion** of pollen grains in water
- Also proved that this motion exists in non-organic matter
→ not related to life



Molecular-Kinetic Theory

- 1905 Albert Einstein
Molecular-Kinetic Theory
→ Quantitative calculations on the movement of small particles in a liquid (Ph. D. Thesis)
- 1908 Jean B. Perrin
Experimental verification using colloid liquid
→ **Existence of atoms**
Statistical physics



Johnson-Nyquist Noise

- 1926 John B. Johnson observed **voltage fluctuation** across a resistor
- 1928 Harry Nyquist

$$V^2(f) = 4k_B T R$$

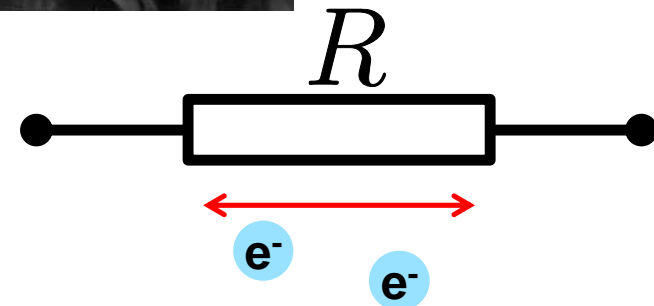
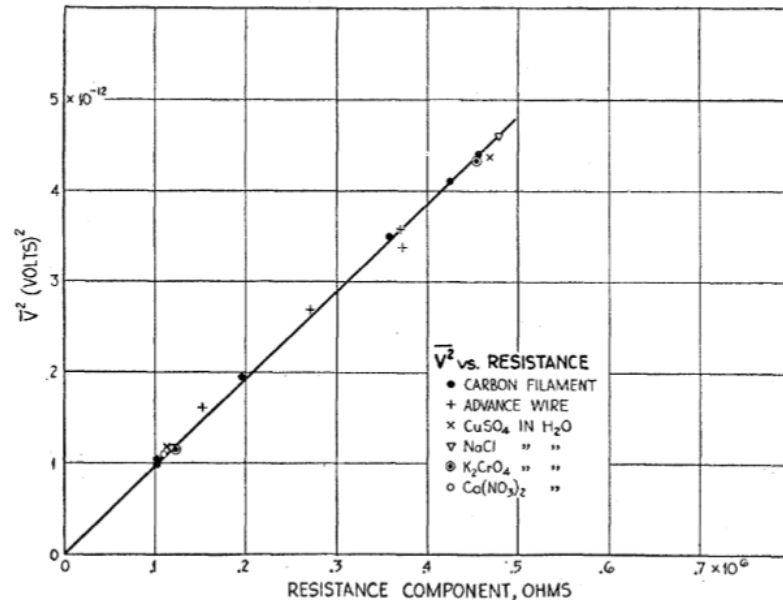
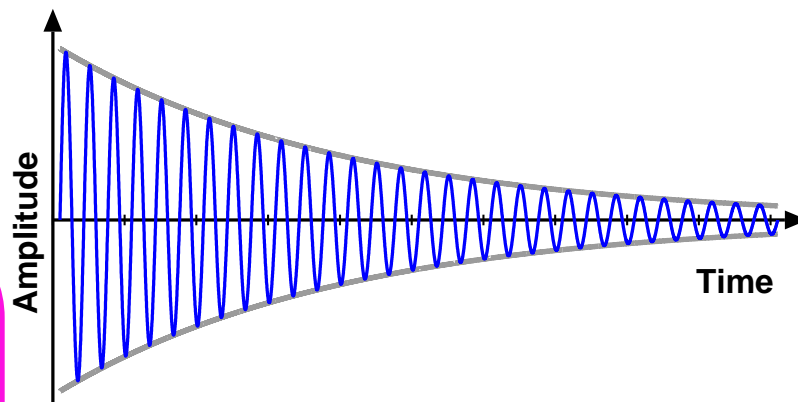
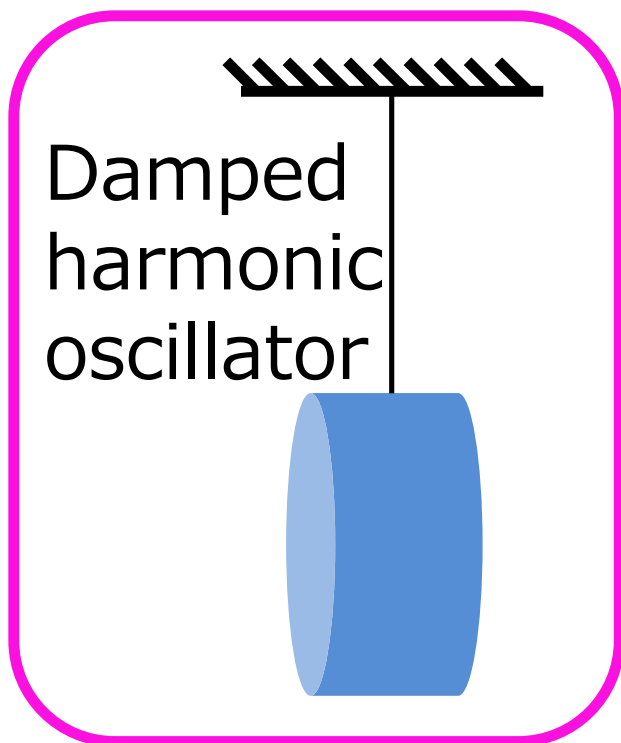


Fig. 4. Voltage-squared vs. resistance component for various kinds of conductors.

Generalization of Brownian Motion

- 1951-52 Herbert Callen et al.

Fluctuation-Dissipation Theorem



Energy dissipation



Thermal
fluctuating force



Thermal
bath
 T

Fluctuation-Dissipation Theorem

- Linear System



- System **impedance**

$$Z(\omega) = \frac{F(\omega)}{v(\omega)} = \frac{F(\omega)}{i\omega x(\omega)}$$

- Thermal fluctuating force for x is

$$F_{\text{th}}^2(\omega) = 4k_{\text{B}}T \text{Re}(Z(\omega))$$

- Analogy with Johnson-Nyquist noise

Voltage $V \leftrightarrow$ Force F

Current $I \leftrightarrow$ Velocity v

Resistor $R \leftrightarrow$ Real part of impedance Z

Fluctuation-Dissipation Theorem

- Thermal fluctuating force for x is

$$F_{\text{th}}^2(\omega) = 4k_{\text{B}}T \text{Re}(Z(\omega))$$

- Thermal fluctuation of x will be

$$\begin{aligned} x_{\text{th}}^2(\omega) &= \frac{F_{\text{th}}^2(\omega)}{\omega^2 |Z(\omega)|^2} \\ &= \frac{4k_{\text{B}}T}{\omega^2} \text{Re}(Y(\omega)) \end{aligned}$$

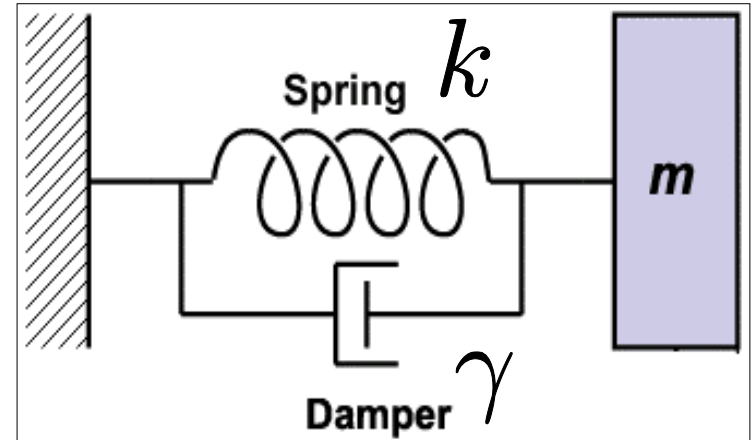
admittance

$$Y(\omega) \equiv Z^{-1}(\omega)$$

Harmonic Oscillator

- Damped harmonic oscillator (**viscous damping**)

$$m\ddot{x} + \gamma\dot{x} + kx = F$$



- Admittance

$$Y(\omega) = \frac{i\omega x(\omega)}{F(\omega)}$$

$$= \frac{i\omega}{-\omega^2 m + i\omega\gamma + k}$$

$$= \frac{\gamma + i(k/\omega - \omega m)}{\gamma^2 + (k/\omega - \omega m)^2}$$

- Thermal noise

$$x_{\text{th}}^2(\omega) = \frac{4k_B T}{\omega^2} \text{Re}(Y(\omega)) = \frac{4k_B T \gamma}{\gamma^2 \omega^2 + (k - m\omega^2)^2}$$

Harmonic Oscillator

- Resonant frequency and Q value

$$\omega_0 = \sqrt{\frac{k}{m}} \quad Q = \frac{m\omega_0}{\gamma}$$

- Thermal noise

$$\begin{aligned} x_{\text{th}}^2(\omega) &= \frac{4k_{\text{B}}T\gamma}{\gamma^2\omega^2 + (k - m\omega^2)^2} \\ &= \frac{4k_{\text{B}}T\omega_0}{mQ} \frac{1}{(\omega^2 - \omega_0^2)^2 + \frac{\omega_0^2\omega^2}{Q^2}} \end{aligned}$$

$$\omega \ll \omega_0$$

$$\frac{4k_{\text{B}}T}{m\omega_0^3} \frac{1}{Q}$$

$$\omega = \omega_0$$

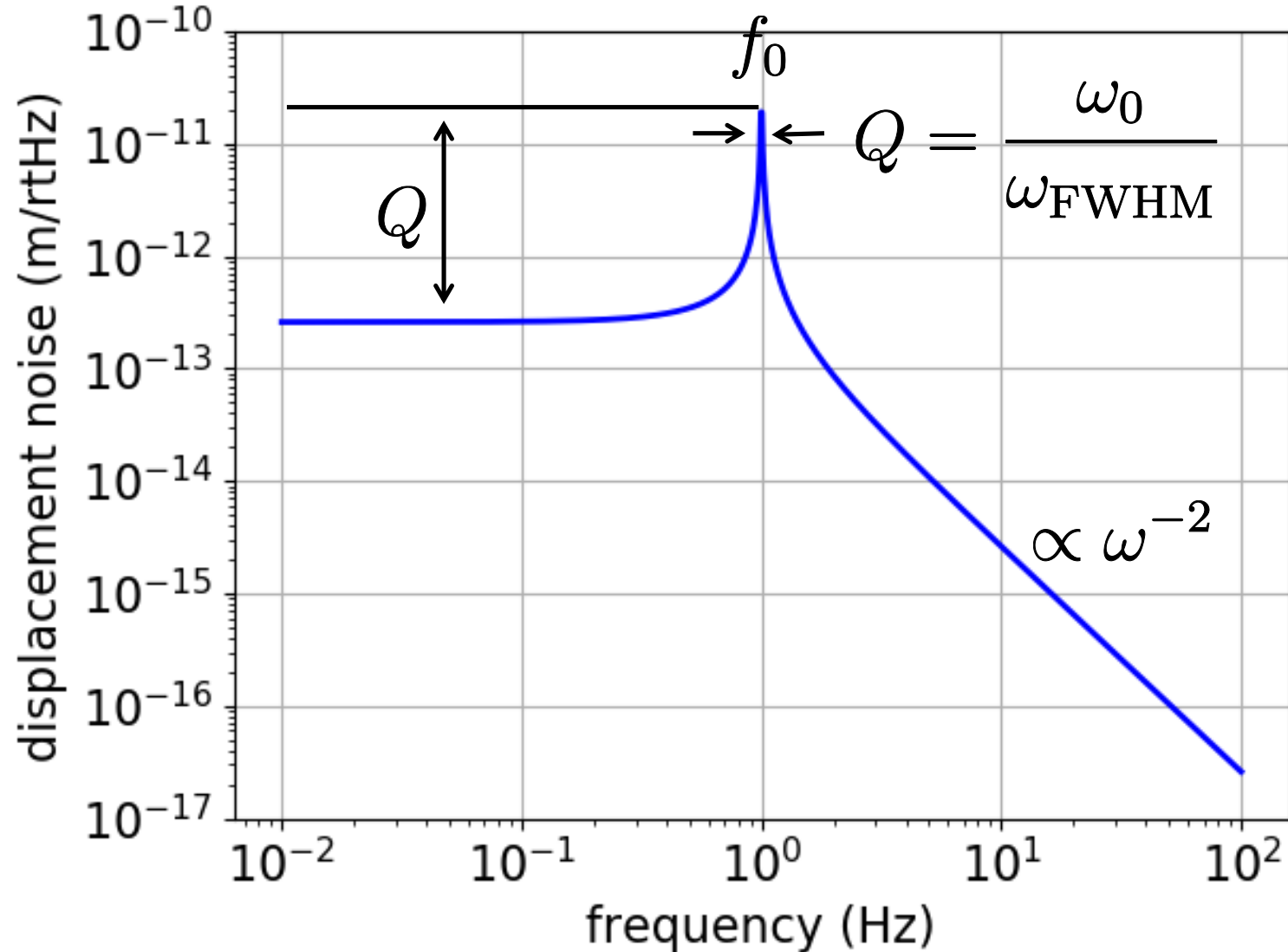
$$\frac{4k_{\text{B}}T}{m\omega_0^3} Q$$

$$\omega \gg \omega_0$$

$$\frac{4k_{\text{B}}T\omega_0}{m\omega^4} \frac{1}{Q}$$

Harmonic Oscillator

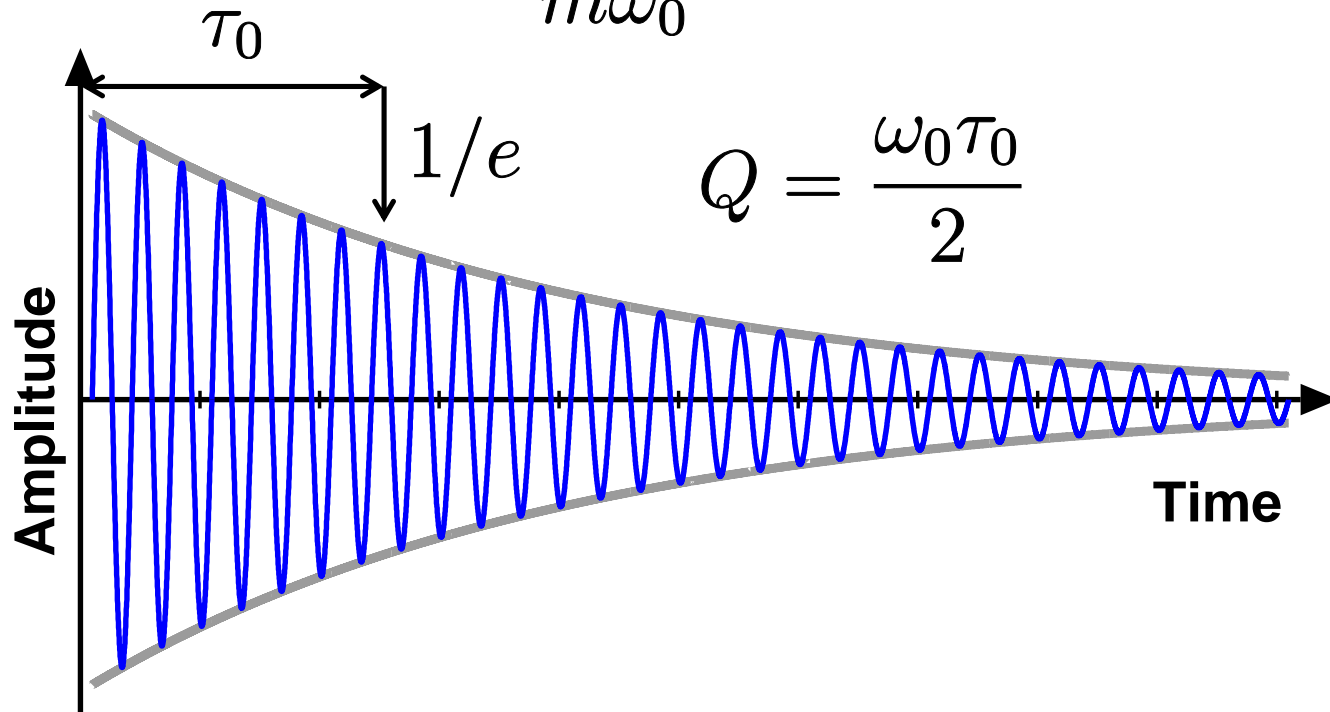
- Thermal noise spectrum



Harmonic Oscillator

- Resonant frequency and Q-value can be measured from the **impulse response**

$$x(t) = \frac{1}{m\omega_0} e^{-\frac{\omega_0 t}{2Q}} \sin \omega_0 t$$



tuning fork

Structural Damping

- Viscous damping
(e.g. gas damping, eddy-current damping)

$$m\ddot{x} + \gamma\dot{x} + kx = F$$

- **Structural damping**
(e.g. internal friction of materials)

- elastic material

$$F_{\text{spring}} = -kx \quad (\text{Hooke's Law})$$

- **anelastic** material  **loss angle**

$$F_{\text{spring}} = -k(1 + i\phi(\omega))x$$

Delay between displacement and force
→ energy dissipation

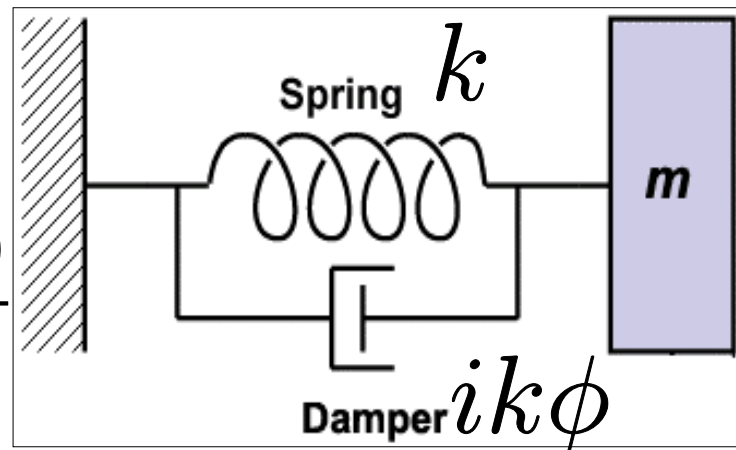
Structural Damping

- Damped harmonic oscillator (structural damping)

$$m\ddot{x} + k(1 + i\phi)x = F$$

- Admittance

$$Y(\omega) = \frac{k\phi\omega + i(k\omega - m\omega^3)}{k^2\phi^2 - (k - m\omega^2)^2}$$



- Thermal noise

$$x_{\text{th}}^2(\omega) = \frac{1}{\omega} \frac{4k_{\text{B}}T k\phi}{k^2\phi^2 + (k - m\omega^2)^2}$$

Structural Damping

- Resonant frequency and Q value

$$\omega_0 = \sqrt{\frac{k}{m}} \quad Q = \frac{1}{\phi(\omega)}$$

- Thermal noise

$$\begin{aligned} x_{\text{th}}^2(\omega) &= \frac{1}{\omega} \frac{4k_{\text{B}}T k \phi}{k^2 \phi^2 + (k - m\omega^2)^2} \\ &= \frac{4k_{\text{B}}T \omega_0^2 \phi}{m\omega} \frac{1}{\omega_0^4 \phi^2 + (\omega^2 - \omega_0^2)^2} \end{aligned}$$

$$\omega \ll \omega_0$$

$$\frac{4k_{\text{B}}T}{m\omega_0^2} \frac{\phi}{\omega}$$

$$\omega = \omega_0$$

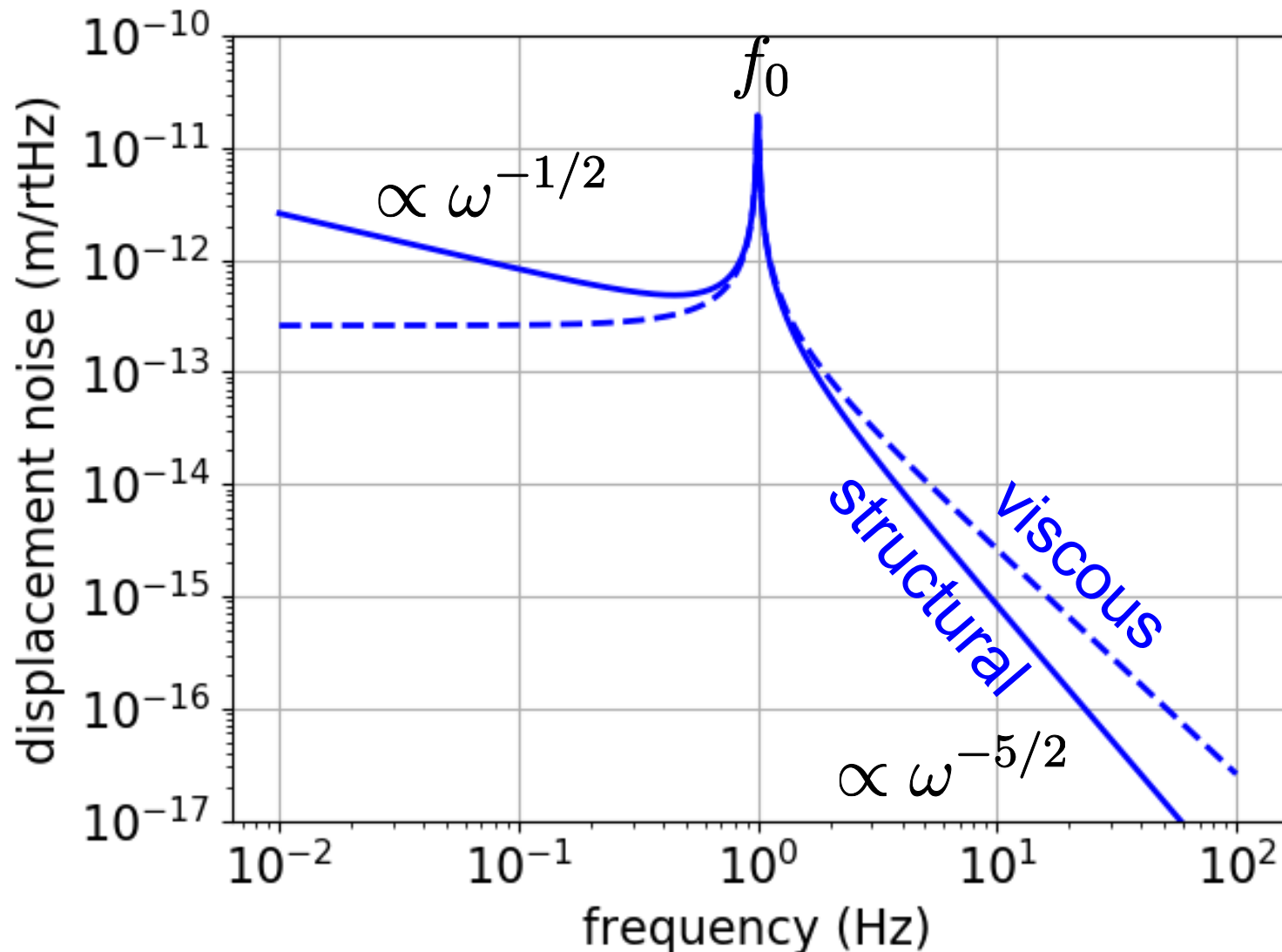
$$\frac{4k_{\text{B}}T}{m\omega_0^3} \frac{1}{\phi}$$

$$\omega \gg \omega_0$$

$$\frac{4k_{\text{B}}T \omega_0}{m\omega^4} \frac{\phi}{\omega}$$

Structural Damping

- Thermal noise spectrum when $\phi(\omega) \sim \text{const.}$



Pendulum Thermal Noise

- Restoring force

$$F_{\text{spring}} = -(mg/l + k_{\text{el}}(1 + i\phi))x$$

$$= -(mg/l + k_{\text{el}})(1 + i\phi_p)x$$

- Gravitational dilution

$$\phi_p \equiv \underbrace{\frac{k_{\text{el}}}{mg/l + k_{\text{el}}}}_{\text{dilution factor}} \phi \approx \frac{\phi}{2l} \sqrt{\frac{EI}{mg}}$$

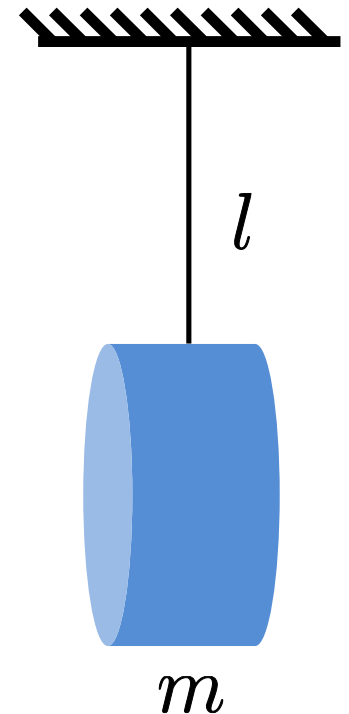
loss angle
of pendulum
 $10^{-5} \sim 10^{-7}$

dilution factor
 $10^{-3} \sim 10^{-2}$

intrinsic loss angle
of wire $10^{-4} \sim 10^{-3}$

$$k_{\text{el}} = \frac{\sqrt{TEI}}{2l^2} = \frac{\sqrt{mgEI}}{2l^2}$$

T : wire tension
 E : wire Young's modulus
 I : wire moment of inertia

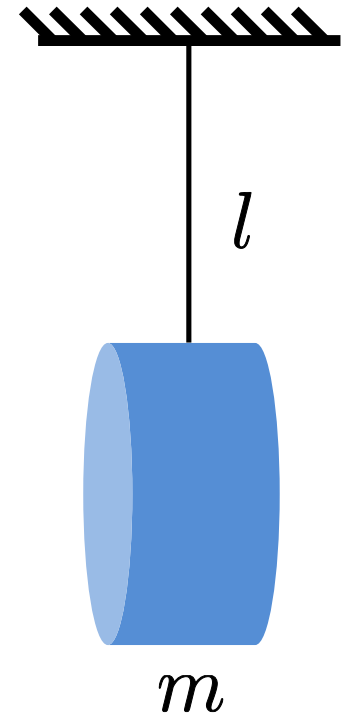


Pendulum Thermal Noise

- Suspension thermal noise ($\omega \gg \omega_0$)

$$x_{\text{susp}}^2(\omega) = \frac{4k_{\text{B}}T\omega_0 \phi_{\text{p}}}{m\omega^4 \omega}$$

$$= \frac{4k_{\text{B}}T}{m\omega^5} \sqrt{\frac{g}{l}} \frac{\phi}{2l\omega} \sqrt{\frac{EI}{mg}}$$



- **To lower the thermal noise**

- lower temperature $x_{\text{susp}}(\omega) \propto \sqrt{T\phi}$
- lower loss angle
- longer suspension $x_{\text{susp}}(\omega) \propto l^{-3/2}$
- heavier mirror

$$x_{\text{susp}}(\omega) \propto m^{-1/4} \text{ assuming } I \propto A^2$$

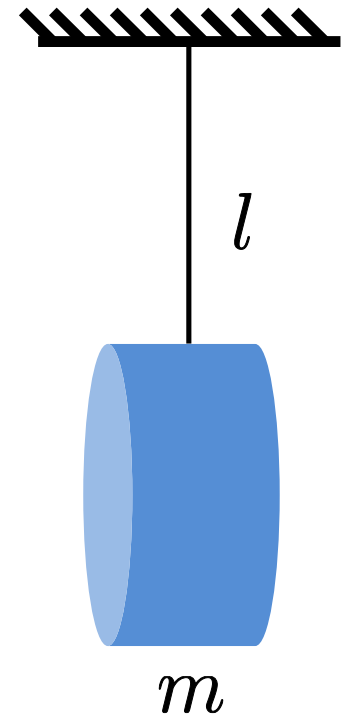
$$A: \text{ wire cross section } m \propto A$$

Pendulum Thermal Noise

- Suspension thermal noise ($\omega \gg \omega_0$)

$$x_{\text{susp}}^2(\omega) = \frac{4k_{\text{B}}T\omega_0 \phi_{\text{p}}}{m\omega^4} \frac{1}{\omega}$$

- Calculate suspension thermal noise for $m=10$ kg, $f_0=1$ Hz, $T=300$ K, $\phi_{\text{p}}=10^{-6}$ at 100 Hz. $k_{\text{B}}=1.38 \times 10^{-23}$ J/K

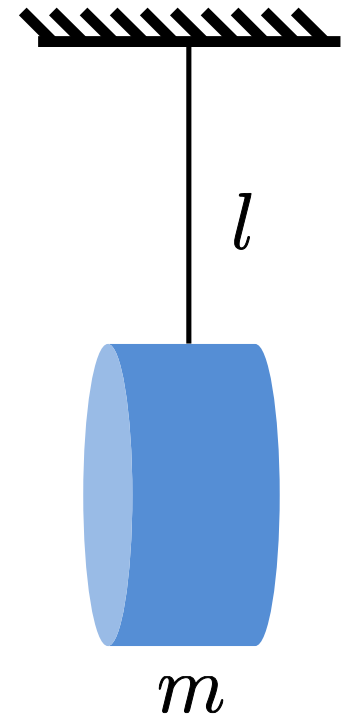


Pendulum Thermal Noise

- Suspension thermal noise ($\omega \gg \omega_0$)

$$x_{\text{susp}}^2(\omega) = \frac{4k_{\text{B}}T\omega_0 \phi_{\text{p}}}{m\omega^4} \frac{1}{\omega}$$

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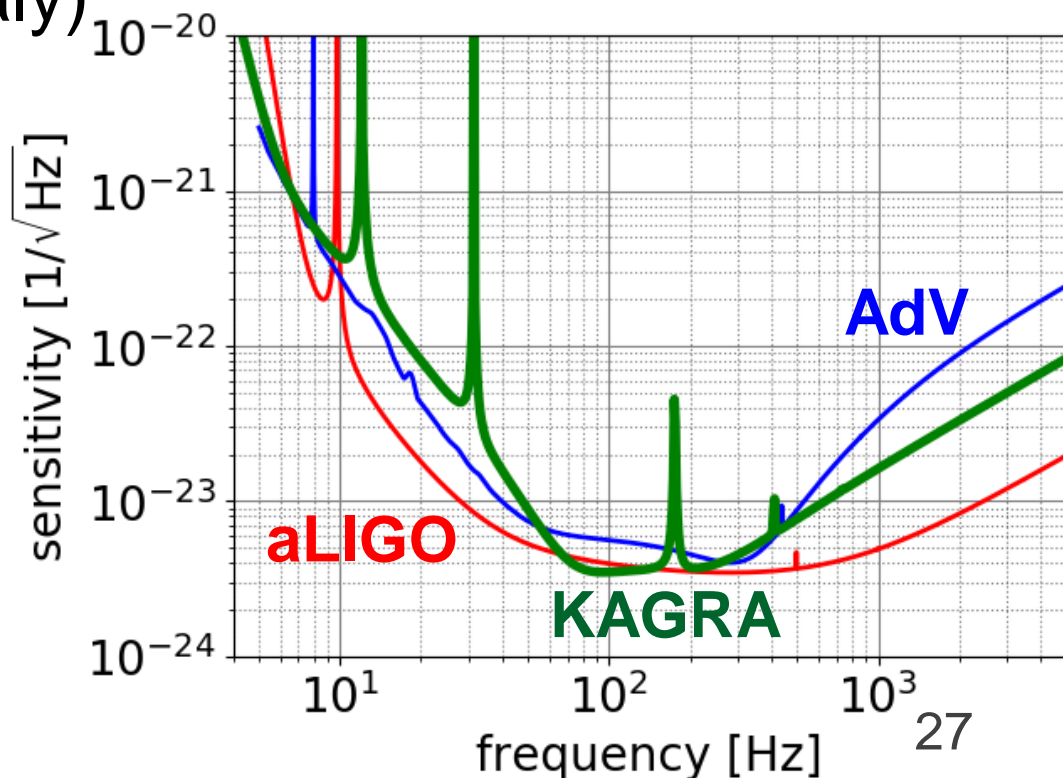


$$x_{\text{susp}}(\omega) = 1.0 \times 10^{-20} \left(\frac{100 \text{ Hz}}{f} \right)^{5/2} \text{ m}/\sqrt{\text{Hz}}$$

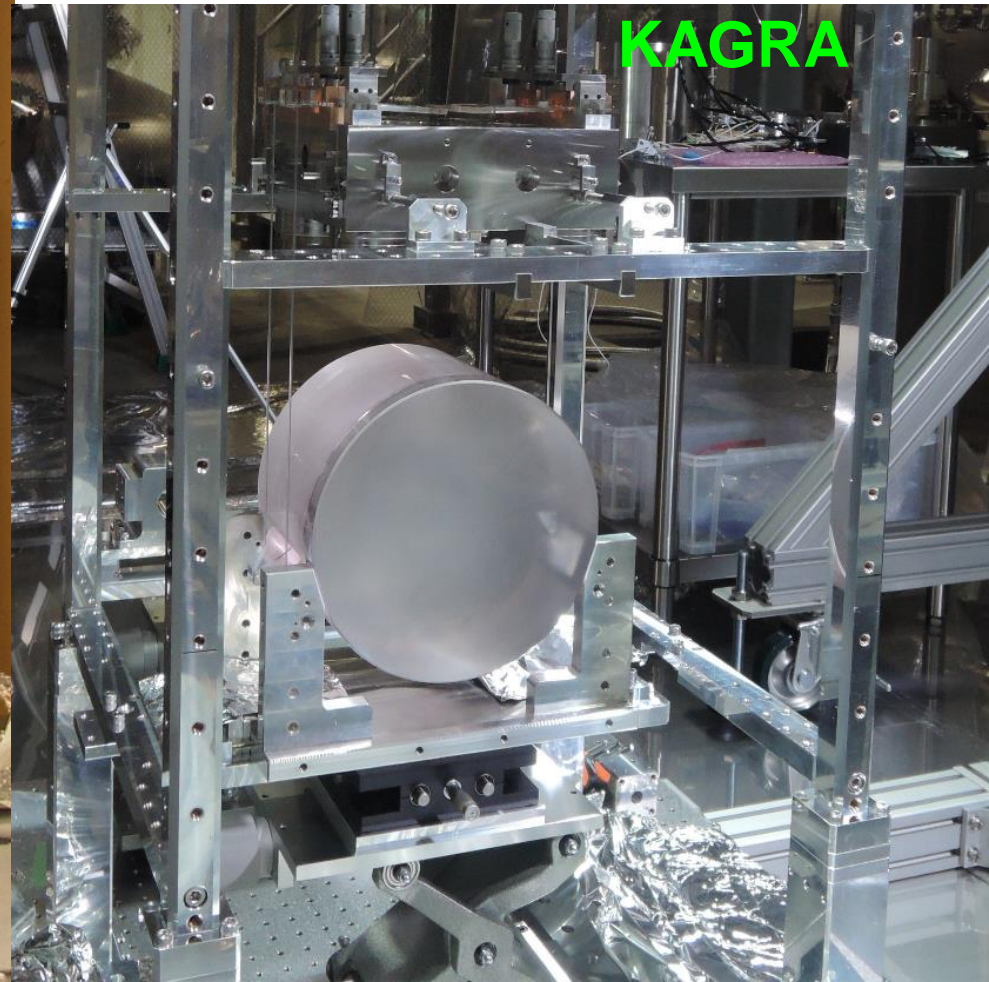
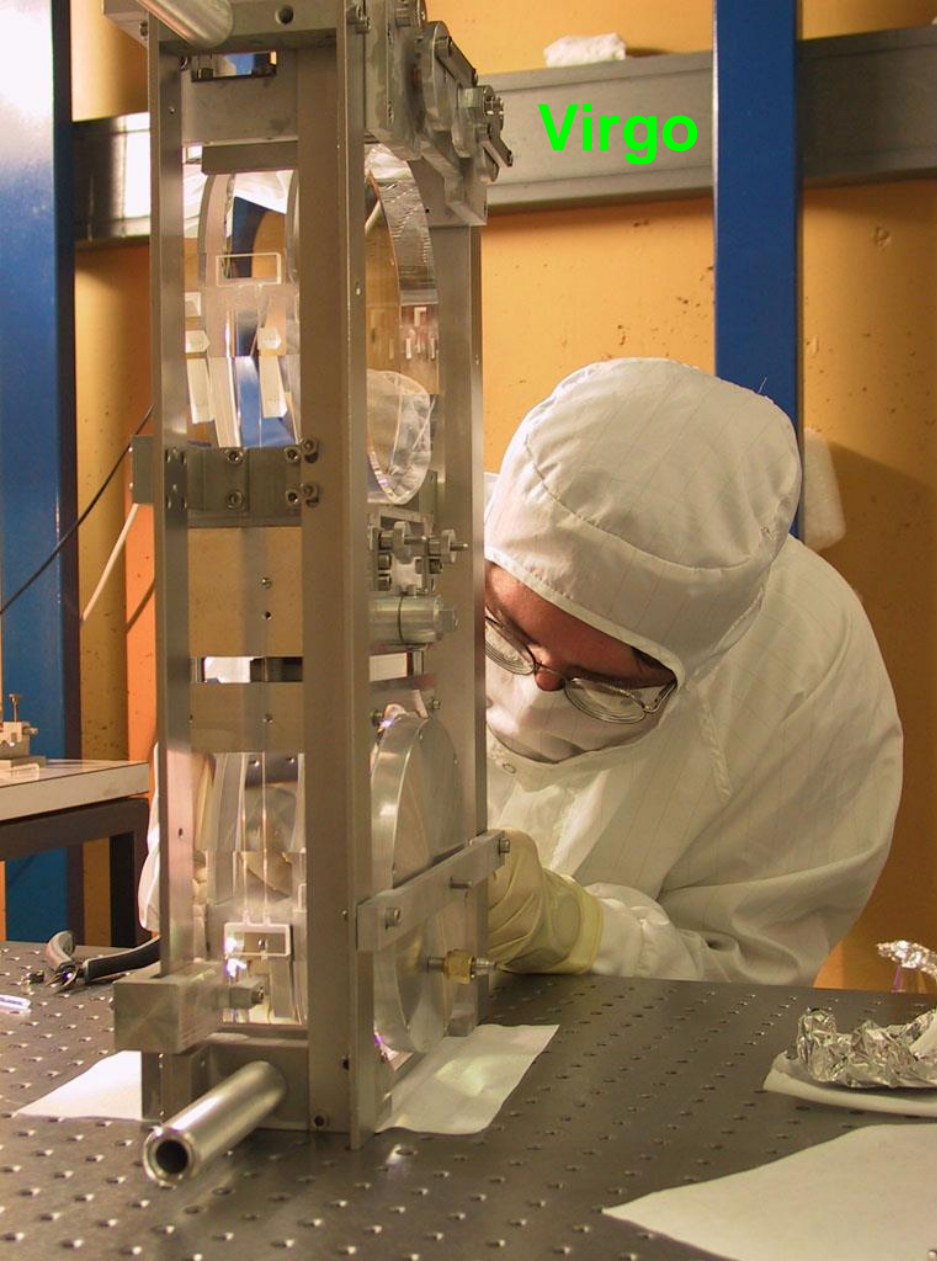
Sufficient for GW detection!

Suspension Thermal Noise in 2G

- Advanced LIGO (US)
40 kg, 60 cm,
fused silica,
295 K, $\phi w = \sim 1e-7$
- Advanced Virgo (Italy)
42 kg, 70 cm,
fused silica,
295 K, $\phi w = \sim 1e-7$
- KAGRA (Japan)
23 kg, 23 cm,
sapphire,
22 K, $\phi w = 2e-7$

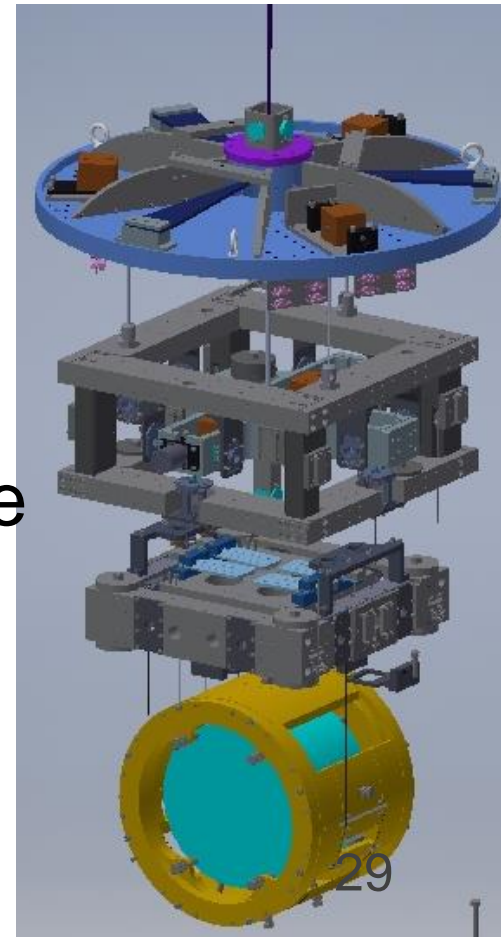


Suspensions

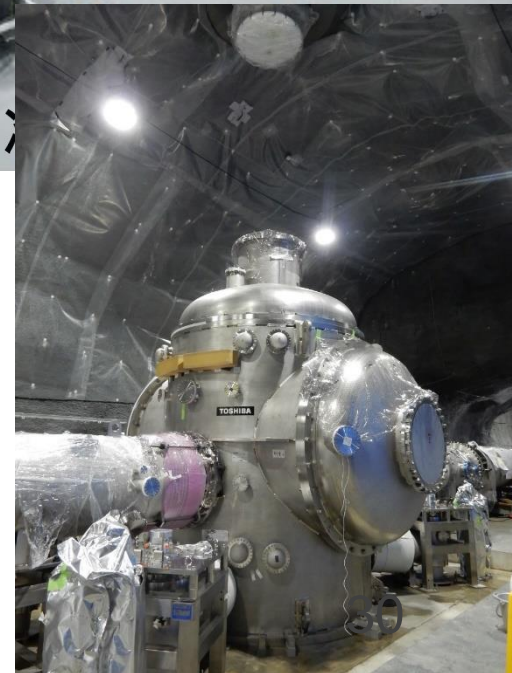
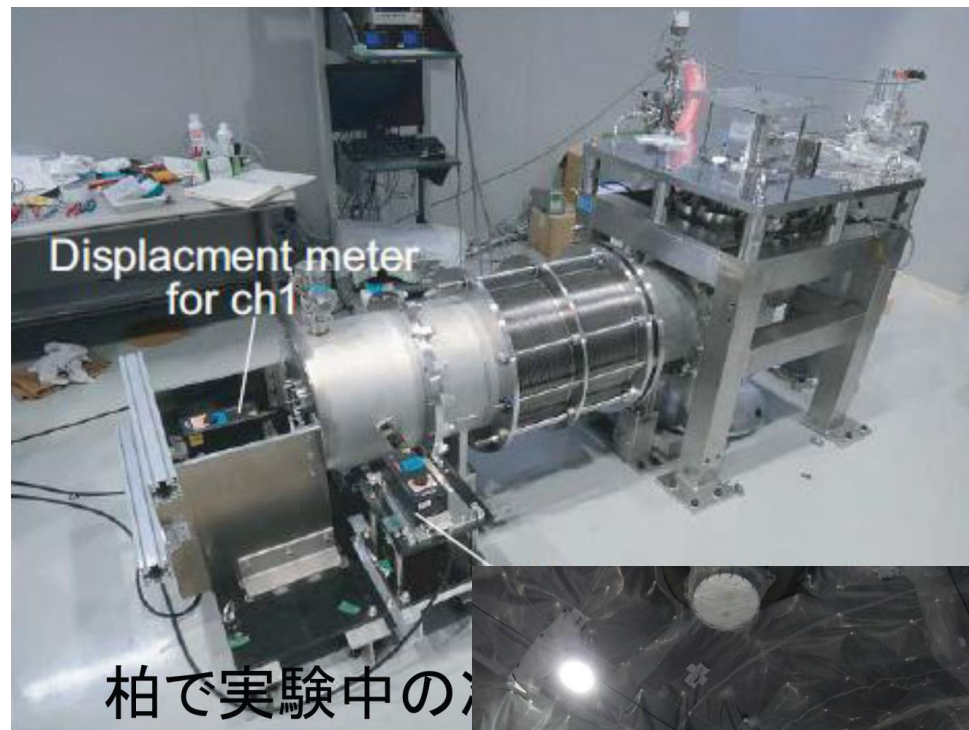
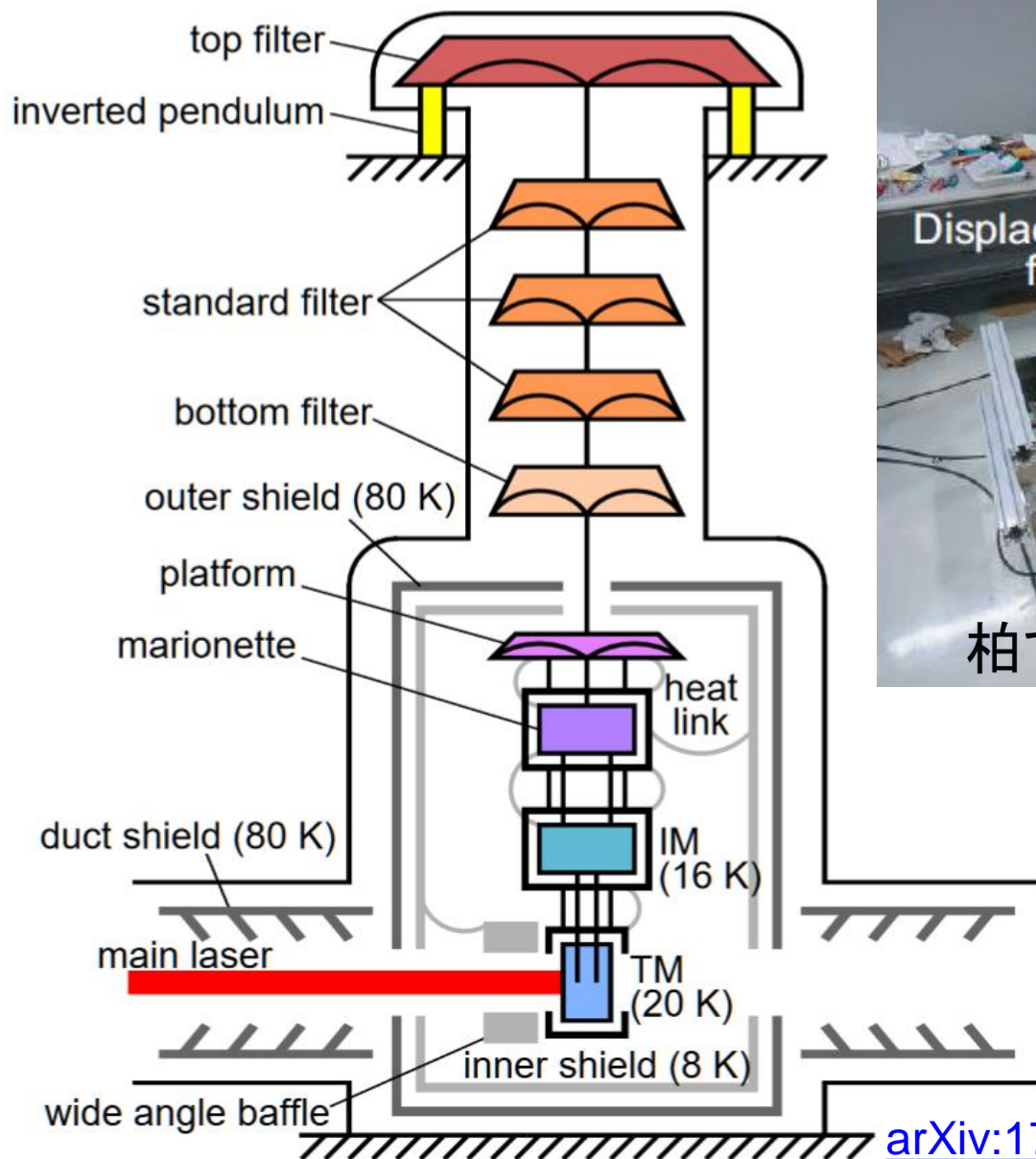


Challenges in Cryogenics

- KAGRA is the first km-scale GW detector to use cryogenics to reduce thermal noise
- Fused silica has large mechanical loss at cryogenic temperatures
 - **sapphire**
- Limitation in mirror size: 23 kg (small compared with aLIGO/AdV)
 - smaller beam size
 - worse quantum and thermal noise
- Thicker wire for **heat extraction**
 - larger suspension thermal noise
- Vibration of cryocoolers

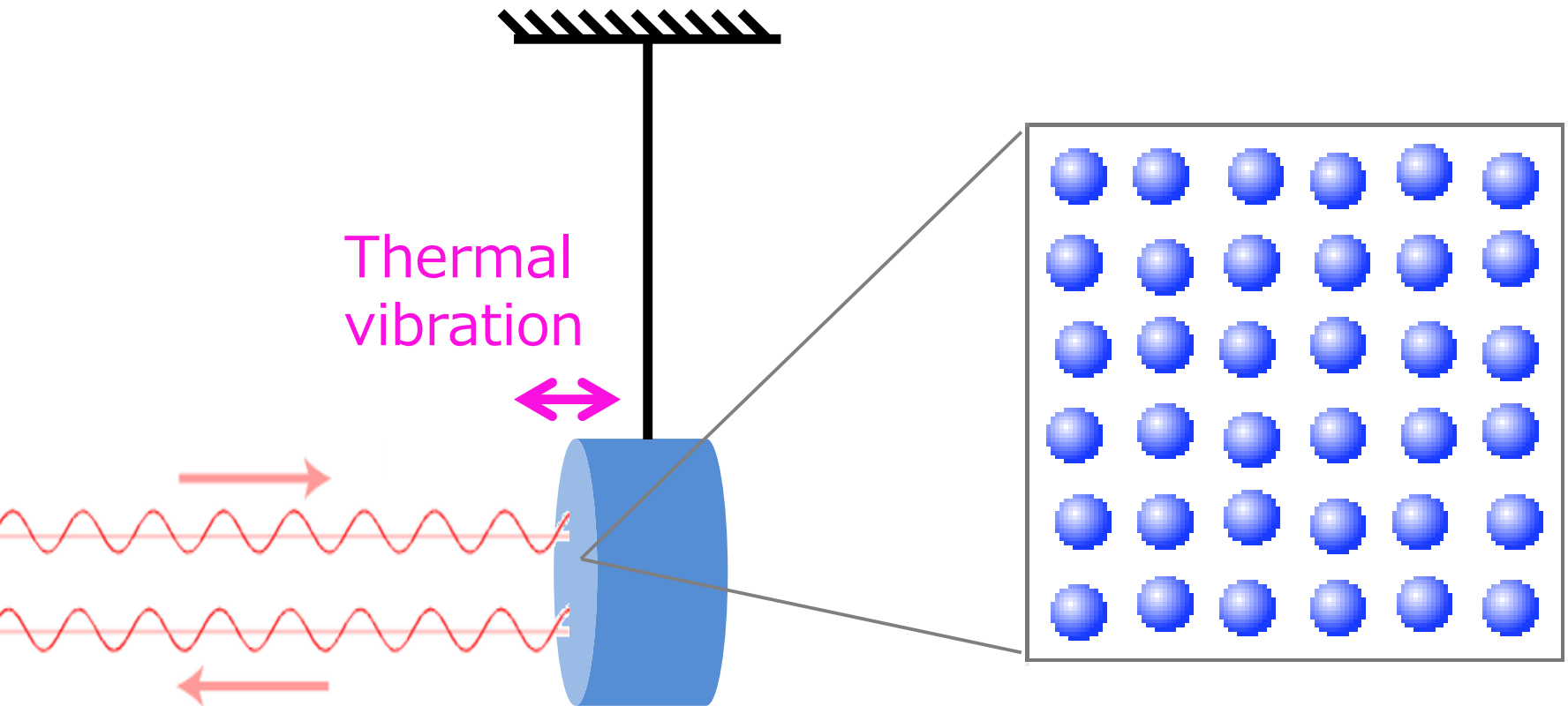


KAGRA Cryogenics



Mirror Thermal Noise

- Thermal vibration of mirror surface

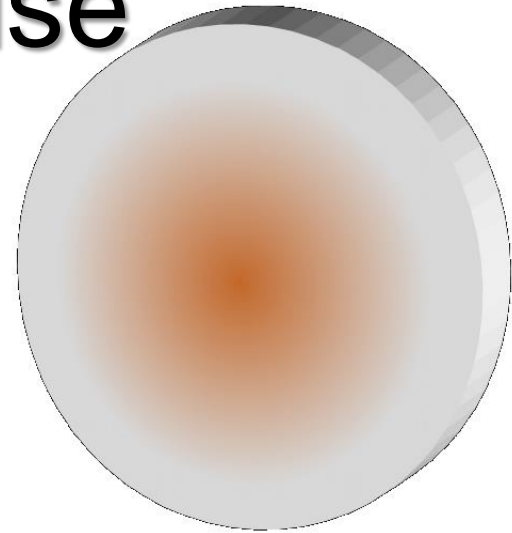


Mirror Thermal Noise

- Thermal vibration of mirror surface
- Structural damping, $\omega \ll \omega_0$

$$x_{\text{mir}}^2(\omega) = \frac{4k_{\text{B}}T}{m_{\text{eff}}\omega_0^2} \frac{\phi}{\omega}$$

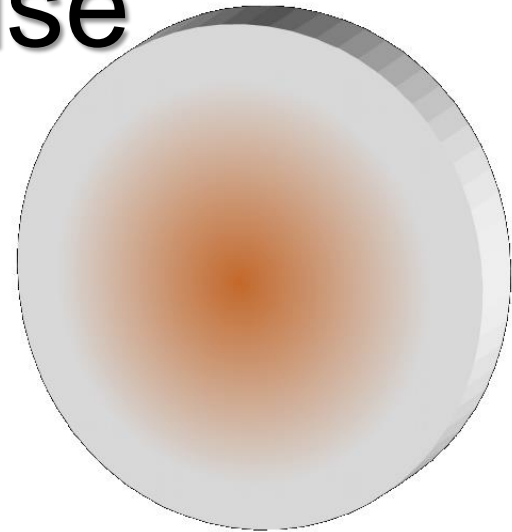
- m_{eff} is reduced mass
function of mirror aspect ratio, mirror radius and **beam radius** ratio, Poisson's ratio
- ω_0 is resonant frequency of vibration mode
 $\omega_0 \propto \sqrt{E}$
- You also have to sum up all the vibration modes



Mirror Thermal Noise

- Simple formula

$$x_{\text{mir}}^2(\omega) = \frac{4k_{\text{B}}T\phi}{\omega} \frac{1 - \sigma}{\sqrt{\pi}Ew}$$



- **To lower the thermal noise**

- lower temperature

- lower loss angle

- larger beam size (needs larger mirror)

$$x_{\text{mir}}(\omega) \propto \sqrt{T\phi}$$

$$x_{\text{mir}}(\omega) \propto 1/\sqrt{w}$$

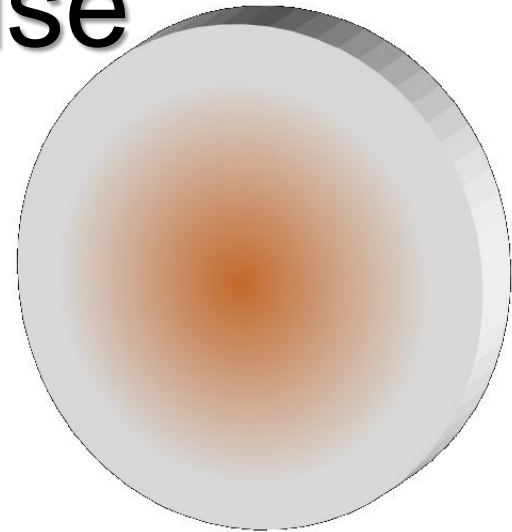
Mirror Thermal Noise

- Simple formula

$$x_{\text{mir}}^2(\omega) = \frac{4k_{\text{B}}T\phi}{\omega} \frac{1 - \sigma}{\sqrt{\pi}Ew}$$

- Calculate mirror thermal noise for fused silica ($E = 73 \text{ GPa}$, $\sigma = 0.17$, $\phi = 1\text{e-}6$)
 $w = 5 \text{ cm}$, $T = 300 \text{ K}$, at 100 Hz

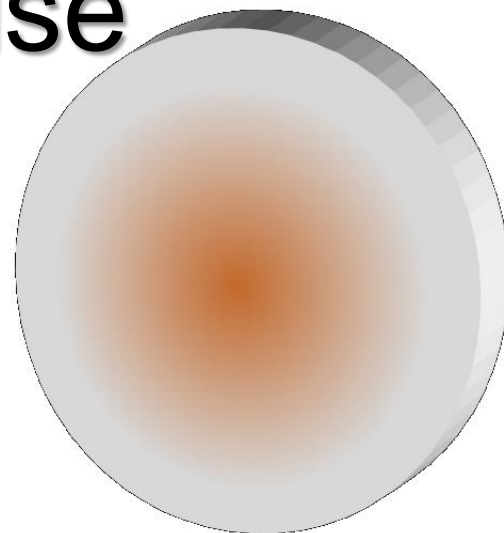
$$k_{\text{B}} = 1.38 \times 10^{-23} \text{ J/K}$$



Mirror Thermal Noise

- Simple formula

$$x_{\text{mir}}^2(\omega) = \frac{4k_{\text{B}}T\phi}{\omega} \frac{1 - \sigma}{\sqrt{\pi}Ew}$$



- Calculate mirror thermal noise for fused silica ($E = 73 \text{ GPa}$, $\sigma = 0.17$, $\phi = 1\text{e-}6$)
 $w = 5 \text{ cm}$, $T = 300 \text{ K}$, at 100 Hz

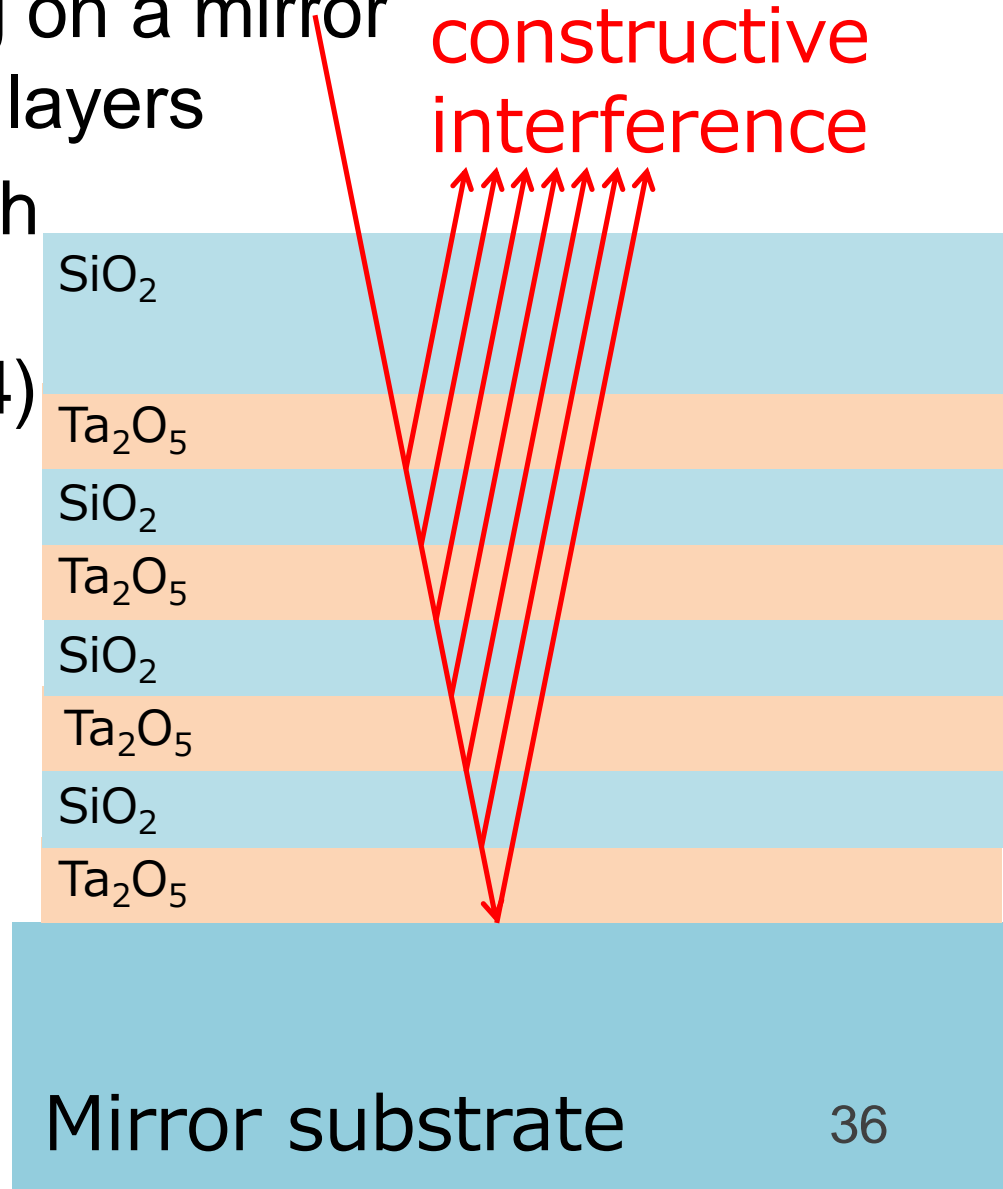
$$k_{\text{B}} = 1.38 \times 10^{-23} \text{ J/K}$$

$$x_{\text{mir}}(\omega) = 5.8 \times 10^{-20} \left(\frac{100 \text{ Hz}}{f} \right)^{1/2} \text{ m}/\sqrt{\text{Hz}}$$

Sufficient for GW detection!

Coating Thermal Noise

- High reflective coating on a mirror
 $\lambda/4$ thick alternative layers
- Active area of research
due to **low loss angle**
($\varphi \sim 1e-4$)



Mirror substrate

Coating Thermal Noise

- Formula (N. Nakagawa+, [PRD 65, 102001 \(2002\)](#))

$$x_{\text{coat}}^2(\omega) = \frac{4k_{\text{B}}T\phi}{\omega} \frac{2d_{\text{co}}(1 + \sigma_{\text{co}})(1 - 2\sigma_{\text{co}})}{\pi E\omega^2}$$

- **To lower the thermal noise**

- lower temperature

- lower loss angle

- larger beam radius (needs larger mirror)

$$x_{\text{coat}}(\omega) \propto 1/w$$

$$x_{\text{coat}}(\omega) \propto \sqrt{T\phi}$$

Coating Thermal Noise

- Formula (N. Nakagawa+, [PRD 65, 102001 \(2002\)](#))

$$x_{\text{coat}}^2(\omega) = \frac{4k_{\text{B}}T\phi}{\omega} \frac{2d_{\text{co}}(1 + \sigma_{\text{co}})(1 - 2\sigma_{\text{co}})}{\pi E w^2}$$

- Calculate coating thermal noise for silica/tantala coating ($E = 72 \text{ Gpa}$, $\sigma = 0.17$, $\phi = 4\text{e-}4$)
 $d = 10 \text{ um}$, $w = 5 \text{ cm}$, $T = 300 \text{ K}$, at 100 Hz

$$k_{\text{B}} = 1.38 \times 10^{-23} \text{ J/K}$$

Coating Thermal Noise

- Formula (N. Nakagawa+, [PRD 65, 102001 \(2002\)](#))

$$x_{\text{coat}}^2(\omega) = \frac{4k_{\text{B}}T\phi}{\omega} \frac{2d_{\text{co}}(1 + \sigma_{\text{co}})(1 - 2\sigma_{\text{co}})}{\pi E\omega^2}$$

- Calculate coating thermal noise for silica/tantala coating ($E = 72 \text{ Gpa}$, $\sigma = 0.17$, $\phi = 4\text{e-}4$)
 $d = 10 \text{ um}$, $w = 5 \text{ cm}$, $T = 300 \text{ K}$, at 100 Hz

$$k_{\text{B}} = 1.38 \times 10^{-23} \text{ J/K}$$

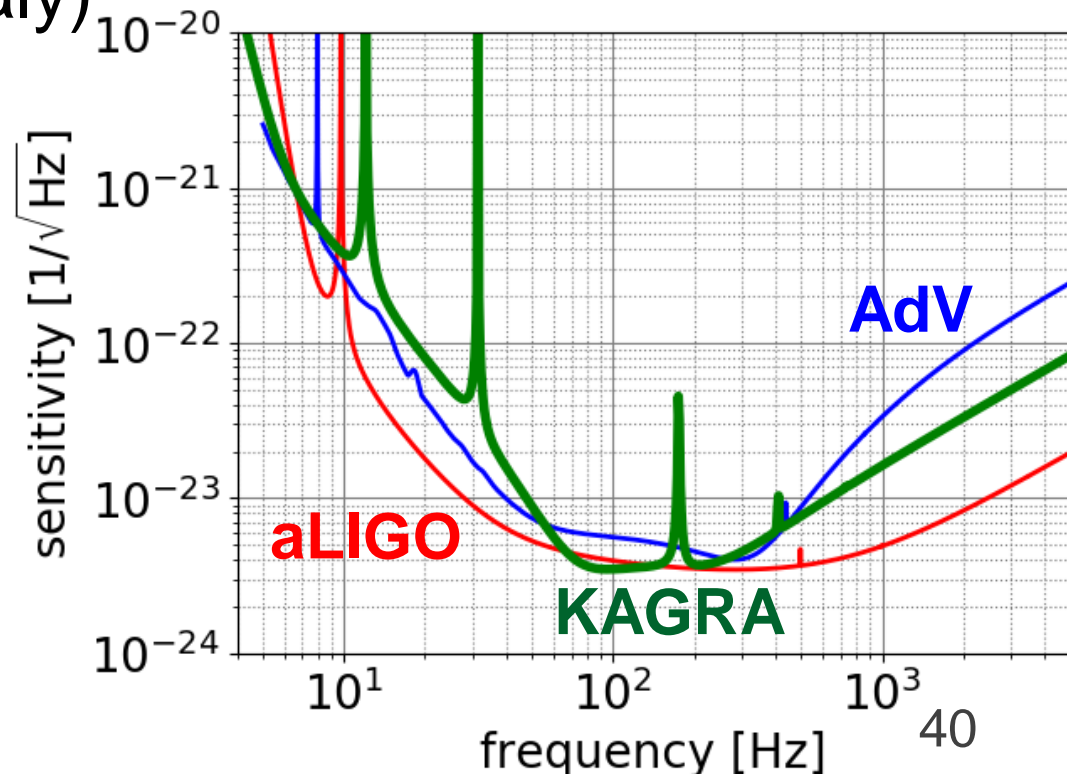
$$x_{\text{coat}}(\omega) = 1.7 \times 10^{-20} \left(\frac{100 \text{ Hz}}{f} \right)^{1/2} \text{ m}/\sqrt{\text{Hz}}$$

Sufficient for GW detection!

Mirror/Coating Thermal Noise in 2G

- Advanced LIGO (US)
w= 5.5 / 6.2 cm,
fused silica,
295 K, $\varphi \sim 1e-6$
- Advanced Virgo (Italy)
w= 4.9 / 5.8 cm,
fused silica,
295 K, $\varphi \sim 1e-6$
- KAGRA (Japan)
w= 3.5 / 3.5 cm,
sapphire,
22 K, $\varphi = 1e-8$

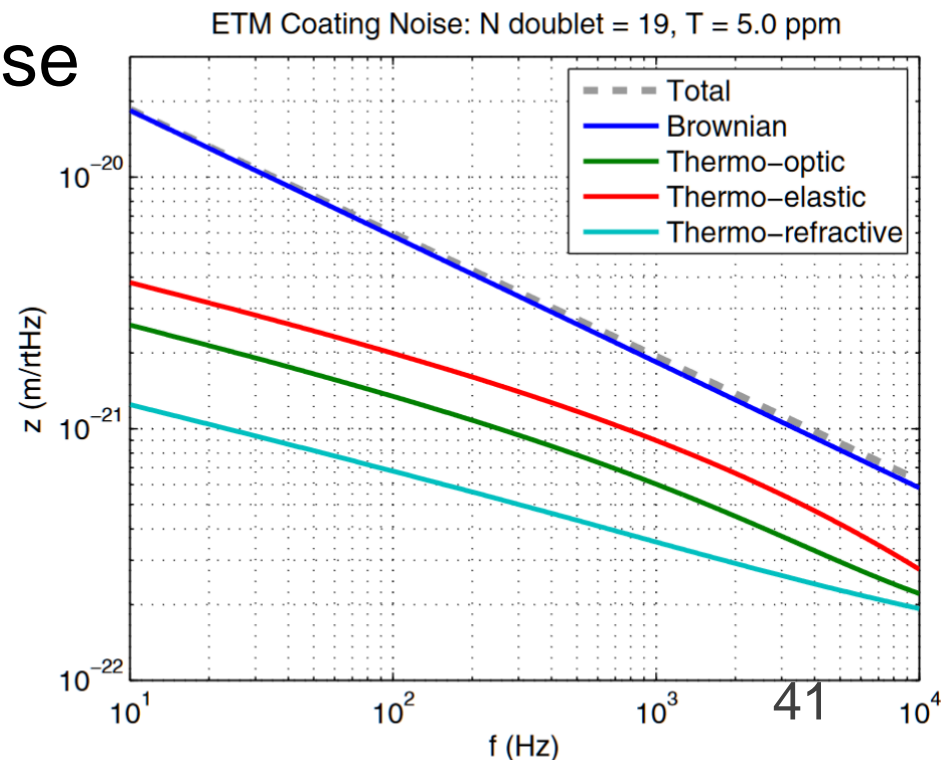
Mirror thermal noise
is not significant, but
coating thermal noise
is troublesome in 2G



Other Coating Thermal Noises

- From thermal dissipation in the coating leads to temperature fluctuation in the coating, which causes:
 - **Thermo-elastic** noise
thermal expansion
 - **Thermo-refractive** noise
refractive index change
- These two can cancel

M. Evans+, [PRD 78, 102003 \(2009\)](#)



Seismic Noise

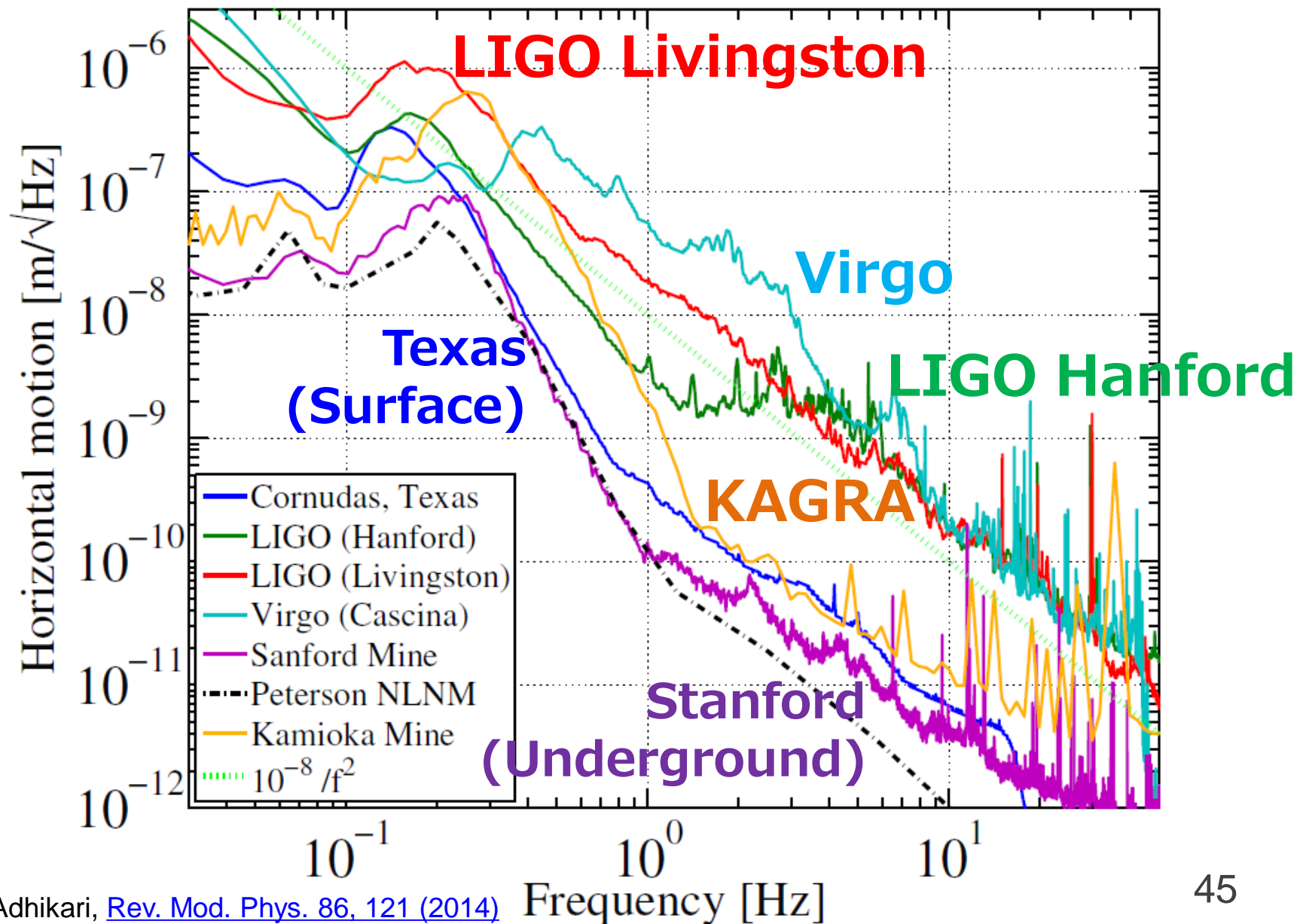
Seismic Vibration

- Ground vibrates even if there is no earthquakes
- Vibration level differs by
 - day and **night**
 - stormy day and **calm day**
 - urban place and **countryside**
 - surface and **underground**
- Site selection is very important for GW detectors

GW Detector Sites



Seismic Vibration Between Sites



Vibration Isolation

- Typical seismic noise (according to Saulson)

$$x_{\text{seis}}(\omega) = \begin{cases} 10^{-9} \text{ m}/\sqrt{\text{Hz}} & 1\text{-}10 \text{ Hz} \\ 10^{-9} (10 \text{ Hz}/f)^2 \text{ m}/\sqrt{\text{Hz}} & >10 \text{ Hz} \end{cases}$$

- Needs vibration attenuation by ~9 orders of magnitude
- Use **pendulums** to attenuate the ground vibration

Simple Pendulum

- Equation of motion

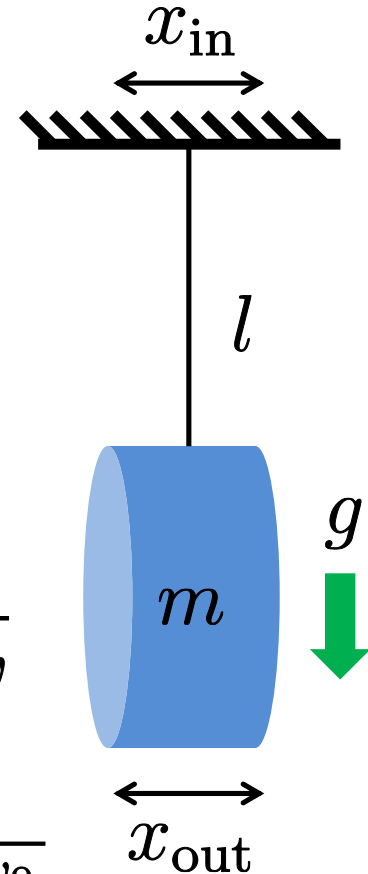
$$m\ddot{x}_{\text{out}} = -\frac{mg}{l}(x_{\text{out}} - x_{\text{in}}) - \gamma\dot{x}_{\text{out}}$$

- Transfer function from x_{in} to x_{out}

$$\begin{aligned} H(\omega) &= \frac{x_{\text{out}}(\omega)}{x_{\text{in}}(\omega)} = \frac{\frac{g}{l}}{-\omega^2 + \frac{g}{l} + i\frac{\gamma}{m}\omega} \\ &= \frac{\omega_0^2}{-\omega^2 + \omega_0^2 + i\frac{\omega\omega_0}{Q}} \end{aligned}$$

where

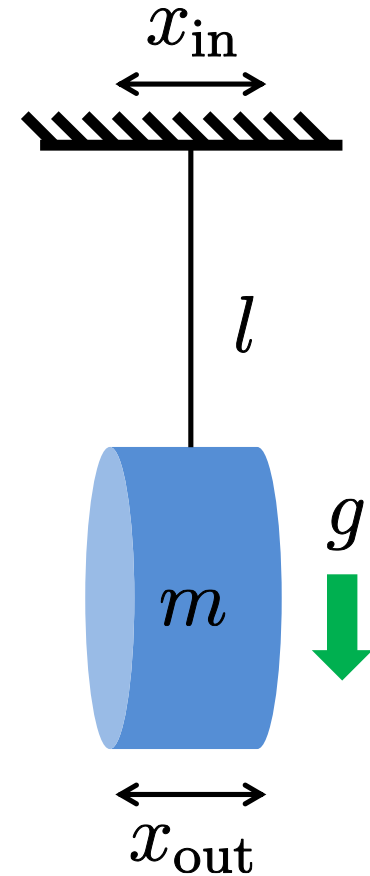
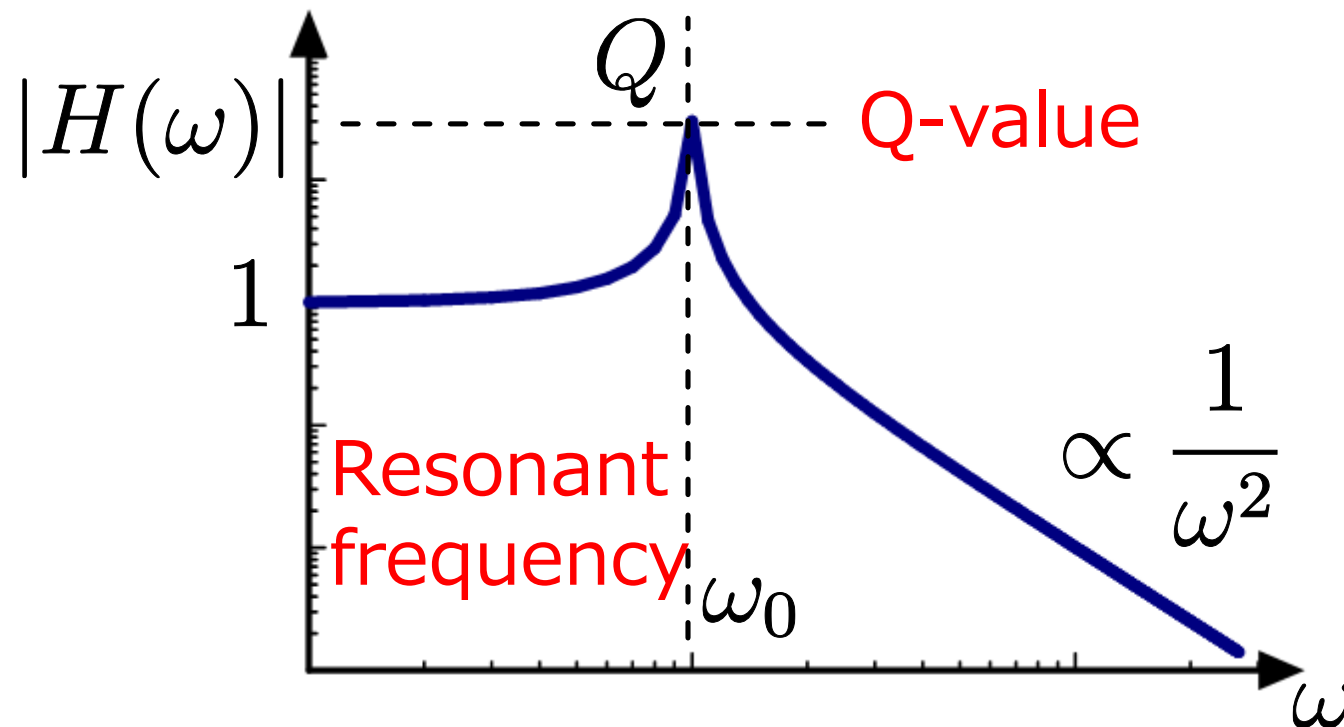
$$\omega_0 = \sqrt{\frac{g}{l}} \quad Q = \frac{m\omega_0}{\gamma}$$



Simple Pendulum

- Seismic attenuation ratio

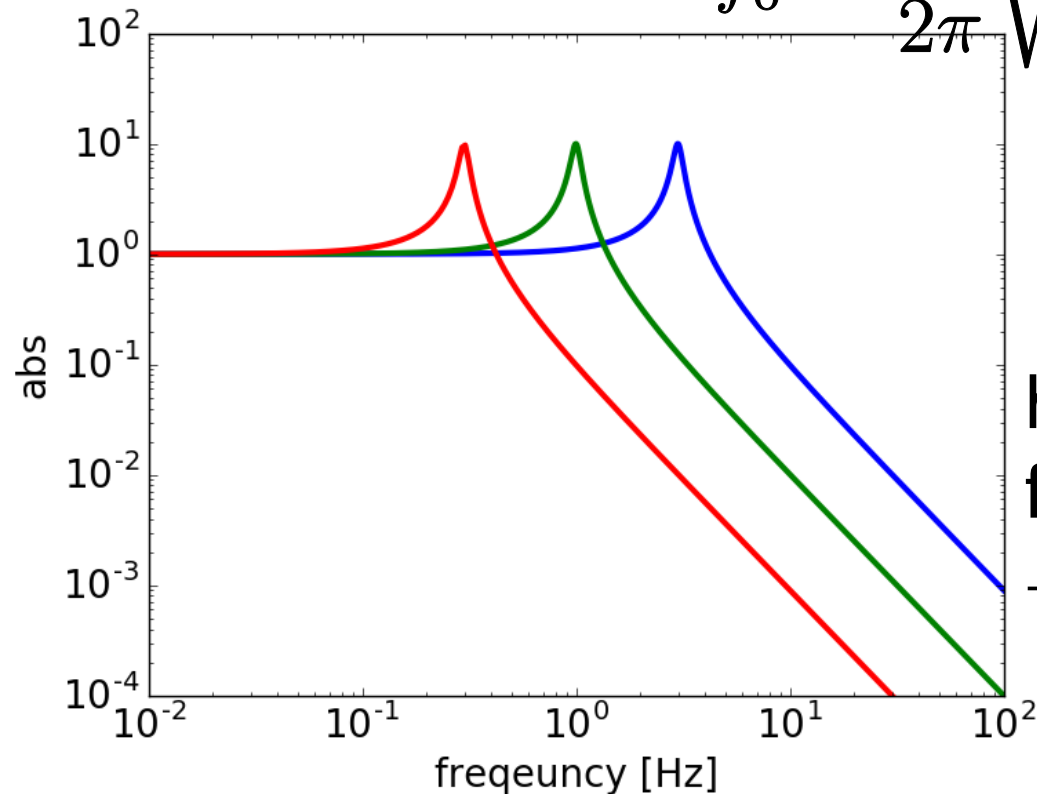
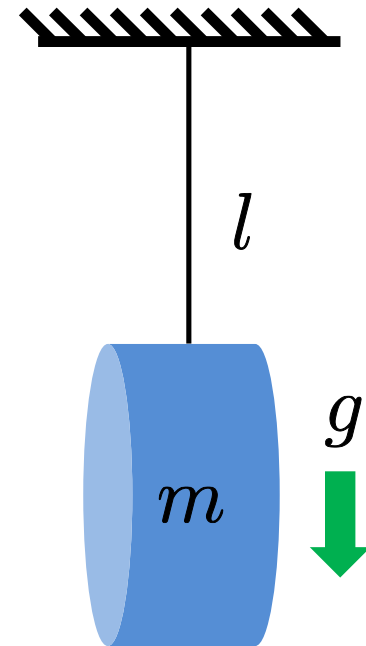
$$H(\omega) = \frac{\omega_0^2}{-\omega^2 + \omega_0^2 + i\frac{\omega\omega_0}{Q}}$$



Resonant Frequency

- **Longer suspension** gives lower resonant frequency, and thus better attenuation ratio at high frequencies

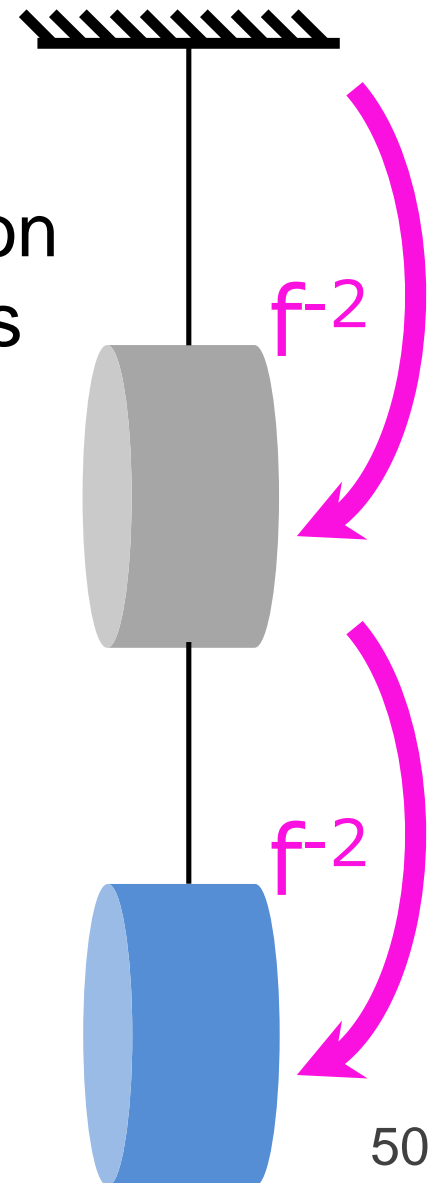
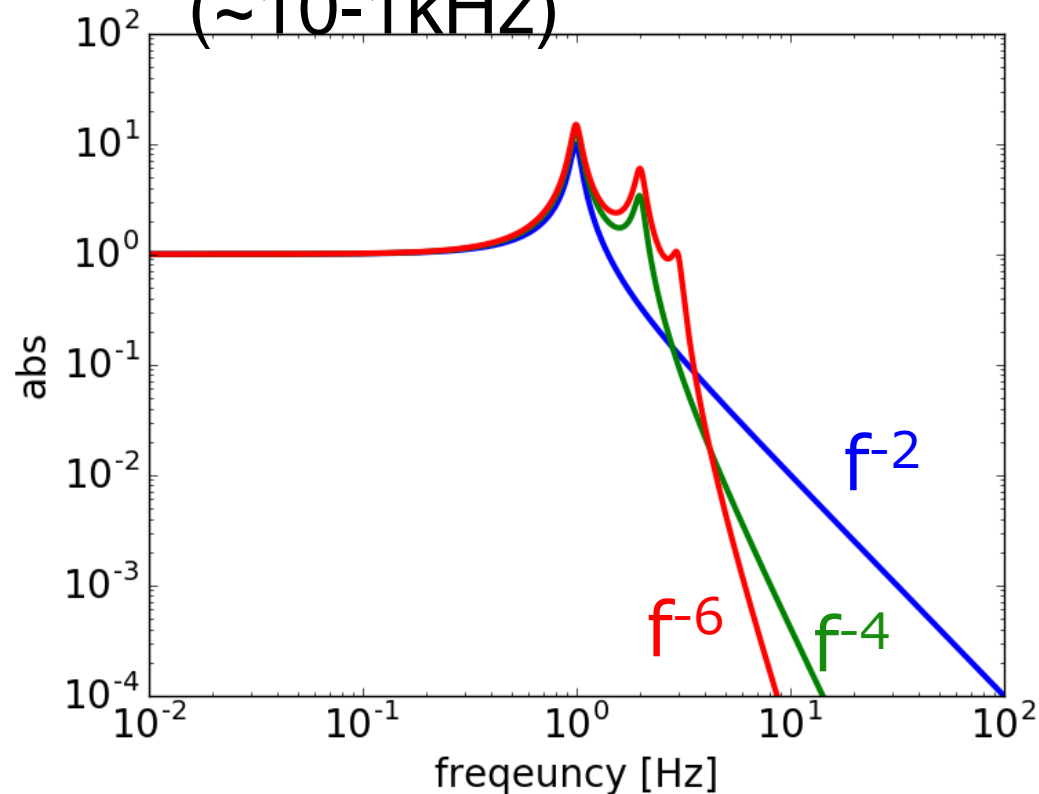
- $l = 1$ m gives $f_0 = \frac{1}{2\pi} \sqrt{\frac{g}{l}} \simeq 0.5$ Hz



hard to get low resonant frequency on Earth
→ space GW detectors

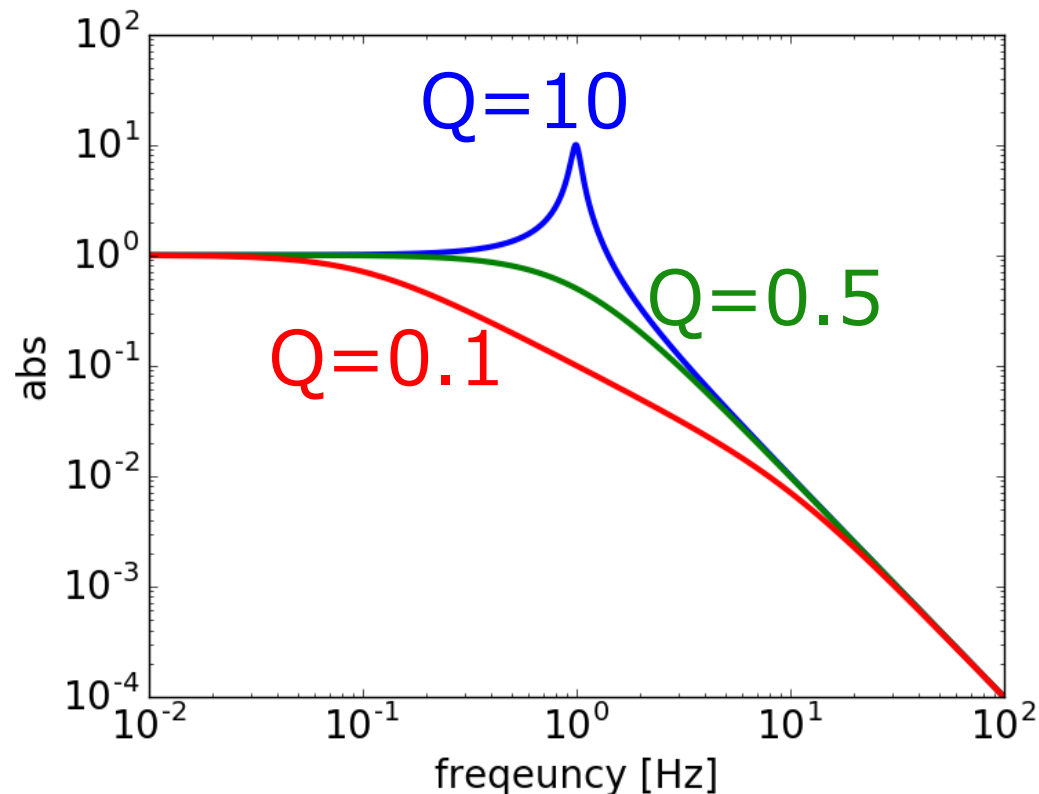
Multiple-Stage Pendulum

- n-stage pendulum has f^{-2n} attenuation at high frequencies
- Gives enough isolation at observation band of ground-based GW detectors (~ 10 - 1 kHz)



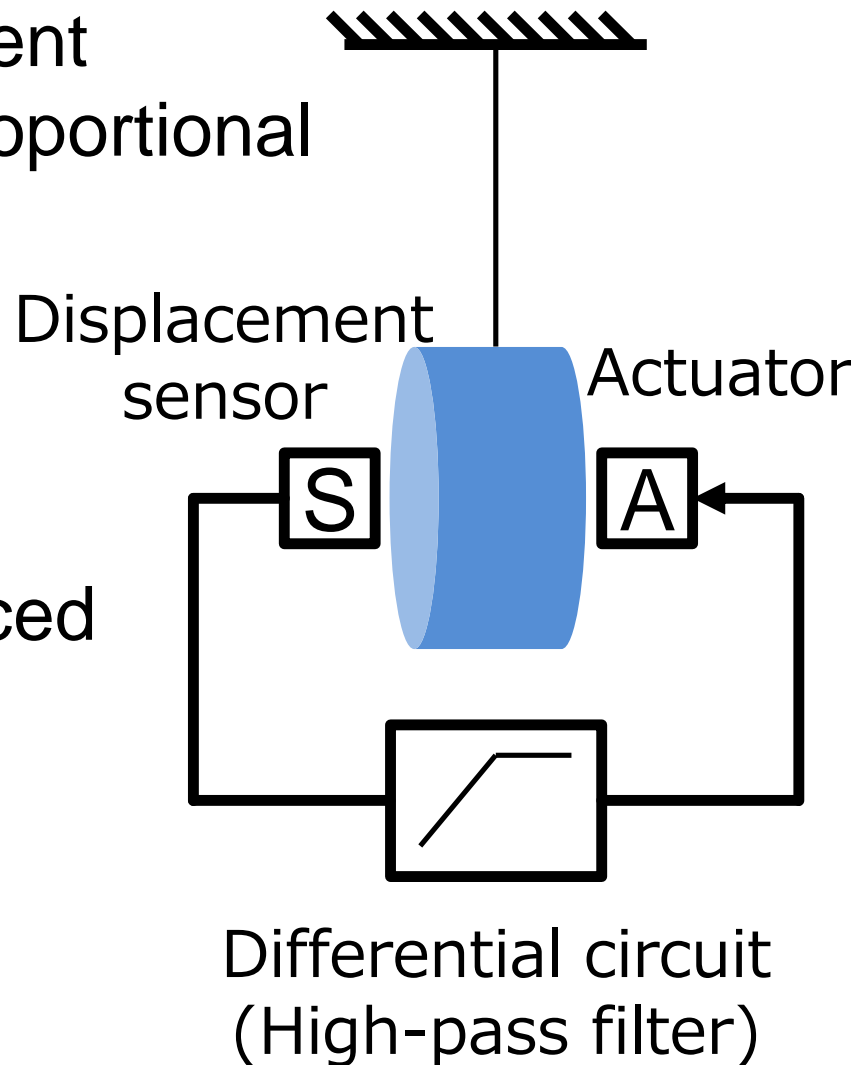
Pendulum Q-value

- Higher Q-value gives better thermal noise, but needs longer time it takes to calm down
- Very low Q-value is bad for seismic attenuation ($Q < 0.5$ is over damping)



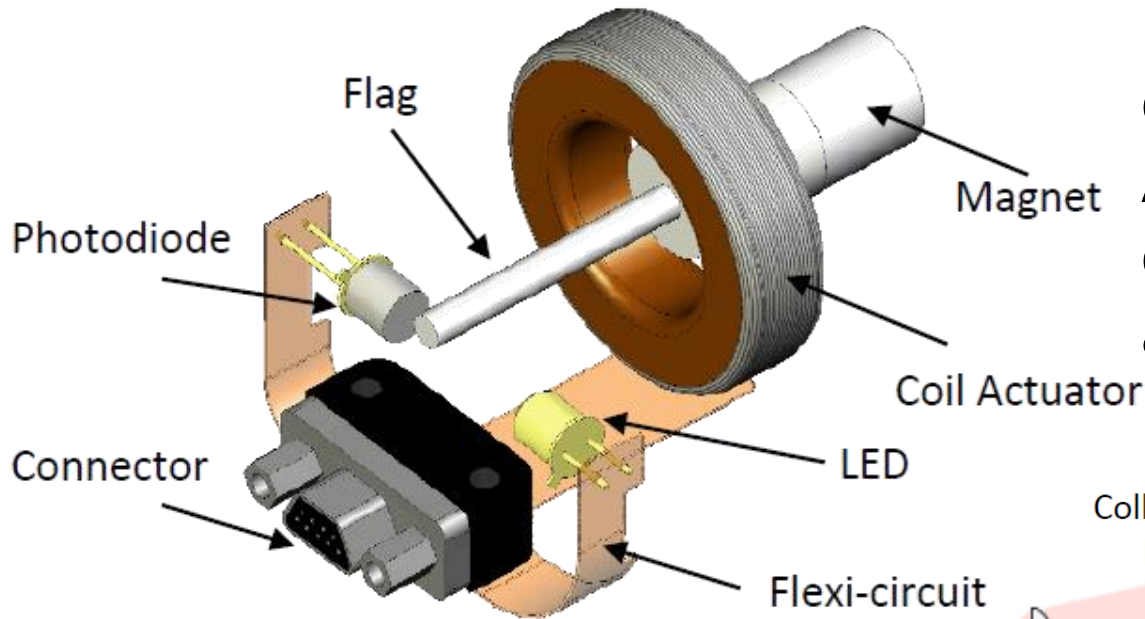
Active Damping

- Measure mirror displacement and give damping force proportional to mirror velocity using differential circuit
- **No degradation** in thermal noise
- Control noises are introduced circuit noise, magnetic noise, sensor noise, actuator noise.....



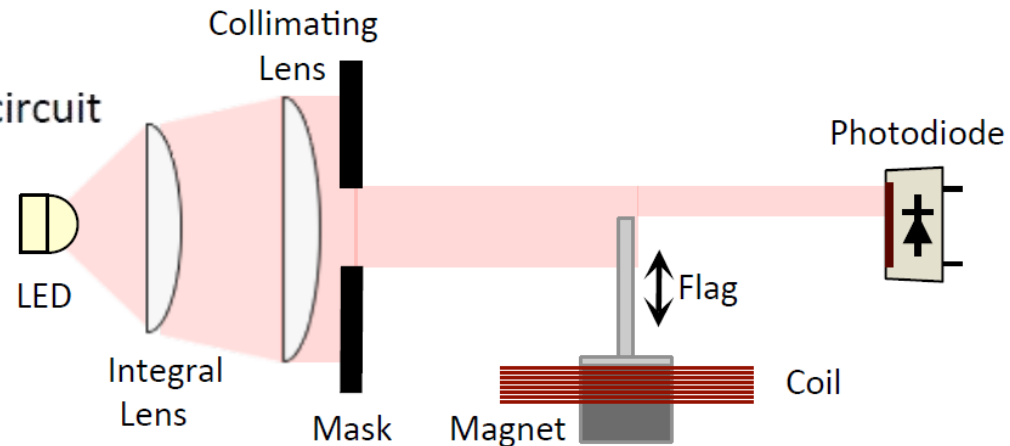
OSEM

- Optical Sensor ElectroMagnet

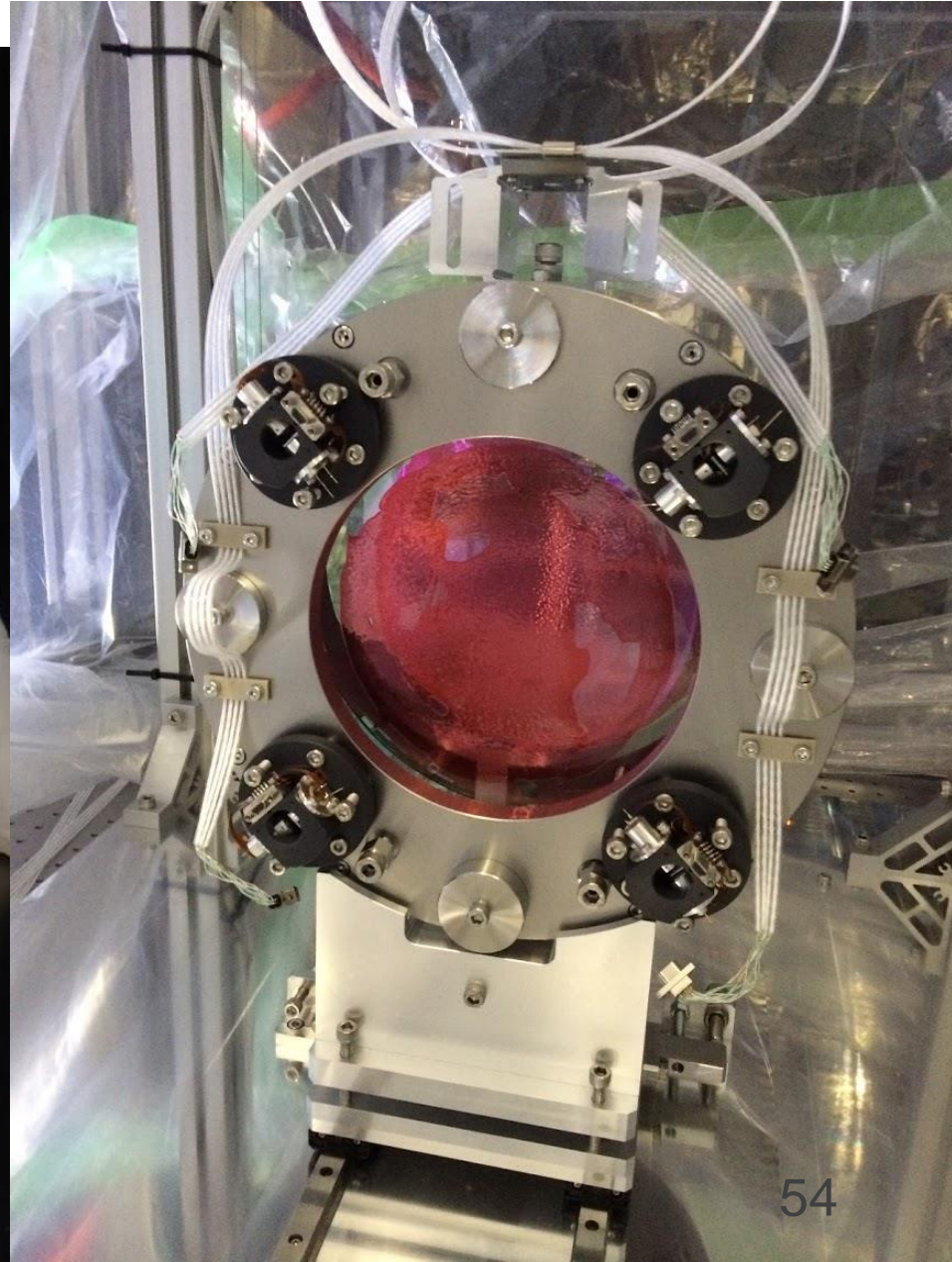
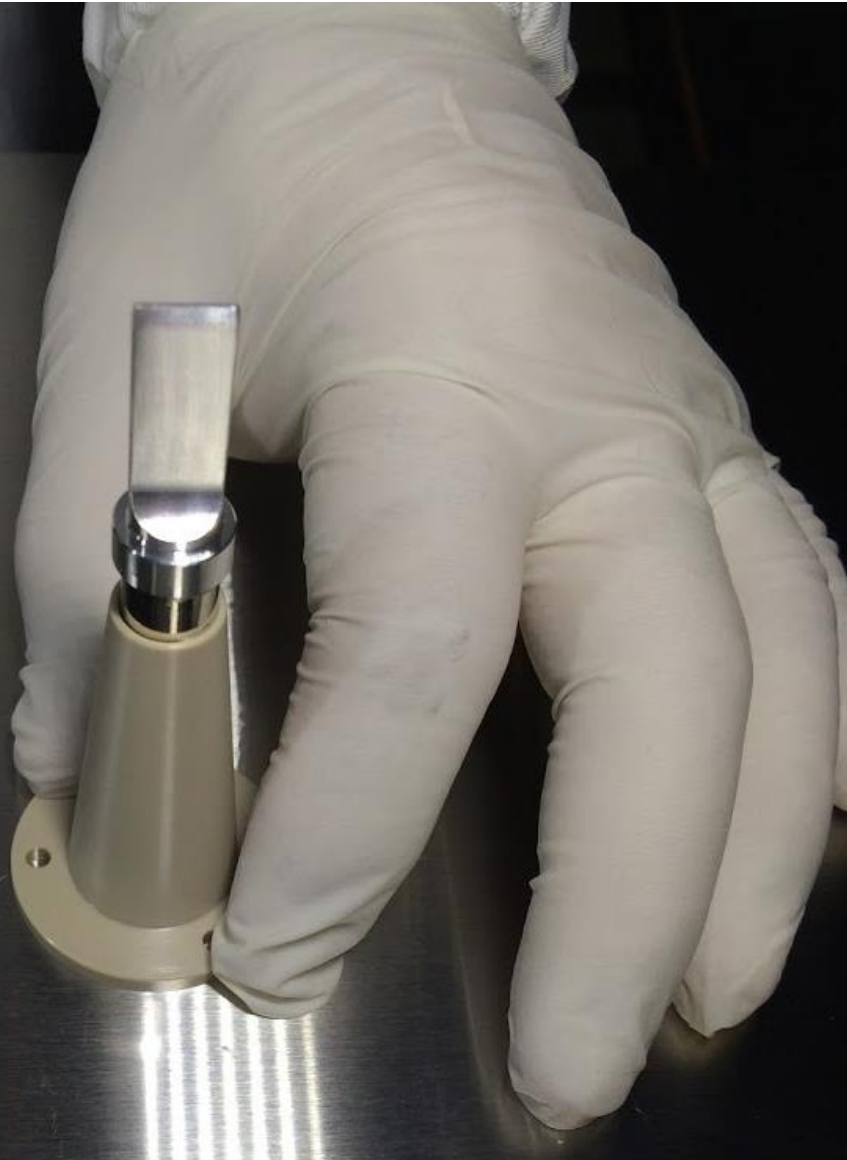


Magnets are attached onto the mirror. Actuation is done by controlling the current applied to the coils.

Mirror displacement is sensed by the amount of light shaded by the flags.

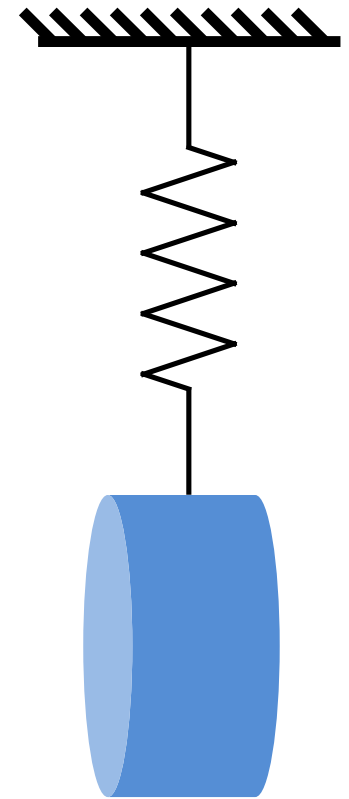


KAGRA OSEM



Vertical Vibration Isolation

- Vertical vibration isolation is also necessary since the beam axis is not perfectly horizontal



Low Frequency Vibration Isolation

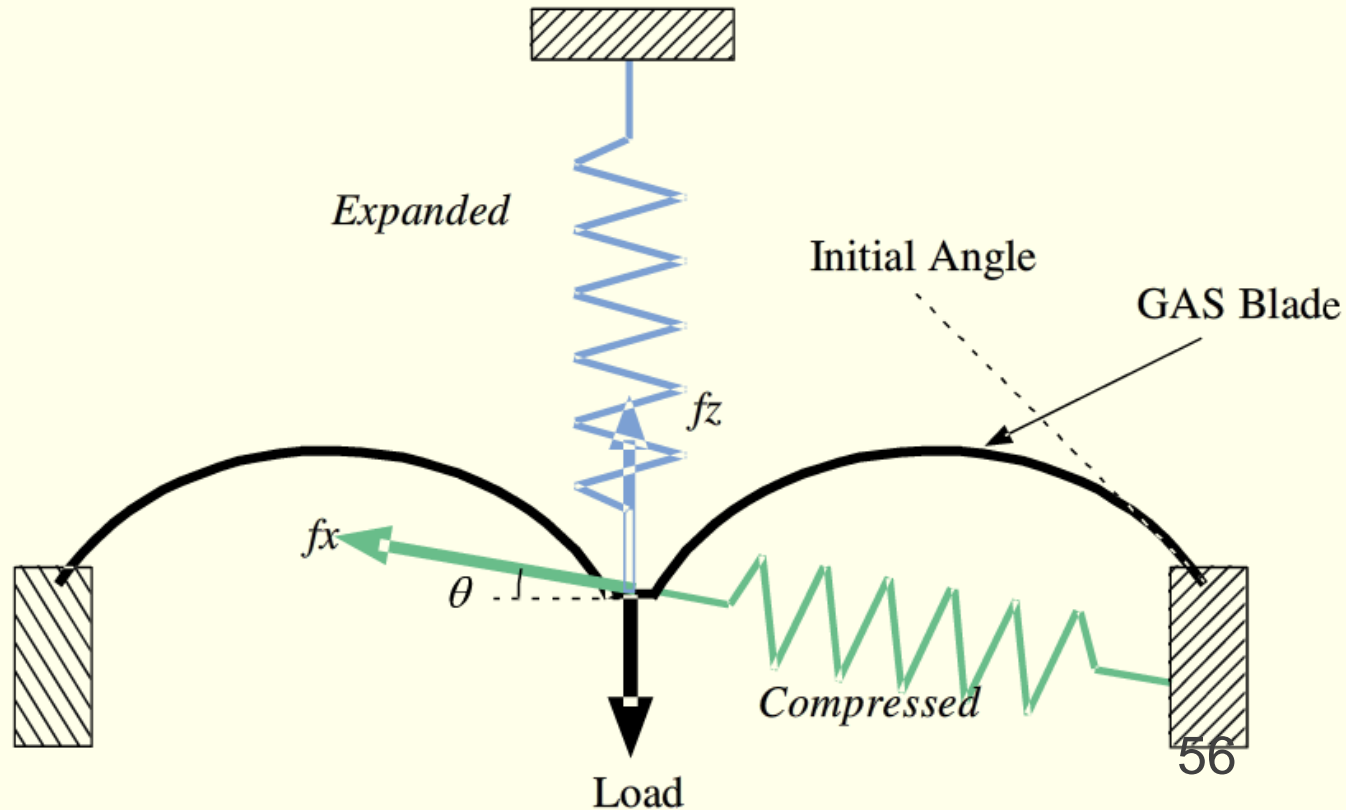
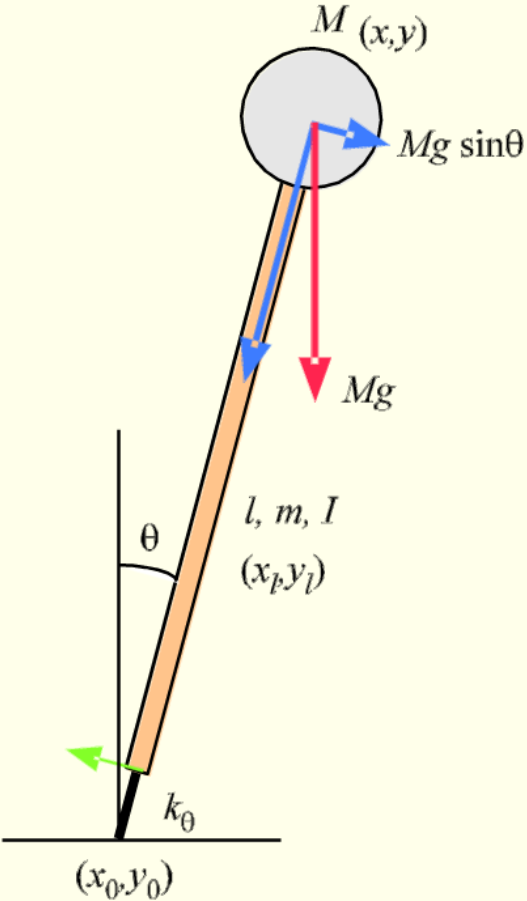
- Usual pendula are not practical for making resonant frequency low

$$f_0 = \frac{1}{2\pi} \sqrt{\frac{g}{l}}$$

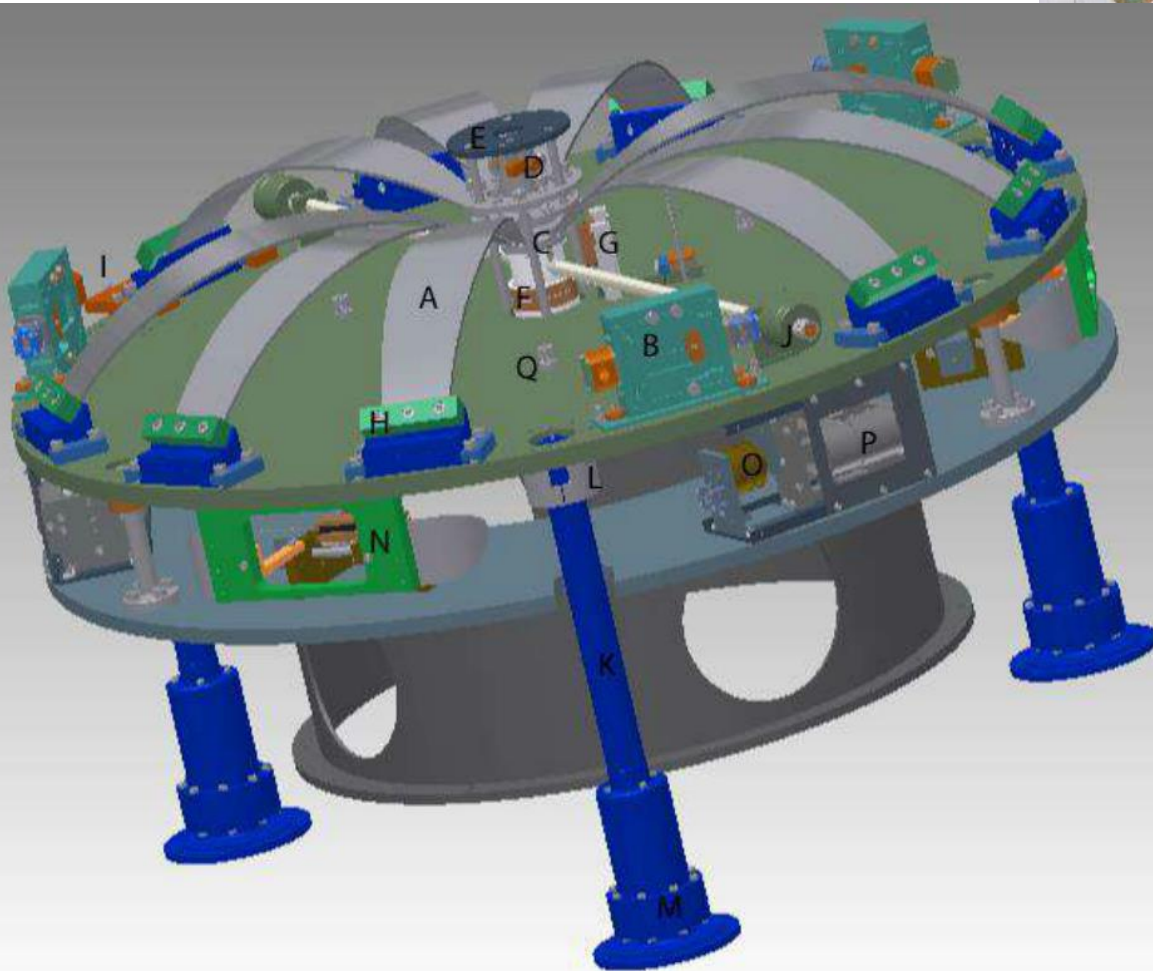
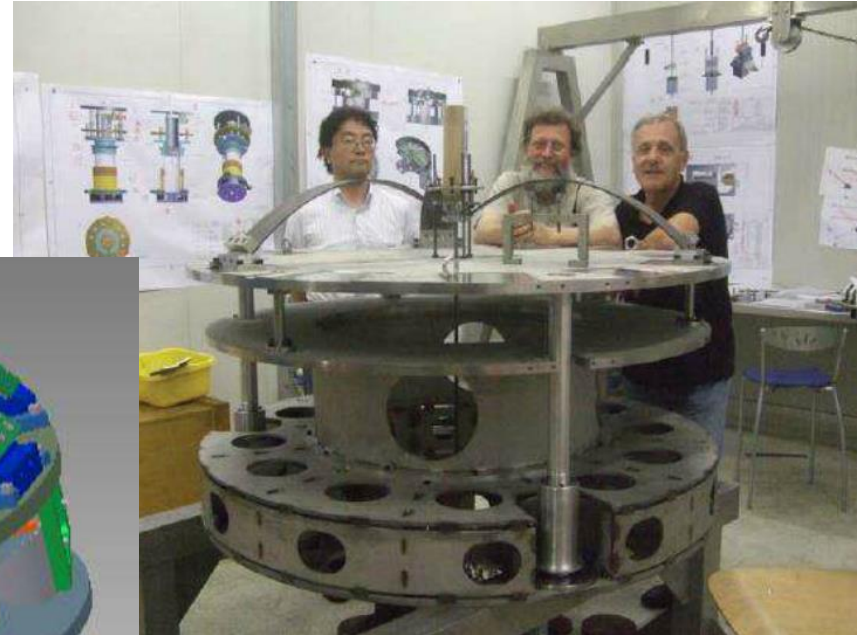
0.5 Hz for 1 m-long pendulum

Inverted pendulum

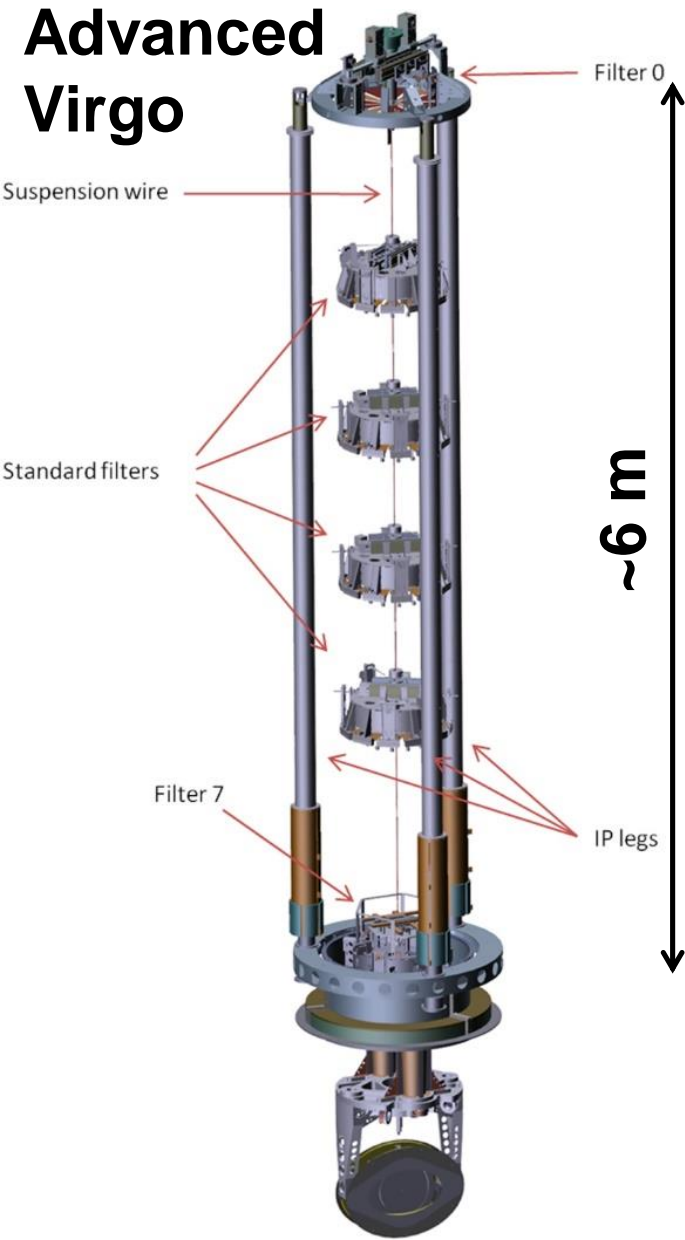
Geometric-Anti-Spring filter



Low Frequency Vibration Isolation



Vibration Isolation System in 2G

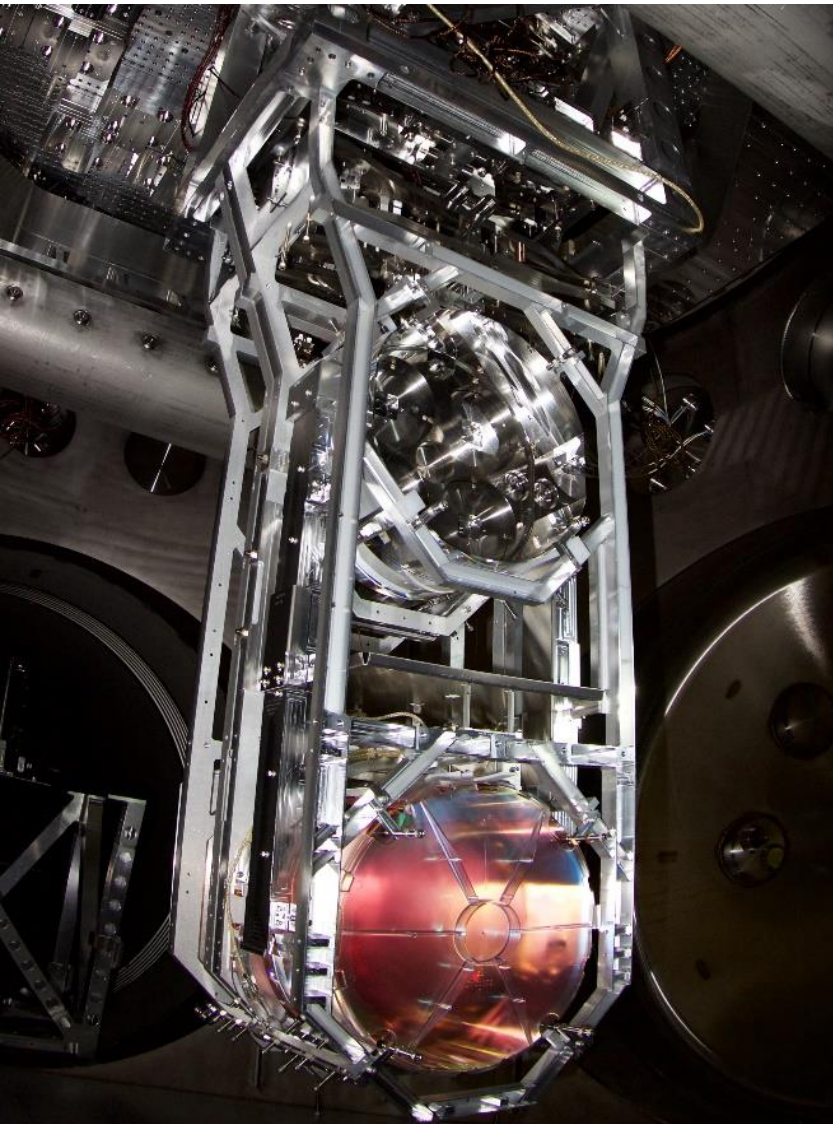


KAGRA (BS)



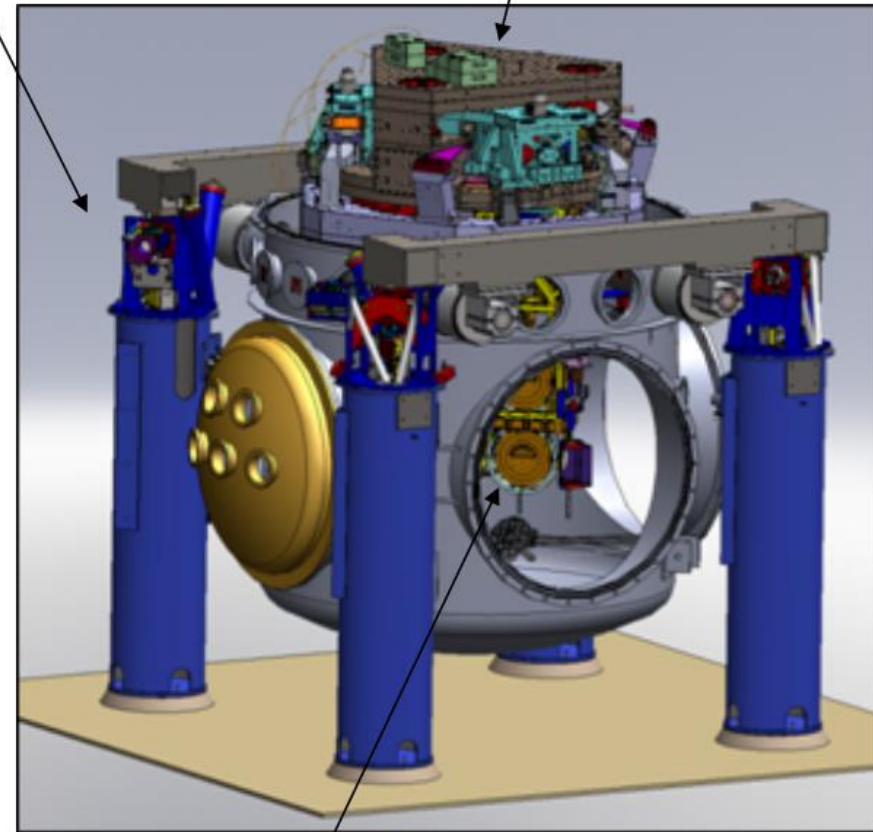
Vibration Isolation System in 2G

Advanced LIGO



hydraulic external pre-isolator (HEPI) (one stage of isolation)

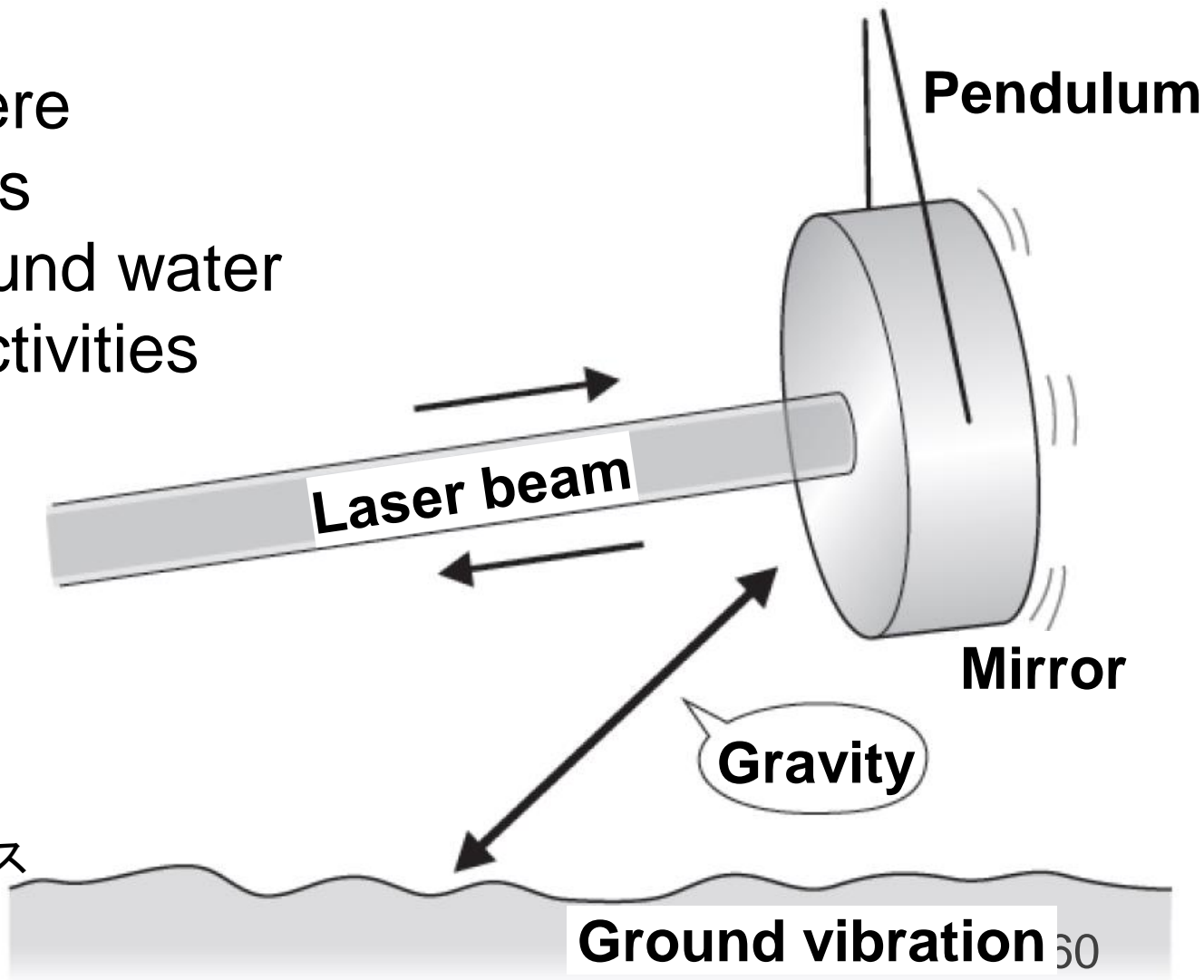
active isolation platform (2 stages of isolation)



quadruple pendulum (four stages of isolation) with monolithic silica final stage

Gravity Gradient Noise

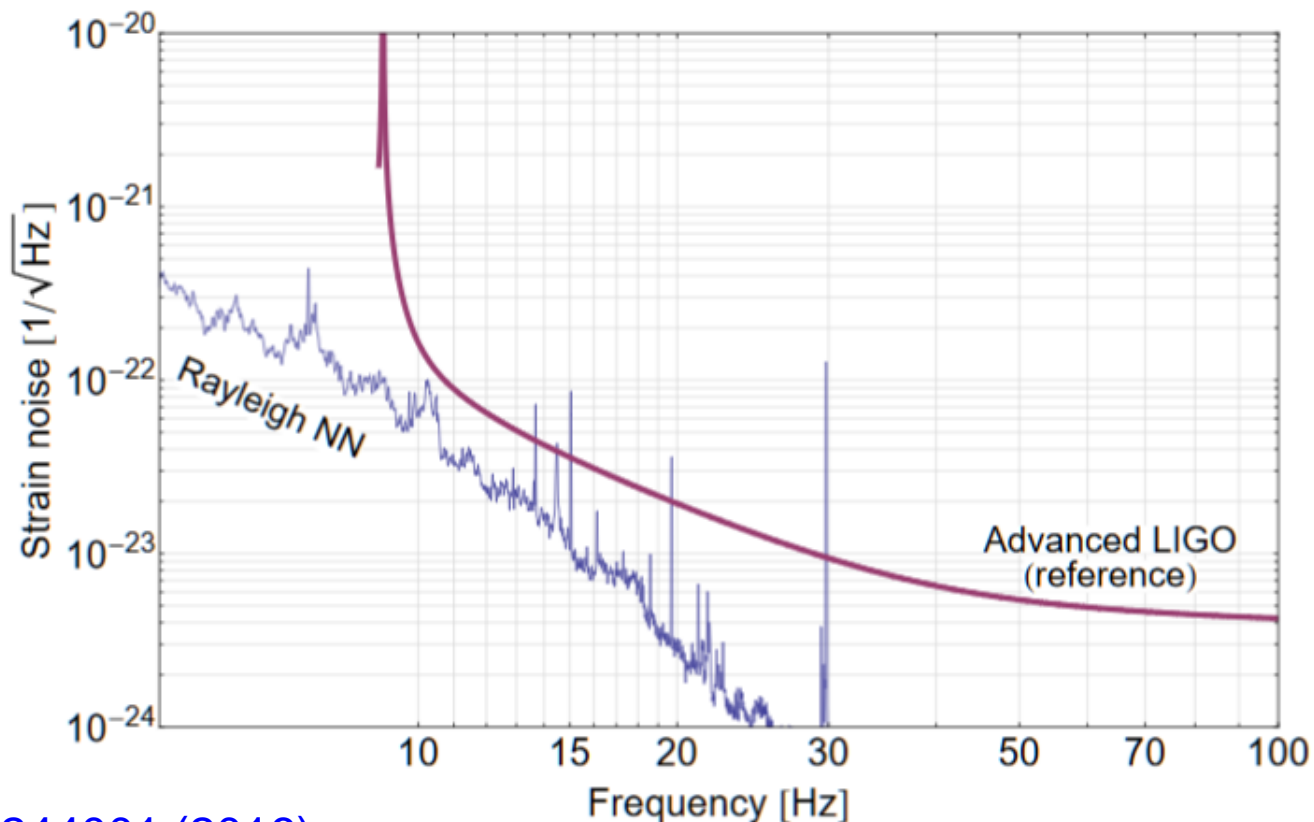
- Newtonian gravitational force acting on a mirror
 - ground
 - atmosphere
 - sea waves
 - underground water
 - human activities



Modified from
講談社ブルーバックス
『重力波とはなにか』
安東正樹著

Gravity Gradient Noise

- Newtonian gravitational force acting on a mirror
- Could be an issue for 2G

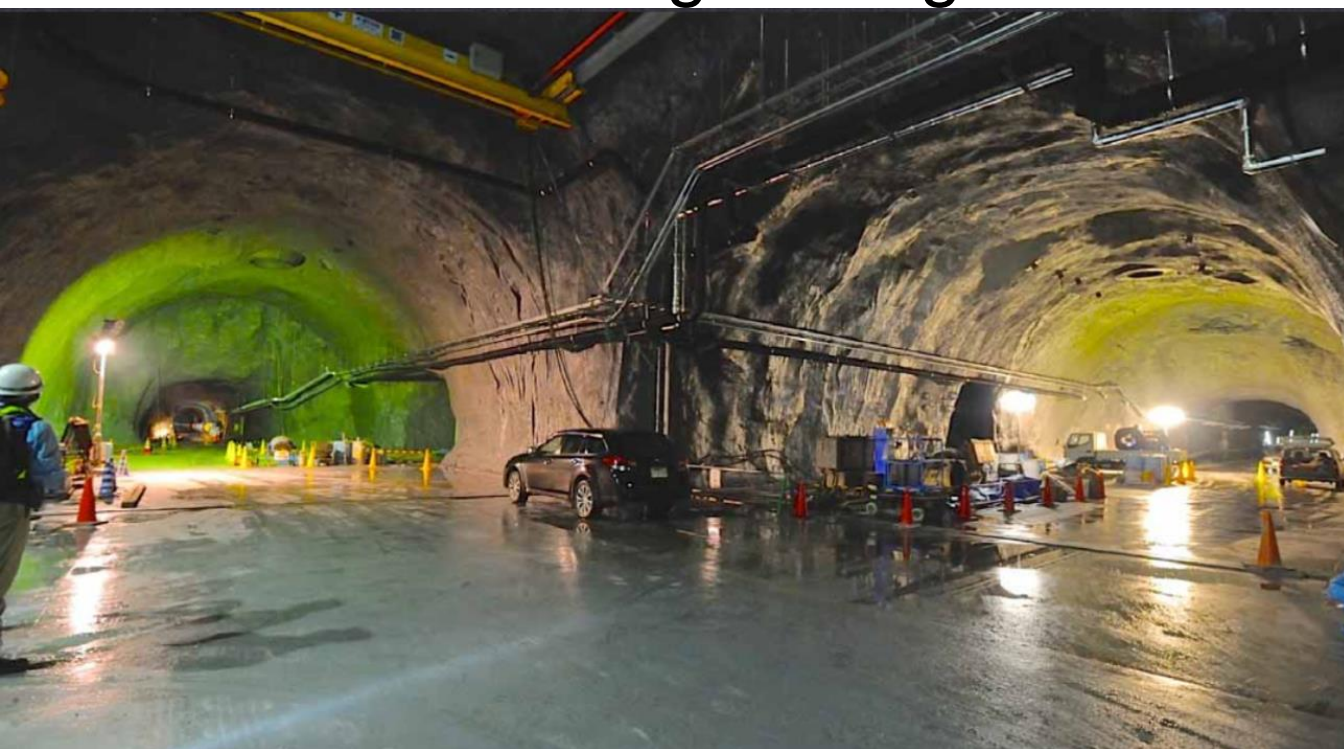


M. Coughlin+, [CQG 33 244001 \(2016\)](#)

FIG. 1: Predicted average Newtonian noise in Advanced LIGO.

Underground GW Detector

- **Underground** site gives lower seismic noise (and lower gravity gradient noise)
- **KAGRA** is the first km-scale underground detector
- Future GW project **Einstein Telescope** also considers using underground site



**KAGRA site
(March 2014)**

Einstein Telescope

- Triangular, 10 km, underground
- Xylophone configuration



LF detector with cryogenic and low power
 HF detector with room temperature and high power



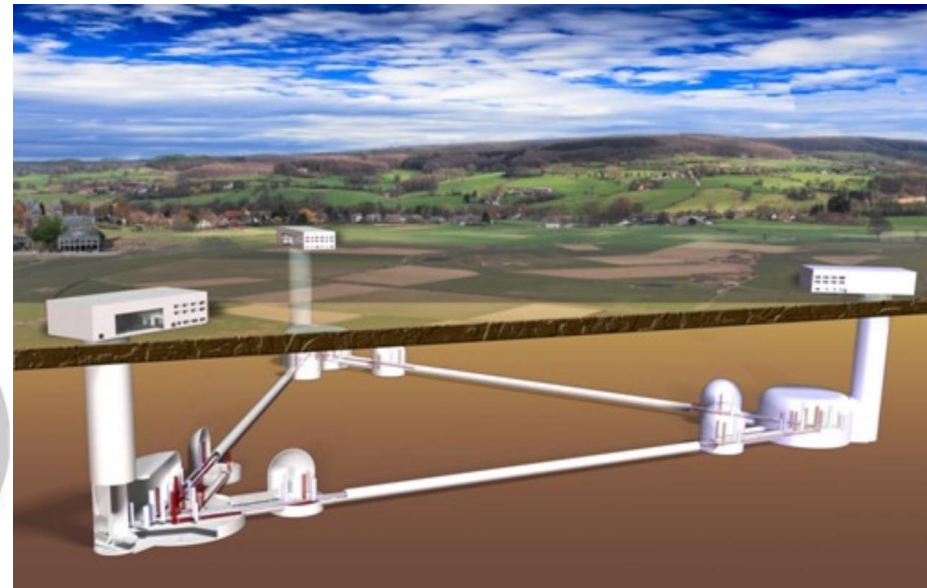
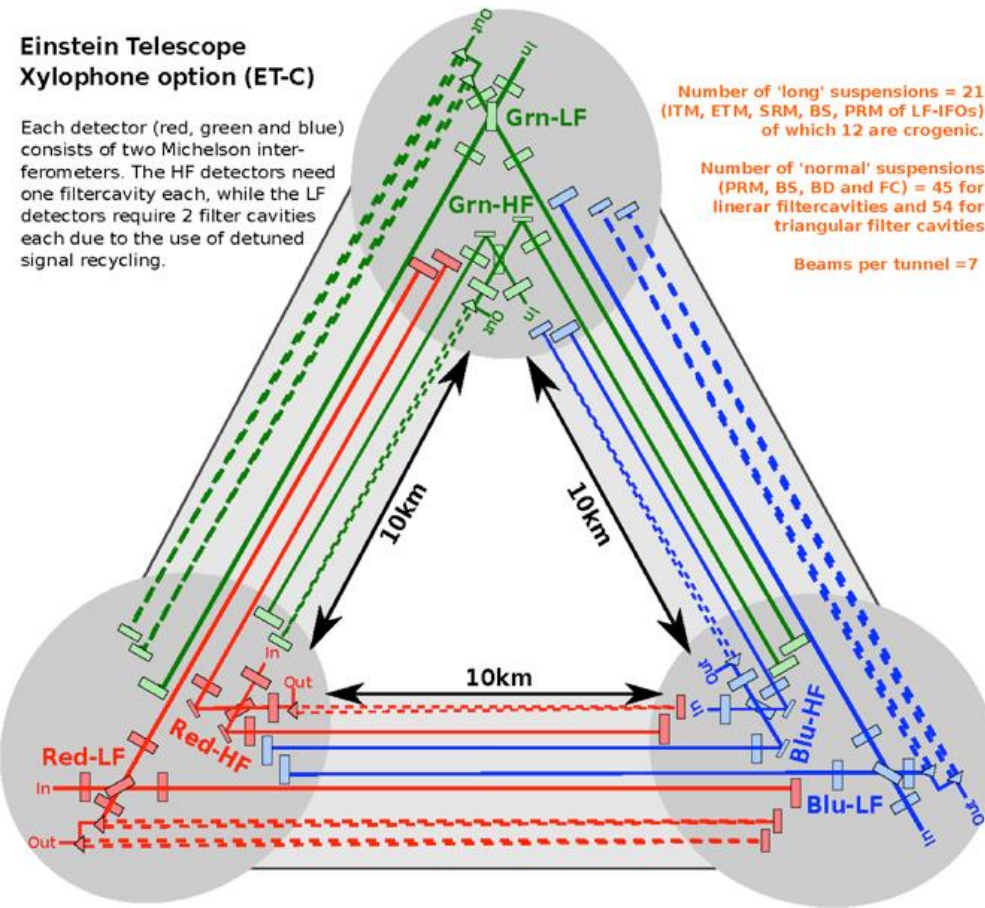
Einstein Telescope Xylophone option (ET-C)

Each detector (red, green and blue) consists of two Michelson interferometers. The HF detectors need one filtercavity each, while the LF detectors require 2 filter cavities each due to the use of detuned signal recycling.

Number of 'long' suspensions = 21
 (ITM, ETM, SRM, BS, PRM of LF-IFOs)
 of which 12 are cryogenic.

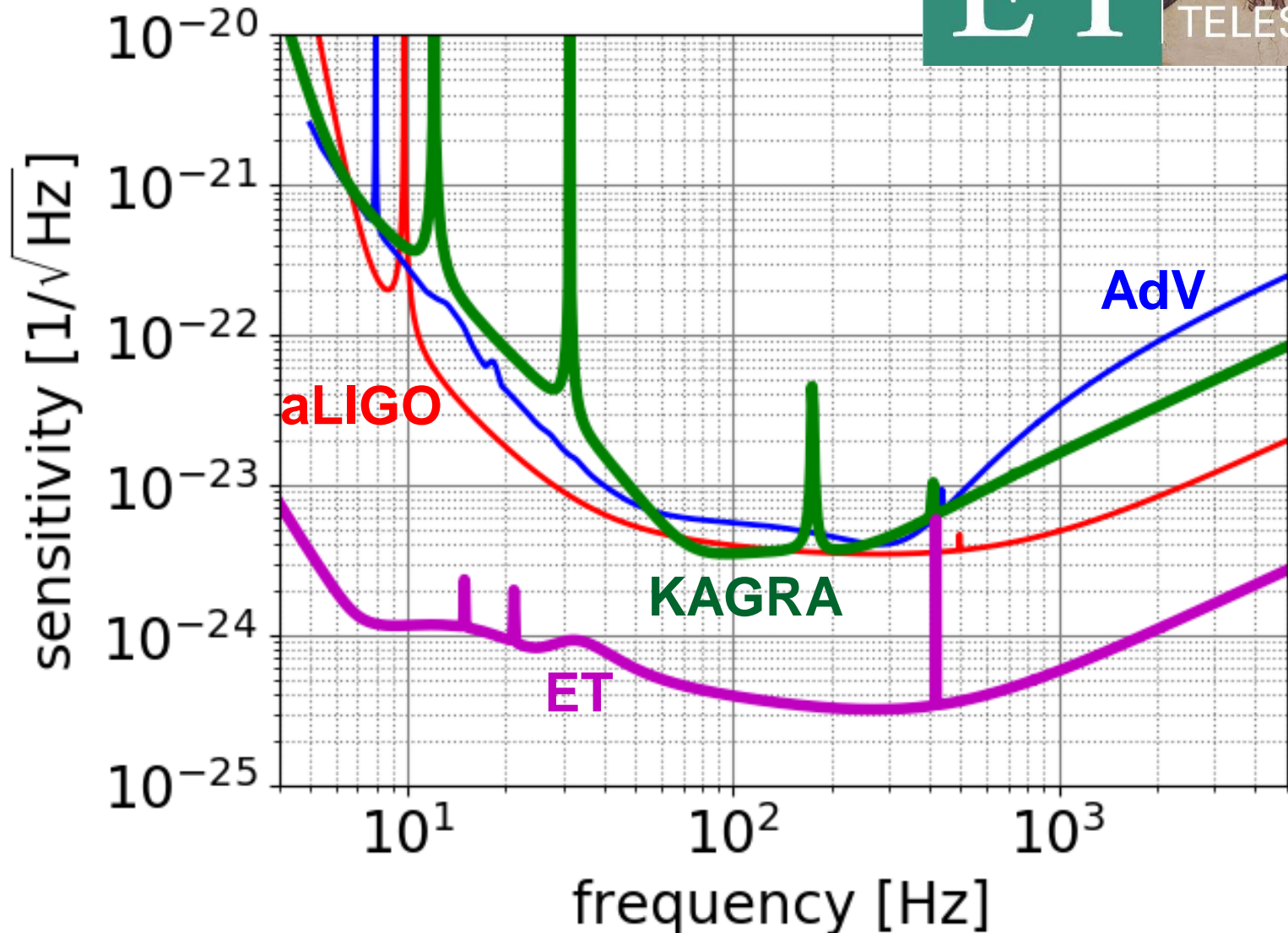
Number of 'normal' suspensions
 (PRM, BS, BD and FC) = 45 for
 linear filtercavities and 54 for
 triangular filter cavities

Beams per tunnel = 7



Einstein Telescope

- Roughly x10 the 2G sensitivity



**Assignment from
Raffaele Flaminio
(by next week)**

Assignment n.1

Consider a Fabry-Perot cavity made of two mirrors M1 and M2. M1 is the input mirror and it has amplitude reflectivity r . M2 is the end mirror and it is perfect reflector. The cavity wavelength is L . E_i is the electric field amplitude of the laser beam entering into the cavity. λ is its wavelength. The cavity is kept in resonance with the laser field.

A gravitational wave produces a small variation of the cavity length $x(t) \ll \lambda$ with linear spectral density $\tilde{x}(f)$.

1. Calculate the variation of the electric field $\tilde{E}_c(f)$ inside the cavity.
2. Calculate the variation of the electric field $\tilde{E}_c(f)$ reflected by the cavity.

Assignment n.2

Consider a double pendulum made of two pendulums in cascade. The double pendulum temperature is $T=300$ K.

The first pendulum has a length $l_1=1$ m and a mass $m_1=100$ kg. the second one hangs from the first mass and has a length $l_2=1$ m and a mass of $m_2=50$ kg.

The first pendulum is affected by a mechanical loss of $\phi_1=10^{-4}$ i.e. the gravitational restoring force has an imaginary part equal to 10^{-4} of its real part.

The second pendulum is affected by a mechanical loss of $\phi_2=10^{-6}$ i.e. the gravitational restoring force has an imaginary part equal to 10^{-6} of its real part.

Using the fluctuation dissipation theorem, calculate the spectrum of the second mass displacement due to thermal noise.

Show that at high frequency the effect of the losses in the upper pendulum can be neglected.

Give an interpretation of this result.

Summary

- Thermal noise
 - suspension / mirror / coating thermal noise
 - cryogenics, low loss angle, longer suspension, and larger mirror reduces thermal noise
 - cryogenics is attractive but challenging
- Seismic noise
 - site selection is very important
 - multiple-stage, low resonant frequency vibration isolation techniques are used
 - underground site is preferred for reducing seismic noise and gravity gradient noise
- KAGRA is currently the only km-scale cryogenic underground GW detector in the world